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MMG LIMITED

五礦資源有限公司

(Incorporated in Hong Kong with limited liability)

(HKEX STOCK CODE: 1208)

(ASX STOCK CODE: MMG)

MINERAL RESOURCES AND ORE RESERVES STATEMENT AS AT 30 JUNE 2018

This announcement is made by MMG Limited (Company or MMG and, together with its subsidiaries, the Group) pursuant to rule 13.09(2) of the Rules Governing the Listing of Securities on The Stock Exchange of Hong Kong Limited (Listing Rules) and the Inside Information Provisions (as defined in the Listing Rules) under Part XIV A of the Securities and Futures Ordinance (Chapter 571 of the Laws of Hong Kong).

The board of directors of the Company (Board) is pleased to report the Group's updated Mineral Resources and Ore Reserves Statement as at 30 June 2018 (Mineral Resources and Ore Reserves Statement).

The key changes to Mineral Resources and Ore Reserves Statement as at 30 June 2018 are:

- The Group's Mineral Resources (contained metal) have decreased for copper (8%), zinc (8%), lead (19%), silver (8%), gold (5%) and molybdenum (9%).
- The Group's Ore Reserves (contained metal) have decreased for copper (8%), zinc (14%), lead (18%), silver (13%), gold (11%) and molybdenum (9%).

For copper metal, the main reasons for the changes are depletion and cost increases at Las Bambas which were partially offset by increased metal price and for zinc metal the main reasons for the changes are depletion and the re-modelling of some areas of the Dugald River deposit following additional drilling.

All data reported here are on a 100% asset basis, with MMG's attributable interest shown against each asset within the Mineral Resources and Ore Reserves tables (pages 4 to 7). Mineral Resources and Ore Reserves for Sepon are not included in this statement as it is subject of a sale process that completed on 30 November 2018.



MMG Limited
MINERAL RESOURCES AND ORE RESERVES STATEMENT
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MINERAL RESOURCES AND ORE RESERVES STATEMENT

A copy of the executive summary of the Mineral Resources and Ore Reserves Statement is annexed to this announcement.

The information referred to in this announcement has been extracted from the report titled Mineral Resources and Ore Reserves Statement as at 30 June 2018 published on 5 December 2018 and is available to view on www.mmg.com. The Company confirms that it is not aware of any new information or data that materially affects the information included in the Mineral Resources and Ore Reserves Statement and, in the case of estimates of Mineral Resources or Ore Reserves, that all material assumptions and technical parameters underpinning the estimates in the Mineral Resources and Ore Reserves Statement continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from the Mineral Resources and Ore Reserves Statement.

By order of the Board
MMG Limited
Gao Xiaoyu
CEO and Executive Director

Hong Kong, 5 December 2018

As at the date of this announcement, the Board comprises nine directors, of which two are executive directors, namely Mr Gao Xiaoyu and Mr Xu Jiqing; three are non-executive directors, namely Mr Guo Wenqing (Chairman), Mr Jiao Jian and Mr Zhang Shuqiang; and four are independent non-executive directors, namely Dr Peter William Cassidy, Mr Leung Cheuk Yan, Ms Jennifer Anne Seabrook and Professor Pei Ker Wei.



MMG Limited
MINERAL RESOURCES AND ORE RESERVES STATEMENT
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EXECUTIVE SUMMARY

Mineral Resources and Ore Reserves for MMG have been estimated as at 30 June 2018, and are reported in accordance with the guidelines in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (2012 JORC Code) and Chapter 18 of the Listing Rules. Mineral Resources and Ore Reserves tables are provided on pages 4 to 7, which include the 30 June 2018 and 30 June 2017 estimates for comparison. The Measured and Indicated Mineral Resources are inclusive of those Mineral Resources that convert to Ore Reserves. All supporting data are provided within the Technical Appendix, available on the MMG website.

Mineral Resources and Ore Reserves information in this statement has been compiled by Competent Persons (as defined by the 2012 JORC Code). Each Competent Person consents to the inclusion of the information in this report that they have provided in the form and context in which it appears. Competent Persons are listed on page 8.

MMG has established processes and structures for the governance of Mineral Resources and Ore Reserves estimation and reporting. MMG has a Mineral Resources and Ore Reserves Committee that regularly convenes to assist the MMG Governance and Nomination Committee and the Board of Directors with respect to the reporting practices of the Company in relation to Mineral Resources and Ore Reserves, and the quality and integrity of these reports of the Group.

Key changes to the Mineral Resources (contained metal) since the 30 June 2017 estimate have been mostly related to depletion¹ together with increased costs at Las Bambas. An increase in metal price assumptions has only partially offset these reductions. At Dugald River, results from close spaced drilling have also resulted in a reduction in the estimated thickness of some parts of the orebody.

Key changes to the Ore Reserves (contained metal) since the 30 June 2017 estimate have been mostly related to depletion. Decreases of Indicated Mineral Resources at Dugald River have resulted in a reduction of available material for conversion to Ore Reserves.

Las Bambas has been operating for 24 months since commercial production was declared on 1 July 2016. During this time the mine has experienced both positive and negative reconciliation factors compared to the Ore Reserve. The 2017 Mineral Resources and Ore Reserves were subject to an external audit in 2018 which recognised that mine practices were still stabilising and made recommendations which could reduce the variations. Any residual discrepancies will be considered prior to the preparation of the 2019 Mineral Resource and Ore Reserve statement.

Pages 9 and 10 provide further discussion of the Mineral Resources and Ore Reserves changes.

¹ Depletion in this report refers to material processed by the mill and depleted from the Mineral Resources and Ore Reserves through mining.



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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MINERAL RESOURCES¹

All data reported here is on a 100% asset basis, with MMG's attributable interest shown against each asset within brackets.

Deposit	2018							2017						
	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)
Las Bambas (62.5%)														
Ferrobamba Oxide Copper														
Indicated	3.0	1.7						9.3	2.0					
Inferred	1.1	1.9						0.6	2.5					
Total	4.1	1.7						9.9	2.0					
Ferrobamba Primary Copper														
Measured	546	0.60			2.7	0.05	204	542	0.64			3.0	0.06	204
Indicated	426	0.61			3.0	0.05	204	546	0.60			2.8	0.05	211
Inferred	254	0.63			3.0	0.05	169	263	0.60			2.4	0.04	158
Total	1,226	0.61			2.9	0.05	197	1,351	0.62			2.8	0.05	198
Ferrobamba Total	1,230							1,361						
Chalcobamba Oxide Copper														
Indicated	6.1	1.5						6.1	1.5					
Inferred	0.7	1.5						0.7	1.5					
Total	6.8	1.5						6.8	1.5					
Chalcobamba Primary Copper														
Measured	75	0.44			1.4	0.02	148	85	0.37			1.1	0.01	148
Indicated	179	0.67			2.5	0.03	140	195	0.67			2.5	0.03	141
Inferred	33	0.54			1.9	0.03	142	36	0.52			1.8	0.02	141
Total	287	0.60			2.2	0.03	143	315	0.57			2.0	0.03	143
Chalcobamba Total	293							322						
Sulfobamba Primary Copper														
Indicated	89	0.65			4.6	0.02	168	85	0.67			4.7	0.02	170
Inferred	106	0.56			6.3	0.02	118	100	0.58			6.5	0.02	119
Total	194	0.60			5.5	0.02	140	184	0.62			5.7	0.02	142
Sulfobamba Total	194							184						
Oxide Copper Stockpile														
Indicated	9.9	1.2						5.5	1.0					
Total	9.9	1.2						5.5	1.0					
Sulphide Stockpile														
Measured	2.3	0.41						0.2	0.85			4.5		148
Total	2.3	0.41						0.2	0.85			4.5		148
Las Bambas Total	1,730							1,873						

¹ S.I. units used for metals of value; Cu=copper, Zn=zinc, Pb=lead, Ag=silver, Au=gold, Mo=molybdenum, Ni=nickel.



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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MINERAL RESOURCES

Deposit	2018							2017						
	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)
Kinsevere (100%)														
Oxide Copper														
Measured	2.0	4.3						3.0	4.4					
Indicated	9.7	3.1						13.6	3.0					
Inferred	1.8	2.4						2.8	2.3					
Total	13.6	3.2						19.4	3.1					
Transition Mixed														
Copper Ore														
Measured	1.3	2.9						0.3	2.7					
Indicated	3.4	2.0						1.4	2.3					
Inferred	0.4	1.9						0.1	2.1					
Total	5.2	2.3						1.8	2.4					
Primary Copper														
Measured	6.1	2.7						0.4	2.5					
Indicated	15.8	2.1						23.8	2.2					
Inferred	2.0	1.7						2.2	1.7					
Total	24.0	2.2						26.4	2.2					
Stockpiles														
Measured														
Indicated	10.2	2.2						7.9	2.5					
Total	10.2	2.2						7.9	2.5					
Kinsevere Total	52.9							55.5						



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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MINERAL RESOURCES

Deposit	2018							2017						
	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)
Dugald River (100%)														
Primary Zinc														
Measured	8.9		12.9	2.3	72			8.1		13.1	2.4	70		
Indicated	24.3		12.6	2.0	30			28.9		12.3	2.3	40		
Inferred	23.5		12.1	1.5	8			27.8		11.4	1.9	10		
Total	56.7		12.4	1.8	27			64.8		12.0	2.2	31		
Primary Copper														
Inferred	6.6	1.5				0.2		4.4	1.8				0.2	
Total	6.6	1.5				0.2		4.4	1.8				0.2	
Dugald River Total	63.3							69.4						
Rosebery (100%)														
Rosebery														
Measured	6.4	0.21	8.6	2.9	113	1.3		6.0	0.26	9.3	3.3	118	1.4	
Indicated	5.6	0.23	7.6	2.4	91	1.2		6.2	0.26	7.9	2.6	112	1.3	
Inferred	6.0	0.28	7.4	2.8	89	1.4		6.5	0.30	7.4	2.7	90	1.4	
Total	18.1	0.24	7.9	2.7	98	1.3		18.6	0.27	8.2	2.9	106	1.4	
Rosebery Total	18.1							18.6						
High Lake (100%)														
High Lake														
Measured														
Indicated	7.9	3.0	3.5	0.3	83	1.3		7.9	3.0	3.5	0.3	83	1.3	
Inferred	6.0	1.8	4.3	0.4	84	1.3		6.0	1.8	4.3	0.4	84	1.3	
Total	14.0	2.5	3.8	0.4	84	1.3		14.0	2.5	3.8	0.4	84	1.3	
Izok Lake (100%)														
Izok Lake														
Measured														
Indicated	13.5	2.4	13	1.4	73	0.18		13.5	2.4	13.3	1.4	73	0.18	
Inferred	1.2	1.5	11	1.3	73	0.21		1.2	1.5	10.5	1.3	73	0.21	
Total	14.6	2.3	13	1.4	73	0.18		14.6	2.3	13.1	1.4	73	0.18	



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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ORE RESERVES¹

All data reported here is on a 100% asset basis, with MMG's attributable interest shown against each asset within brackets.

Deposit	2018							2017						
	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)	Tonnes (Mt)	Cu (%)	Zn (%)	Pb (%)	Ag (g/t)	Au (g/t)	Mo (ppm)
Las Bambas (62.5%)														
Ferrobamba Primary Copper														
Proved	504	0.62			2.9	0.05	197	497	0.68			3.2	0.06	206
Probable	287	0.68			3.7	0.07	179	326	0.71			3.6	0.06	207
Total	791	0.64			3.2	0.06	191	823	0.69			3.4	0.06	207
Chalcobamba Primary Copper														
Proved	56	0.54			1.8	0.02	144	59	0.53			1.8	0.02	141
Probable	139	0.72			2.7	0.03	135	143	0.72			2.7	0.03	132
Total	195	0.67			2.5	0.03	137	202	0.66			2.5	0.03	134
Sulfobamba Primary Copper														
Proved														
Probable	59	0.81			5.9	0.03	161	60	0.80			5.9	0.03	161
Total	59	0.81			5.9	0.03	161	60	0.80			5.9	0.03	161
Primary Copper Stockpiles														
Proved	2.3	0.41			1.7		158	0.17	0.85			4.5		148
Total	2.3	0.41			1.7		158	0.17	0.85			4.5		148
Las Bambas Total	1,048							1,085						
Kinsevere (100%)														
Oxide Copper														
Proved	1.9	4.4						2.6	4.5					
Probable	6.1	3.7						8.1	3.5					
Total	8.0	3.8						10.7	3.7					
Stockpiles														
Proved														
Probable	7.7	2.3						2.5	3.6					
Total	7.7	2.3						2.5	3.6					
Kinsevere Total	15.7							13.2						
Dugald River (100%)														
Primary Zinc														
Proved	6.9		11.5	2.1	65			7.9		11.8	2.1	62		
Probable	21.7		11.7	2.0	30			24.9		11.9	2.2	39		
Total	28.6		11.7	2.0	38			32.8		11.9	2.2	44		
Dugald River Total	28.6							32.8						
Rosebery (100%)														
Proved	3.7	0.21	8.3	3.0	114	1.4		3.8	0.25	9.0	3.4	119	1.4	
Probable	1.7	0.19	7.3	2.9	113	1.4		1.8	0.21	7.6	3.0	131	1.3	
Total	5.4	0.21	8.0	3.0	114	1.4		5.6	0.24	8.6	3.3	123	1.4	
Rosebery Total	5.4							5.6						

¹ S.I. units used for metals of value; Cu=copper, Zn=zinc, Pb=lead, Ag=silver, Au=gold, Mo=molybdenum.



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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COMPETENT PERSONS

Deposit	Accountability	Competent Person	Professional Membership	Employer
MMG Mineral Resources and Ore Reserves Committee	Mineral Resources	Rex Berthelsen ¹	HonFAusIMM(CP)	MMG
MMG Mineral Resources and Ore Reserves Committee	Ore Reserves	Nan Wang ¹	MAusIMM(CP)	MMG
MMG Mineral Resources and Ore Reserves Committee	Metallurgy: Mineral Resources / Ore Reserves	Geoffrey Senior ¹	MAusIMM	MMG
Las Bambas	Mineral Resources	Rex Berthelsen ¹	HonFAusIMM(CP)	MMG
Las Bambas	Ore Reserves	Yao Wu ¹	MAusIMM(CP)	MMG
Las Bambas	Metallurgy: Mineral Resources / Ore Reserves	Amy Lamb ¹	MAusIMM(CP)	MMG
Kinsevere	Mineral Resources	Douglas Corley ¹	MAIG R.P.Geo.	MMG
Kinsevere	Ore Reserves	Jodi Wright ¹	MAusIMM(CP)	MMG
Kinsevere	Metallurgy: Mineral Resources / Ore Reserves	Nigel Thiel ¹	MAusIMM(CP)	MMG
Rosebery	Mineral Resources	Anna Lewin	MAusIMM(CP)	MMG
Rosebery	Ore Reserves	Karel Steyn ¹	MAusIMM	MMG
Rosebery	Metallurgy: Mineral Resources / Ore Reserves	Kevin Rees	MAusIMM(CP)	MMG
Dugald River	Mineral Resources	Douglas Corley ¹	MAIG R.P.Geo.	MMG
Dugald River	Ore Reserves	Karel Steyn ¹	MAusIMM	MMG
Dugald River	Metallurgy: Mineral Resources / Ore Reserves	Nigel Thiel ¹	MAusIMM(CP)	MMG
High Lake, Izok Lake	Mineral Resources	Allan Armitage	MAPEG ² (P.Geo)	Formerly MMG

The information in this report that relates to Mineral Resources and Ore Reserves is based on information compiled by the listed Competent Persons, who are Members or Fellows of the Australasian Institute of Mining and Metallurgy (AusIMM), the Australian Institute of Geoscientists (AIG) or a Recognised Professional Organisation (RPO) and have sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which they are undertaking to qualify as Competent Persons as defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Each of the Competent Persons has given consent to the inclusion in the report of the matters based on their information in the form and context in which it appears.

¹ Participants in the MMG Long-Term Incentive Plans which may include Mineral Resources and Ore Reserves growth as a performance condition

² Member of the Association of Professional Engineers and Geoscientists of British Columbia



SUMMARY OF SIGNIFICANT CHANGES

MINERAL RESOURCES

Mineral Resources as at 30 June 2018 have changed since the 30 June 2017 estimate for a number of reasons with the most significant changes outlined in this section.

Decreases:

The decreases in Mineral Resources (contained metal) are due to:

- depletion at all producing operations;
- higher cost assumptions at Las Bambas;
- re-modelling at Dugald River following results from closer spaced drilling;
- re-modelling at Rosebery following additional drilling, partially offset by favourable TC/RC's which have improved economics and,
- changes to the pit shell resulting from reduction in minimum mining width at Kinsevere.



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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ORE RESERVES

Ore Reserves as at 30 June 2018 (contained metal) have decreased for copper (8%), zinc (14%), lead (18%), silver (13%), gold (11%) and molybdenum (9%).

Variations to Ore Reserves (contained metal) on an individual site basis are discussed below:

Decreases:

A net reduction in Ore Reserves (metal) for copper, zinc, lead, silver, gold and molybdenum due to:

- depletion at all producing operations;
- a further reduction at Las Bambas due to an increase in cost and modification of recovery formula for the Chalcobamba ore;
- a further reduction at Kinsevere due to an increase in the mining dilution assumption from 5% in 2017 to 10% in 2018 and a slight drop of copper grade in the Mineral Resources model. Inclusion of additional stockpiles did not offset these reductions;
- a further reduction at Dugald River due to stope width reduction from the Mineral Resources model resulting from additional drilling results and Mineral Resources modelling;
- a positive conversion from Mineral Resources to Ore Reserves at Rosebery, but not sufficient to offset depletion.



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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KEY ASSUMPTIONS

PRICES AND EXCHANGE RATES

The following price and foreign exchange assumptions, set according to the relevant MMG Standard as at January 2018, have been applied to all Mineral Resources and Ore Reserves estimates. Price assumptions for all metals have changed from the 2017 Mineral Resources and Ore Reserves statement.

Table 1 : 2018 Price (real) and foreign exchange assumptions

	Ore Reserves	Mineral Resources
Cu (US\$/lb)	3.02	3.51
Zn (US\$/lb)	1.23	1.47
Pb (US\$/lb)	0.97	1.16
Au US\$/oz	1236	1442
Ag US\$/oz	17.9	20.3
Mo (US\$/lb)	8.08	9.39
USD:CAD	1.18	As per Ore Reserves
AUD:USD	0.80	
USD:PEN	3.10	

Table 2 : 2017 Price (real) and foreign exchange assumptions

	Ore Reserves	Mineral Resources
Cu (US\$/lb)	2.96	3.40
Zn (US\$/lb)	1.19	1.43
Pb (US\$/lb)	0.95	1.14
Au US\$/oz	1200	1400
Ag US\$/oz	17.5	20.4
Mo (US\$/lb)	8.3	9.5
USD:CAD	1.18	As per Ore Reserves
AUD:USD	0.80	As per Ore Reserves
USD:PEN	3.10	

Table 3 – Differences in Prices (real) and foreign exchange assumptions (2017 – 2018)

	Ore Reserves	Mineral Resources
Cu (US\$/lb)	0.06	0.11
Zn (US\$/lb)	0.04	0.04
Pb (US\$/lb)	0.02	0.02
Au US\$/oz	36	42
Ag US\$/oz	0.4	-0.1
Mo (US\$/lb)	-0.22	-0.11
USD:CAD	0	
AUD:USD	0	
USD:PEN	0	



MINERAL RESOURCES AND ORE RESERVES STATEMENT

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CUT-OFF GRADES

Mineral Resources and Ore Reserves cut-off values are shown in Table 4 and Table 5 respectively.

Table 4 : Mineral Resources cut-off grades

Site	Mineralisation	Likely Mining Method ¹	Cut-Off Value	Comments
Las Bambas	Oxide Copper	OP	1% Cu	Cut-off is applied as a range that varies for each deposit and mineralised rock type at Las Bambas. <i>In-situ</i> copper Mineral Resources constrained within US\$3.51/lb Cu pit shell.
	Primary Copper	OP	0.16 – 0.23% Cu	
Kinsevere	Oxide Copper & Stockpiles	OP	0.6% CuAS ²	<i>In-situ</i> copper Mineral Resources constrained within a US\$3.51/lb Cu pit shell.
	Transition Mixed Copper	OP	0.6-0.7% Cu ³	
	Primary Copper	OP	0.7% Cu ³	
Rosebery	Rosebery (Zn, Cu, Pb, Au, Ag)	UG	A\$167/t NSR ⁴	Remnant upper mine areas A\$179/t NSR ⁴
Dugald River	Primary Zinc (Zn, Pb, Ag)	UG	A\$146/t NSR ⁴	
	Primary Copper	UG	1% Cu	
High Lake	Cu, Zn, Pb, Ag, Au	OP	2.0% CuEq ⁵	CuEq ⁵ = Cu + (Zn×0.30) + (Pb×0.33) + (Au×0.56) + (Ag×0.01); based on Long-Term prices and metal recoveries at Au:75%, Ag:83%, Cu:89%, Pb:81% and Zn:93%.
High Lake Izok Lake	Cu, Zn, Pb, Ag, Au Cu, Zn, Pb, Ag, Au	UG	4.0% CuEq ⁵	CuEq ⁵ = Cu + (Zn×0.30) + (Pb×0.33) + (Au×0.56) + (Ag×0.01); based on Long-Term prices and metal recoveries at Au:75%, Ag:83%, Cu:89%, Pb:81% and Zn:93%.
		OP	4.0% ZnEq ⁶	ZnEq ⁶ = Zn + (Cu×3.31) + (Pb×1.09) + (Au×1.87) + (Ag×0.033); prices and metal recoveries as per High Lake.

¹ OP = Open Pit, UG = Underground

² CuAS = Acid Soluble Copper

³ Cu = Total Copper

⁴ NSR = Net Smelter Return

⁵ CuEq = Copper Equivalent

⁶ ZnEq = Zinc Equivalent



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Table 5 : Ore Reserves cut-off grades

Site	Mineralisation	Mining Method	Cut-Off Value	Comments
Las Bambas	Primary Copper Ferrobamba	OP	0.19 – 0.26 %Cu	Range based on rock type recovery.
	Primary Copper Chalcobamba		0.21 – 0.28 %Cu	
	Primary Copper Sulfobamba		0.24 – 0.28 %Cu	
Kinsevere	Copper Oxide	OP	1.4% CuAS ¹	Approximate cut-off grades shown in this table for ex-pit material. Variable cut-off grade based on net value script.
		OP	1.0% CuAS ¹	For existing stockpiles reclaim.
Rosebery	(Zn, Cu, Pb, Au, Ag)	UG	A\$167/t NSR ²	
Dugald River	Primary Zinc	UG	A\$146/t NSR ²	

¹ CuAS = Acid Soluble Copper

² NSR = Net Smelter Return



MMG Limited
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PROCESSING RECOVERIES

Average processing recoveries are shown in Table 6. More detailed processing recovery relationships are provided in the Technical Appendix.

Table 6: Processing Recoveries

Site	Product	Recovery						Concentrate Moisture Assumptions
		Copper	Zinc	Lead	Silver	Gold	Mo	
Las Bambas	Copper Concentrate	86%	-	-	75%	71%		10%
	Molybdenum Concentrate						55%	5%
Rosebery	Zinc Concentrate		84%		8%	6%		8%
	Lead Concentrate		7%	81%	41%	13%		6%
	Copper Concentrate	57%			43%	33%		9%
	Doré ¹ (gold and silver)				0.2%	31%		
Dugald River	Zinc Concentrate	-	87%		25%	-		10%
	Lead Concentrate	-		70%	40%	-		10%
Kinsevere	Copper Cathode	76% (96% CuAS ²)	-	-	-	-		-

The Technical Appendix published on the MMG website contains additional Mineral Resources and Ore Reserves information (including the Table 1 disclosure).

¹ Silver in Rosebery doré is calculated as a constant ratio to gold in the doré. Silver is set to 0.17 against gold being 20.7

² CuAS = Acid Soluble Copper



MMG Mineral Resources and Ore Reserves Statement as at 30 June 2018

Technical Appendix

5 December 2018

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APPROVALS PAGE

	Rex Berthelsen	Group Manager Resource Geology	5/12/18
Signature	Name	Position	Date
	Nan Wang	Group Manager Mining	5/12/18
Signature	Name	Position	Date
	Geoffrey Senior	General Manager Group Technical Services	5/12/18
Signature	Name	Position	Date

The above signed endorse and approve this Mineral Resources and Ore Reserves Statement Technical Appendix.

1 INTRODUCTION

On 20th December 2012 an updated JORC¹ Code was released – the previous release being the 2004 Edition. The JORC Code 2012 Edition defines the requirements for public reporting of Exploration Results, Mineral Resources and Ore Reserves by mining companies. Reporting according to the JORC Code is a requirement of the MMG listing on The Stock Exchange of Hong Kong² as per amendments to Chapter 18 of the Listing Rules that were announced on 3rd June 2010.

The core of the change to JORC Code is enhanced disclosure of the material information prepared by the Competent Person with the requirement for the addition of a publicly released detailed Appendix to the Mineral Resources and Ore Reserves release document, which outlines the supporting details to the Mineral Resources and Ore Reserves numbers.

This Technical Appendix provides these supporting details.

Under the JORC Code, reporting in compliance with the guidelines of JORC Code 2012 Edition became compulsory from 1 Dec 2013.

The principles governing the operation and application of the JORC Code are Transparency, Materiality and Competence:

- Transparency requires that the reader of a Public Report is provided with sufficient information, the presentation of which is clear and unambiguous, to understand the report and not be misled by this information or by omission of material information that is known to the Competent Person.
- Materiality requires that a Public Report contains all the relevant information that investors and their professional advisers would reasonably require, and reasonably expect to find in the report, for the purpose of making a reasoned and balanced judgment regarding the Exploration Results, Mineral Resources or Ore Reserves being reported. Where relevant information is not supplied an explanation must be provided to justify its exclusion.
- Competence requires that the Public Report be based on work that is the responsibility of suitably qualified and experienced persons who are subject to an enforceable professional code of ethics (the Competent Person).

¹ JORC = Joint Ore Reserves Committee.

² Specifically, the Updated Rules of Chapter 18 of the Hong Kong Stock Exchange Listing Rules require a Competent Person's report to comply with standards acceptable to the HKSE including JORC Code (the Australian code), NI 43-101 (the Canadian code) and SAMREC Code (the South African code) for Mineral Resources and Ore Reserves. MMG Limited has chosen to report using the JORC Code.

2 COMMON TO ALL SITES

The economic analysis undertaken for each Ore Reserves described in this document and for the whole Company has resulted in positive net present values (NPVs). MMG uses a discount rate appropriate to the size and nature of the organisation and individual deposits.

2.1 Commodity Price Assumptions

The price and foreign exchange assumptions used for the 2018 Mineral Resources and Ore Reserves estimation at the date at which work commenced on the Mineral Resources and Ore Reserves are as shown in Table 1.

Table 1 Price (real) and foreign exchange assumptions

	Ore Reserves	Mineral Resources
Cu (US\$/lb)	3.02	3.51
Zn (US\$/lb)	1.23	1.47
Pb (US\$/lb)	0.97	1.16
Au US\$/oz	1236	1442
Ag US\$/oz	17.9	20.3
Mo (US\$/lb)	8.08	9.39
USD:CAD	1.18	As per Ore Reserves
AUD:USD	0.80	
USD:PEN	3.10	

2.2 Competent Persons

Table 2 – Competent Persons

Deposit	Accountability	Competent Person	Professional Membership	Employer
MMG Mineral Resources and Ore Reserves Committee	Mineral Resources	Rex Berthelsen ¹	HonFAusIMM(CP)	MMG
MMG Mineral Resources and Ore Reserves Committee	Ore Reserves	Nan Wang ¹	MAusIMM(CP)	MMG
MMG Mineral Resources and Ore Reserves Committee	Metallurgy: Mineral Resources / Ore Reserves	Geoffry Senior ¹	MAusIMM	MMG
Las Bambas	Mineral Resources	Rex Berthelsen ¹	HonFAusIMM(CP)	MMG
Las Bambas	Ore Reserves	Yao Wu ¹	MAusIMM(CP)	MMG
Las Bambas	Metallurgy: Mineral Resources / Ore Reserves	Amy Lamb ¹	MAusIMM(CP)	MMG
Kinsevere	Mineral Resources	Douglas Corley ¹	MAIG R.P.Geo.	MMG
Kinsevere	Ore Reserves	Jodi Wright ¹	MAusIMM(CP)	MMG
Kinsevere	Metallurgy: Mineral Resources / Ore Reserves	Nigel Thiel ¹	MAusIMM(CP)	MMG
Rosebery	Mineral Resources	Anna Lewin	MAusIMM(CP)	MMG
Rosebery	Ore Reserves	Karel Steyn ¹	MAusIMM	MMG
Rosebery	Metallurgy: Mineral Resources / Ore Reserves	Kevin Rees	MAusIMM(CP)	MMG
Dugald River	Mineral Resources	Douglas Corley ¹	MAIG R.P.Geo.	MMG
Dugald River	Ore Reserves	Karel Steyn ¹	MAusIMM	MMG
Dugald River	Metallurgy: Mineral Resources / Ore Reserves	Nigel Thiel ¹	MAusIMM(CP)	MMG
High Lake, Izok Lake	Mineral Resources	Allan Armitage	MAPEG ² (P.Geo)	Formerly MMG

The information in this report that relates to Mineral Resources and Ore Reserves is based on information compiled by the listed Competent Persons, who are Members or Fellows of the Australasian Institute of Mining and Metallurgy (AusIMM), the Australian Institute of Geoscientists (AIG) or a Recognised Professional Organisation (RPO) and have sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which they are undertaking to qualify as Competent Persons as defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (2012 JORC Code). Each of the Competent Persons has given consent to the inclusion in the report of the matters based on their information in the form and context in which it appears.

¹ Participants in the MMG Long-Term Incentive Plans which may include Mineral Resources and Ore Reserves growth as a performance condition.

² Member of the Association of Professional Engineers and Geoscientists of British Columbia.

3 LAS BAMBAS OPERATION

3.1 Introduction and Setting

Las Bambas is a world class copper gold (Cu-Au) mine located in the Andes of southern Peru approximately 75km south-southwest of Cusco, approximately 300km north-northwest of Arequipa, and approximately 150km northeast of Espinar (also named Yauri). Las Bambas is readily accessible from either Cusco or Arequipa over a combination of paved and good quality gravel roads. Road travel from Cusco takes approximately 6 hours, while road travel from Arequipa takes approximately 9 hours.

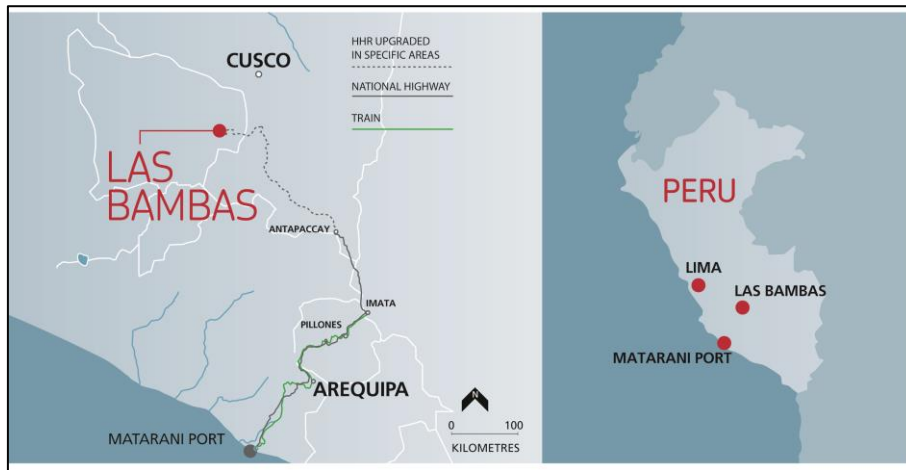


Figure 3-1 Las Bambas Mine location

Las Bambas is a truck and excavator mining operation with a conventional copper concentrator. Copper production commenced in the fourth quarter 2015 with the first concentrate achieved on 26 November. The first shipment of product departed the Port of Matarani for China on 15 January 2016. The mine has achieved full capacity, running at over 400,000 tonnes per day. Both lines of the copper concentrate plant have been commissioned. The primary crusher was commissioned during the fourth quarter of 2015 and the overland conveyor has now reached 100% capacity of 8,000 tonnes per hour. The tailings dam reached planned levels with discharge and water recirculation back to plant fully operational. Commercial production was declared on July 1, 2016.

Las Bambas is a joint venture project between the operator MMG (62.5%), a wholly owned subsidiary of Guoxin International Investment Co. Ltd (22.5%) and CITIC Metal Co. Ltd (15.0%).

The Mineral Resources and Ore Reserves have been updated with additional drilling completed in 2017 for the June 2018 release. The 2018 Mineral Resources estimation includes updated geological interpretation and estimation parameters.

3.2 Mineral Resources – Las Bambas

3.2.1 Results

The 2018 Las Bambas Mineral Resources is summarised in Table 3. The Las Bambas Mineral Resources is inclusive of the Ore Reserves. All data reported here is on a 100% asset basis. MMG's attributable interest in Las Bambas is 62.5%.

Table 3 2018 Las Bambas Mineral Resources tonnage and grade (as at 30 June 2018)

Las Bambas Mineral Resource									
						Contained Metal			
Ferrobamba Oxide Copper ¹	Tonnes (Mt)	Copper (% Cu)	Silver (g/t Ag)	Gold (g/t Au)	Mo (ppm)	Copper (kt)	Silver (Moz)	Gold (Moz)	Mo (kt)
Indicated	3.0	1.7				51			
Inferred	1.1	1.9				20			
Total	4.1	1.7				71			
Ferrobamba Primary Copper²									
Measured	546	0.60	2.7	0.05	204	3,256	48	0.9	111
Indicated	426	0.61	3.0	0.05	204	2,591	41	0.7	87
Inferred	254	0.63	3.0	0.05	169	1,608	24	0.4	43
Total	1,226	0.61	2.9	0.05	197	7,455	113	2.0	241
Ferrobamba Total	1,230	0.61				7,526	113	3.3	241
Chalcobamba Oxide Copper¹									
Indicated	6.1	1.5				89			
Inferred	0.7	1.5				10			
Total	6.8	1.5				99			
Chalcobamba Primary Copper³									
Measured	75	0.44	1.4	0.02	148	335	3	0.04	11
Indicated	179	0.67	2.5	0.03	140	1,206	15	0.18	25
Inferred	33	0.54	1.9	0.03	142	177	2	0.03	5
Total	287	0.60	2.2	0.03	143	1,719	20	0.25	41
Chalcobamba Total	293	0.62	2.1	0.03	139	1,818	20	1.12	41
Sulfobamba Oxide Copper¹									
Inferred									
Total									
Sulfobamba Primary Copper⁴									
Indicated	89	0.65	4.6	0.02	168	579	13	0.1	15
Inferred	106	0.56	6.3	0.02	118	596	21	0.1	12
Total	194	0.60	5.5	0.02	140	1,175	34	0.1	27
Sulfobamba Total	194	0.60	5.5	0.02	140	1,175	34	0.1	27
Oxide Stockpiles									
Indicated	9.9	1.2				10			
Sulphide Stockpiles									
Measured	2.3	0.41	1.7		158	9.5	0.13		0.36
Total Contained	1,730					10,649	168	2.4	310

Notes:

- 1% Cu Cut-off grade contained within a US\$3.51/lb pit shell for oxide material.
 - Average (0.16% Cu) cut-off grade contained within a US\$3.51/lb pit shell for primary material.
 - Average (0.18% Cu) cut-off grade contained within a US\$3.51/lb pit shell for primary material.
 - Average (0.19% Cu) cut-off grade contained within a US\$3.51/lb pit shell for primary material.
- Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors. Contained metal does not imply recoverable metal.

3.2.2 Mineral Resources JORC 2012 Assessment and Reporting Criteria

The following information provided in Table 4 complies with the 2012 JORC Code requirements specified by "Table-1 Section 1-3" of the Code.

Table 4 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Las Bambas Mineral Resources 2018

Assessment Criteria	Commentary
Section 1 Sampling Techniques and Data	
Sampling techniques	<ul style="list-style-type: none"> • Diamond drilling (DD) was used to obtain an average 2m sample that is half core split, crushed and pulverised to produce a pulp (95% passing 105µm). Diamond core is selected, marked and numbered for sampling by the logging geologist. Sample details are stored in an acQure database for correlation with returned geochemical assay results. • Samples for analysis are bagged, shuffled, re-numbered and de-identified prior to dispatch. • Whole core was delivered to the Inspectorate Laboratory in Lima (2005-2010) and Certimin Laboratory in Lima (2014 to 2015) for half core splitting and sample preparation. From mid-2015 core samples were cut and sampled at an ALS sample preparation laboratory on-site. Samples are then sent to ALS Lima for preparation and analysis. • There are no inherent sampling problems recognised. • Measures taken to ensure sample representivity include the collection, and analysis of coarse crush duplicates.
Drilling techniques	<ul style="list-style-type: none"> • The drilling type is wireline diamond core drilling from surface. Drill core is not oriented. All drillholes used in the Mineral Resource estimates have been drilled using HQ size.
Drill sample recovery	<ul style="list-style-type: none"> • Recovery is estimated by measuring the recovered core within a drill run length and recorded in the acQure database. Run by run recovery has been recorded for 436,248m of the total 449,211m of diamond drilling in the data used for Mineral Resources estimation for the Sulfobamba, Chalcobamba and Ferrobamba deposits. Diamond drill recovery average is about 97% for all deposits (98% for Sulfobamba, 97% for Chalcobamba and Ferrobamba deposits). • The drilling process is controlled by the drill crew and geological supervision provides a means for maximising sample recovery and ensures suitable core presentation. No other measures are taken to maximise core recovery. • There is no detectable correlation between recovery and grade which can be determined from graphical and statistical analysis. Preferential loss/gains of fine or coarse materials are not significant and do not result in sample bias as the nature of mineralisation is stockwork veins and disseminated sulphides. Diamond core sampling is applied and recovery is considered high.
Logging	<ul style="list-style-type: none"> • 100% of diamond drill core used in the Mineral Resource estimates has been geologically and geotechnically logged to support Mineral Resources estimation, mining and metallurgy studies. • Geological logging is qualitative and geotechnical logging is quantitative. All drill core is photographed.

Assessment Criteria	Commentary
Section 1 Sampling Techniques and Data	
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> • All samples included in the Mineral Resource estimates are from diamond drill core. Drill core is longitudinally sawn to provide half-core samples within intervals directed by the logging geologist. The remaining half-core is kept and stored in the original sample tray. The standard sampling length is 2m for PQ core (minimum 1.2m) and HQ core (minimum 1.2m, maximum 2.2m) while NQ core is sampled at 2.5m (minimum 1.5m). Sample intervals do not cross geological boundaries. • From 2005 until 2010 geological samples have been processed in the following manner: Dried, crushed, pulverised to 95% passing 105µm. Sizing analysis is carried out on 1 in 30 samples. • From 2010 geological samples have been processed in the following manner: Dried, crushed, pulverised to 95% passing 105µm. Sizing analyses are carried out on one in 10-15 samples. • Representivity of samples is checked by duplication at the crush stage one in every 40 samples. No field duplicates are taken. • Twelve month rolling Quality Assurance / Quality Control (QAQC) analysis of sample preparation techniques indicates the process is appropriate for Las Bambas samples. • The sample types, nature, quality and sample preparation techniques are considered appropriate for the style of the Las Bambas mineralisation (porphyry and skarn Cu-Mo mineralisation) by the Competent Person.
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> • From 2005 until 2010 the assay methods undertaken by Inspectorate (Lima) for Las Bambas were as follows: <ul style="list-style-type: none"> ○ Cu, Ag, Pb, Zn, Mo - 0.5g of sample. Digestion by 4-Acids. Reading by Atomic Absorption Spectrometry (AAS). ○ Acid soluble - 0.2g sample. Leaching by a 15% solution of H₂SO₄ at 73°C for 5 minutes. Reading by AAS. ○ Acid soluble - 0.2g of sample. Digestion by a citric acid solution at 65°C for 15 minutes. Reading by AAS. ○ Au - Cupellation at 950°C. Reading by AAS. Above detection limit analysis by gravimetry. ○ 35 elements - Digestion by aqua-regia and reading by ICP. • From 2010 to 2015 routine assay methods undertaken by Certimin (Lima) for Las Bambas are as follows: <ul style="list-style-type: none"> ○ Cu, Ag, Pb, Zn, Mo - 0.5g of sample. Digestion by 4-Acids. Reading by Atomic Absorption Spectrometry (AAS). ○ Acid soluble copper – 0.2g sample. Leaching by a 15% solution of H₂SO₄ at 73°C for 5 minutes. Reading by AAS. ○ Acid Soluble copper - 0.2g of sample. Digestion by a citric acid solution at 65°C for 15 minutes. Reading by AAS. ○ Au - Fire assay with AAS Finish. Over-range results are re-assayed by Gravimetric Finish. ○ 35 elements - Digestion by aqua-regia and reading by ICP. • From 2015 to present routine assay methods undertaken by ALS (Lima) for Las Bambas are as follows: <ul style="list-style-type: none"> ○ Cu, Ag, Pb, Zn, Mo - 0.5g of sample. Digestion by 4-Acids. Reading by Atomic

Assessment Criteria	Commentary
Section 1 Sampling Techniques and Data	
	<p>Absorption Spectrometry (AAS).</p> <ul style="list-style-type: none"> ○ Acid soluble copper – 0.5g sample. Leaching by a 5% solution of H₂SO₄ at ambient temperature for 1 hour. Reading by AAS. ○ Au - Fire assay with AAS Finish. Over-range results are re-assayed by Gravimetric Finish. ○ 35 elements - Digestion by aqua-regia and reading by ICP. <ul style="list-style-type: none"> ● All of the above methods with the exception of the acid soluble copper are considered total digest. ● Since 2013, composited pulps have been submitted to Certimin Laboratory for sequential copper analysis. This method produces results of acid soluble (H₂SO₄), then cyanide soluble followed by residual copper in sequence. This analysis is used for geometallurgical modelling. ● No geophysical tools, spectrometers or handheld XRF instruments have been used in the analysis of samples external to the ALS laboratory for the estimation of Mineral Resources. ● Assay techniques are considered suitable and representative; independent umpire laboratory checks occurred routinely between 2005-2010 using the ALS Chemex laboratory in Lima. Check samples were inserted at a rate of 1 in every 25 samples (2005-2007), every 50 samples (2008) and every 40 samples (2010). For the 2014 to 2017 programs, duplicated samples were collected at the time of sampling and securely stored. Samples were then sent to the Inspectorate Laboratory, Lima, for third party (umpire) analysis. The samples were selected at a rate of 1:40. Results received indicate a good correlation between datasets and show no bias for copper, molybdenum, silver and gold. ● Inspectorate, Certimin and ALS release quarterly QAQC data to Las Bambas for analysis of internal laboratory standard performance. The performance of the laboratory internal standards is within acceptable limits. ● Las Bambas routinely insert: <ul style="list-style-type: none"> ○ Primary coarse duplicates: Inserted at a rate of 1:25 samples (2005-2007), 1:50 samples (2008), and 1:40 samples (2010- present). ○ Coarse blank samples: Inserted after a high-grade sample (coarse blank samples currently make up about 4.2% of all samples analysed). ○ Pulp duplicates samples: Inserted 1:25 samples (2005-2007), 1:50 samples (2008), and 1:40 samples (2010-present). ○ Pulp blank samples: Inserted before the coarse blank sample and always after a high grade sample (pulp blank samples currently make up about 4.2% of all samples analysed). ○ Certified Reference Material (CRM) samples: Inserted at a rate of 1:50 samples (2005-2006), 1:40 samples (2007) and 1:20 samples (2008 to present). ● QAQC analysis has shown that: <ul style="list-style-type: none"> ○ Blanks: a minimum level of sample contamination by copper was detected during the sample preparation and assay. ○ Duplicates: the analytical precision is within acceptable ranges when compared to the original sample, i.e., more than 90% of the pairs of samples are within the

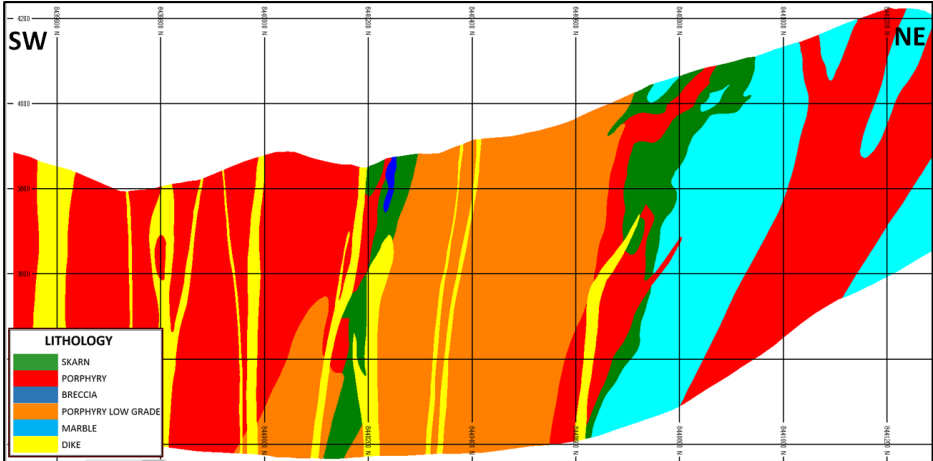
Assessment Criteria	Commentary
Section 1 Sampling Techniques and Data	
	<p>error limits evaluated for a maximum relative error of 10% ($R^2 > 0.90$). These results were also repeated in the external ALS check samples.</p> <ul style="list-style-type: none"> ○ Certified Reference Material: acceptable levels of accuracy and precision have been established. • Sizing test results are not routinely analysed.
Verification of sampling and assaying	<ul style="list-style-type: none"> • Verification by independent personnel was not undertaken at the time of drilling. However, drilling, core logging and sampling data is entered by geologists; assay results are entered by the resource geologist after data is checked for outliers, sample swaps, performance of duplicates, blanks and standards, and significant intersections are checked against core log entries and core photos. Errors are rectified before data is entered into the database. • Apart from 20 metallurgical drillholes drilled in 2007 which twinned Mineral Resource Ferrobamba drillholes, no twinned drillholes have been completed. • All drillholes are logged using laptop computers directly into the drillhole database (acQuire). Prior to November, 2014 diamond drillholes were logged on paper and transcribed into the database. Assay results are provided in digital format (both spreadsheet and PDF) by the laboratories and are automatically loaded into the database after validation. All laboratory primary data and certificates are stored on the Las Bambas server. • The database has internal validation processes which prevent invalid or unapproved records from being stored. Additional manual data validation occurs in Vulcan software before data is used for interpretation and Mineral Resources modelling. Unreliable data is flagged and excluded from Mineral Resources estimation work. • No adjustments have been made to assay data – if there is any doubt about the data quality or location, the drillhole is excluded from the estimation process.
Location of data points	<ul style="list-style-type: none"> • In 2005 collar positions of surface drillholes were picked up by Horizons South America using Trimble 5700 differential GPS equipment. From 2006, the Las Bambas engineering personnel have performed all subsequent surveys using the same equipment. Since 2014, drillholes are set out using UTM co-ordinates with a hand held Differential Global Positioning System (DGPS) and are accurate to within 1m. On completion of drilling, collar locations are picked up by the onsite surveyors using DGPS (Trimble or Topcon). These collar locations are accurate to within 0.5m. • During the 2014 due diligence process (2014) RPM independently checked five collar locations at Ferrobamba and Chalcobamba with a handheld GPS and noted only small differences and well within the error limit of the GPS used. RPM did not undertake independent checking of any Sulfobamba drillholes. The collar locations are considered accurate for Mineral Resources estimation work. • In 2005 the drilling contractor conducted downhole survey's using the AccuShot method for non-vertical drillholes. Vertical holes were not surveyed. If the AccuShot arrangement was not working, the acid test (inclination only) was used. Since 2006, all drillholes are surveyed using Reflex Maxibor II equipment units which take measurements every 3m. The downhole surveys are considered accurate for Mineral Resources estimation work.

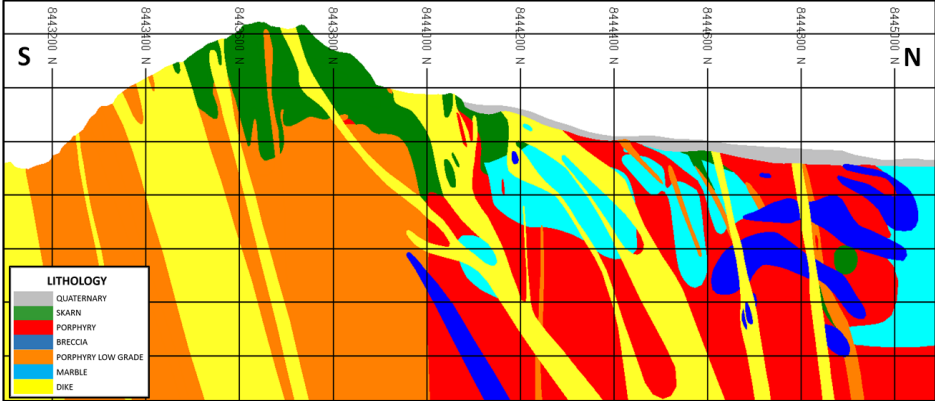
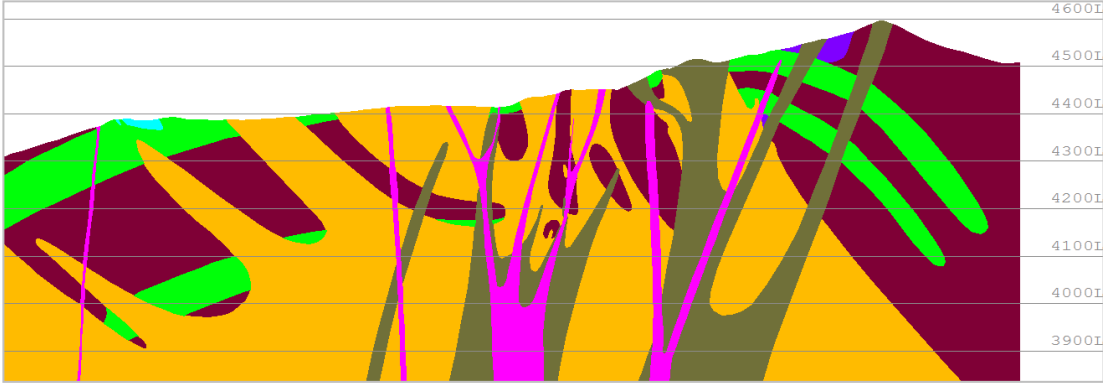
Assessment Criteria	Commentary
Section 1 Sampling Techniques and Data	
	<ul style="list-style-type: none"> • The datum used is WGS 84 with a UTM coordinate system zone 19 South. • In 2006 Horizons South America surveyed the topography at a scale of 1:1000 based on aerophotogrammetric restitution of orthophotos. A digital model of the land was generated every 10m and, using interpolation, contour lines were obtained every metre. The maps delivered were drafted in UTM coordinates and the projections used were WGS 84 and PSAD 56. A triangulated surface model presumably derived from this survey is in current use at site and is considered suitable for Mineral Resources and Ore Reserves estimation purposes.
Data spacing and distribution	<ul style="list-style-type: none"> • The Las Bambas mineral deposits are drilled on variable spacing dependent on rock type (porphyry vs. skarn). Drill spacing typically ranges from 100m x 100m to 25m x 25m and is considered sufficient to establish the degree of geological and grade continuity appropriate for Mineral Resources estimation and classifications applied. • Drillhole spacing of approximately 25m x 25m within skarn hosted material and 50m x 50m within porphyry hosted is considered sufficient for long term Mineral Resources estimation purposes based on a drillhole spacing study undertaken in 2015. While the 25m spacing is suitable for Mineral Resource estimation, the Las Bambas deposits tend to have short scale 5m - 10m variations within the skarn that are not captured by the infill drilling at this spacing. This localised geological variability is captured by mapping and drillhole logging. • Diamond drillhole samples are not composited prior to routine chemical analysis; however the nominal sample length is generally 2m. All sequential copper analysis is undertaken on pulps that are composited most commonly to 8m but sample lengths as small as 1m are contained in the database. • A programme of pulp re-analysis has commenced in 2018 to acquire sequential copper analyses on the original 2m sample pulps.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> • Overall drillhole orientation is planned at 90 degrees to the strike of the mineralised zone for each deposit. Drillhole spacing and orientation is planned to provide evenly spaced, high angle intercepts of the mineralised zone where possible, thus minimising sampling bias related to orientation. However, in some locations namely the east and western areas of Ferrobamba containing skarn, due to the orientation of the drilling grid some drillholes are orientated along strike, yet still manage to intersect the ore zones at moderate angles. • Drilling orientation is not considered to have introduced sampling bias.
Sample security	<ul style="list-style-type: none"> • Measures to provide sample security include: <ul style="list-style-type: none"> ○ Adequately trained and supervised sampling personnel. ○ Samples are stored in a locked compound with restricted access during preparation. ○ Dispatch to various laboratories via contract transport provider in sealed containers. ○ Receipt of samples acknowledged by receiving analytical laboratory by email and checked against expected submission list. ○ Assay data returned separately in both spreadsheet and PDF formats.
Audit and	<ul style="list-style-type: none"> • In 2015, an internal audit, checking 5% of the total samples contained in the acquire

Assessment Criteria	Commentary
Section 1 Sampling Techniques and Data	
reviews	<p>database was undertaken comparing database entry values to the original laboratory certificates for Cu, Ag, Mo, As and S. No material issues were identified.</p> <ul style="list-style-type: none"> Internal audits of the Inspectorate and Certimin laboratories have occurred twice a month by Las Bambas personnel. Historically, any issues identified have been rectified. Currently, there are no outstanding material issues. An independent third party audit was completed by AMC Consultants (Brisbane office) on the 2017 Mineral Resource model in February 2018. The audit identified some minor improvements to the estimation process but concluded there were not material issues or risks to long term mine planning. The Competent Person has visited the both the Certimin and ALS laboratories in Lima.

Assessment Criteria	Commentary
Section 2 Reporting of Exploration Results	
Mineral tenement and land tenure status	<ul style="list-style-type: none"> The Las Bambas project has tenure over 41 Mineral Concessions. These Mineral Concessions secure the right to the minerals in the area, but do not provide rights to the surface land. Property of surface land is acquired through a separate process. The below map outlines the 41 Mineral Concessions and the mine property owned by MMG. <div data-bbox="491 1272 1300 1818" style="text-align: center;"> </div> <ul style="list-style-type: none"> Tenure over the 41 Concessions is in good standing. There are no known impediments to operating in the area.

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Section 2 Reporting of Exploration Results																																																																																																																																																																								
Exploration done by other parties	<ul style="list-style-type: none"> The Las Bambas project has a long history of exploration by the current and previous owners. Exploration commenced in 1966 with around 450km of surface diamond drilling drilled to date. Initial exploration was completed by Cerro de Pasco followed by Cyprus, Phelps Dodge, BHP, Tech, and Pro Invest prior to Xstrata Resources definition drilling which commenced in 2005. All historical drilling is outlined in the table below. Glencore and Xstrata merged to form Glencore plc. In 2013, MMG Ltd, Guoxin International Investment Corporation. Limited and CITIC Metal Co., Ltd enter into an agreement to purchase the Las Bambas project from Glencore plc. <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: left;">Company</th> <th style="text-align: left;">Year</th> <th style="text-align: left;">Deposit</th> <th style="text-align: left;">Purpose</th> <th style="text-align: left;">Type</th> <th style="text-align: left;"># of DDH</th> <th style="text-align: left;">Drill size</th> <th style="text-align: right;">Metres Drilled</th> </tr> </thead> <tbody> <tr> <td rowspan="2">Cerro de Pasco</td> <td>1996</td> <td>Chalcobamba</td> <td>Exploration</td> <td></td> <td>6</td> <td></td> <td style="text-align: right;">906.4</td> </tr> <tr> <td>1996</td> <td>Chalcobamba</td> <td>Exploration</td> <td>DDH</td> <td>9</td> <td>Unknown</td> <td style="text-align: right;">1,367.3</td> </tr> <tr> <td rowspan="2">Phelps Dodge</td> <td rowspan="2">1997</td> <td>Ferrobamba</td> <td 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Geology	<ul style="list-style-type: none"> Las Bambas is located in a belt of Cu (Mo-Au) skarn deposits associated with porphyry type systems situated in south-eastern Peru. This metallogenic belt is controlled by the Andahuaylas-Yauri Batholith of Eocene- Oligocene age, which is emplaced in Mesozoic sedimentary units, with the Ferrobamba Formation (Lower to Upper Cretaceous) being 																																																																																																																																																																							

Assessment Criteria	Commentary
Section 2 Reporting of Exploration Results	
	<p>of greatest mineralising importance.</p> <ul style="list-style-type: none"> The porphyry style mineralisation occurs in quartz-monzonite to granodiorite rocks. Hypogene copper sulphides are the main copper bearing minerals with minor occurrence of supergene copper oxides and carbonates near surface. The intrusive rocks of the batholith in contact with the Ferrobamba limestones gave rise to contact metamorphism and, in certain locations, skarn bodies with Cu (Mo-Au) mineralisation.
Drillhole information	<ul style="list-style-type: none"> Historical exploration drillholes (prior to 2005) have been excluded from the Mineral Resource estimates. Drillhole data is not provided in this report as this report is for the Las Bambas Mineral Resources which use all available data and no single hole is material for the Mineral Resource estimates.
Data aggregation methods	<ul style="list-style-type: none"> Historical exploration drillholes (prior to 2005) have been excluded from the Mineral Resource estimates. No metal equivalents were used in the Mineral Resources estimation.
Relationship between mineralisation width and intercepts lengths	<ul style="list-style-type: none"> No exploration diamond drillholes have been completed in the 2018 reporting period. Historical exploration drillholes (prior to 2005) have been excluded from the Mineral Resource estimates. Mineralisation true widths are captured by interpreted mineralisation 3D wireframes. Drillholes are drilled to achieve intersections as close to orthogonal as possible.
Diagrams	 <p>The diagram is a geological cross-section titled "Section Through Ferrobamba". It shows a series of vertical drillhole locations from SW to NE. The lithology is color-coded: Skarn (green), Porphyry (red), Breccia (blue), Porphyry Low Grade (orange), Marble (cyan), and Dike (yellow). The section shows a complex geological structure with various rock units and features like dikes and breccias.</p> <p style="text-align: center;">Section Through Ferrobamba</p>

Assessment Criteria	Commentary
Section 2 Reporting of Exploration Results	
	 <p style="text-align: center;">Section Through Chalcobamba</p>  <p style="text-align: center;">Section Through Sulfobamba</p>
Balanced reporting	<ul style="list-style-type: none"> All drilling completed during the 2018 reporting period completed at Ferrobamba is infill in nature. Historical exploration drillholes (prior to 2005) have been excluded from the Mineral Resource estimates. A small number of holes were drilled at Chalcobamba for the purpose of hydrogeology, geotechnical and infill.
Other substantive exploration data	<ul style="list-style-type: none"> No substantive exploration diamond drillholes have been completed in the 2018 reporting period. Historical exploration drillholes (prior to 2005) have been excluded from the Mineral Resource estimates. Over the past 3 years, several orebody knowledge studies have been carried out including skarn zonation, vein densities and a large age dating program. Results from these studies are assisting with improving the understanding of the orebodies. Studies on clay and talc mapping have also commenced. This work will continue.
Further work	<ul style="list-style-type: none"> An ongoing program of regional and deposit scale mapping, cross sectional studies, infrared spectral analyses, isotopic and petrographic studies and soil sampling. A program of exploration assessment and targeting is currently underway to identify exploration options for the Las Bambas leases. Permitting for regional exploration drilling is underway. Ongoing infill programs are planned to increase deposit confidence.

Criteria	Status
Section 3 Estimating and Reporting of Mineral Resources	
Database integrity	<ul style="list-style-type: none"> • The following measures are in place to ensure database integrity: <ul style="list-style-type: none"> ○ All Las Bambas drillhole data is stored in an SQL database (acQuire) on the Las Bambas site server, which is regularly backed-up. ○ Geological logging is entered directly into laptop computers which are uploaded to the database. Prior to November 2014, diamond drillholes were logged on paper logging forms and transcribed into the database. From November 2015 logging was entered directly into a customised interface using portable tablet computers. ○ Assays are loaded directly into the database from digital files provided from the assay laboratory. • The measures described above ensure that transcription or data entry errors are minimised. <ul style="list-style-type: none"> • Data validation procedures include: <ul style="list-style-type: none"> ○ A database validation project was undertaken in early 2015 checking 5% of the assayed samples in the database against original laboratory certificates. No material issues were identified. ○ The database has internal validation processes which prevent invalid or unapproved records to be stored.
Site visits	<ul style="list-style-type: none"> • The Competent Person has undertaken numerous site visits to Las Bambas since acquisition. In the view of the Competent Person there are no material risks to the Mineral Resources based on observations of site practices. • Several site visits to the Ferrobamba area and the Chalcobamba area have been conducted but due to local community restrictions, the Competent Person has been unable to visit Sulfobamba to date. • The site previously employed a practice of 'double blind' sample randomisation at the laboratory. It essentially guarantees the secrecy of the results from the operating laboratory. It does however pose a minor risk of compromising sample provenance, although the risk is probably low. This practice has now ceased.
Geological interpretation	<ul style="list-style-type: none"> • There is good confidence on the geological continuity and interpretation of the Ferrobamba and Chalcobamba deposits. Confidence in the Sulfobamba deposit is considered moderate due to limited drilling. • The 2018 geological interpretation was undertaken on paper sections orientated perpendicular to the established structural trend of each deposit. Section spacing for the interpretations varied between deposits from 25m at Ferrobamba to 50m at Sulfobamba. The geological logging, assay data and surface mapping were used in the interpretation. The drilling and surface mapping were checked against each other to ensure they were concordant. • No alternative interpretations have been generated for the Las Bambas mineralisation and geology. • Exploratory data analysis (EDA) indicated that the lithological characterisation used for the 2010 geological interpretation were for the most part valid (with minor changes) and were applied for the 2018 modelling. Each lithological unit was modelled according to age, with the youngest modelled first. Structural considerations such as plunge of the units, folding and faults were taken into consideration (where

Criteria	Status
Section 3 Estimating and Reporting of Mineral Resources	
	<p>information existed). Orthogonal sections were also interpreted to ensure lithological continuity.</p> <ul style="list-style-type: none"> • Oxidation domains were produced for the Ferrobamba and Chalcobamba models. Oxidation domains were based on logged mineral species and acid soluble copper to total copper assay ratios. • Geological interpretations were then modelled as wireframe solids (based on the paper sections) and were peer reviewed within the Las Bambas Geology department and by the Competent Person. • Specific grade domains (copper and molybdenum) were not created, with the exception of interpreted, spatially coherent high-grade shoots at Sulfobamba. A domain cut-off of 0.8% Cu was used for the high-grade domain. The introduction of the high-grade domain was supported by EDA, contact plots, and change of support analysis.
Dimensions	<ul style="list-style-type: none"> • The Las Bambas Mineral Resources refers to three distinct deposits; each have been defined by drilling and estimated: <ul style="list-style-type: none"> ○ Ferrobamba Mineral Resources occupies a footprint which is 2500m N-S and 1800m E-W and over 900m vertically. ○ Chalcobamba Mineral Resources occupies a footprint of 2300m N-S and 1300m E-W and 800m vertically ○ Sulfobamba Mineral Resources is 1800m along strike in a NE direction and 850m across strike in a NW direction and 450m deep.
Estimation and modelling techniques	<ul style="list-style-type: none"> • Mineral Resources estimation for the three deposits has been undertaken in Vulcan (Maptek) mining software with the following key assumptions and parameters: <ul style="list-style-type: none"> ○ Ordinary Kriging interpolation has been applied for the estimation of Cu, Mo, Ag, Au, As, Ca, Mg, S, CuAS (acid soluble copper), CuCN (cyanide soluble copper) and density. This is considered appropriate for the estimation of Mineral Resources at Las Bambas. ○ The Ferrobamba, Chalcobamba and Sulfobamba block models utilised sub-blocking. Models were then regularised for use in mine planning purposes. ○ Extreme grade values were managed by upper grade capping based on statistical assessment evaluated for all variables and domains. Consideration was also given to the metal content above the top cap value. ○ All elements were estimated into lithology domains. At Ferrobamba five different orientation domains were identified in the skarn and were used in the interpolation. The boundaries between each orientation domain were treated as semi-soft boundaries. At Sulfobamba high-grade skarn shoots were identified and were used in the interpolation of copper only. The boundaries between the low and the high-grade skarn were treated as hard boundaries. ○ Data compositing for estimation was set to 4m, which matches two times the majority of drillhole sample lengths (2m), provides good definition across interpreted domains, and adequately accounts for bench height. CuAS and CuCN was composited to 8m which matches the majority of composite sample lengths. ○ Variogram analysis was updated for all deposits. Variogram analysis was undertaken in Vulcan software (Ferrobamba, Sulfobamba) and Supervisor (Snowden) software (Chalcobamba). ○ No assumptions have been made about the correlation between variables. All

Criteria	Status
Section 3 Estimating and Reporting of Mineral Resources	
	<p>variables are comparably informed and independently estimated.</p> <ul style="list-style-type: none"> ○ Interpolation was undertaken in three to four passes. • Check estimates using Discrete Gaussian change of support modelling have been performed on all models. Block model results are comparable with previous Mineral Resources estimations after changes due to drilling and re-modelling by the site. • Assumptions about the recovery of by-products is accounted in the net-smelter return (NSR) calculation which includes the recovery of Mo, Ag and Au along with the standard payable terms. • Arsenic is considered a deleterious element and has been estimated. Sulphur, calcium and magnesium are also estimated to assist in the determination of NAF (non-acid forming), PAF (potentially acid forming) and acid neutralising material. • Block sizes for all three deposits were selected based on Quantitative Kriging Neighbourhood Analysis (QKNA). The Ferrobamba block size was 20m x 20m x 15m with sub-blocks of 5m x 5m x 5m. Chalcobamba block size was set to 30m x 30m x 15m, with sub-blocks of 10m x 10m x 5m. The block size at Sulfobamba was set to 50m x 50m x 15m (sub-blocked to 25m x 25m x 7.5m) which roughly equates to the drill spacing. The search anisotropy employed was based on both the ranges of the variograms and the drill spacing. All models were regularised to 20m x 20m x 15m for use in Ore Reserve estimates. • The selective mining unit is assumed to be approximately 20m x 20m x 15m (x,y,z) which equates to the Ferrobamba block model block size. • Block model validation was conducted by the following processes – no material issues were identified: <ul style="list-style-type: none"> ○ Visual inspections for true fit for all wireframes (to check for correct placement of blocks and sub-blocks). ○ Visual comparison of block model grades against composite sample grades. ○ Global statistical comparison of the estimated block model grades against the declustered composite statistics. ○ Change of support analysis on major lithological domains. ○ Swath plots and drift plots were generated and checked for skarn and porphyry domains.
Moisture	<ul style="list-style-type: none"> • All tonnages are stated on a dry basis.
Cut-off parameters	<ul style="list-style-type: none"> • The Mineral Resources is reported above a range of cut-offs based on material type and ore body. The cut-off ranges from 0.16% Cu cut-off grade for hypogene material to 0.20% Cu for marble/calc-silicate hosted material and 0.21% Cu for breccia at Ferrobamba. Oxide material has been reported above a 1% Cu cut-off grade. The reported Mineral Resources have also been constrained within a US\$3.51/lb pit shell with revenue factor=1. • The reporting cut-off grade is in line with MMG’s policy on reporting of Mineral Resources which considers current and future mining and processing costs and satisfies the requirement for prospects for future economic extraction.
Mining factors or	<ul style="list-style-type: none"> • Mining of the Las Bambas deposits is undertaken by open pit mining method, which is expected to continue throughout the life of mine. Large scale mining equipment including 300 tonne trucks and 100 tonne face shovels will be used for material

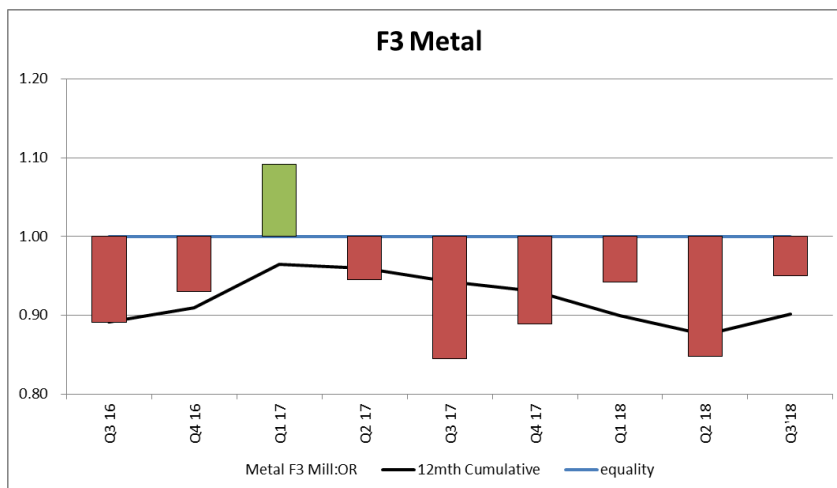
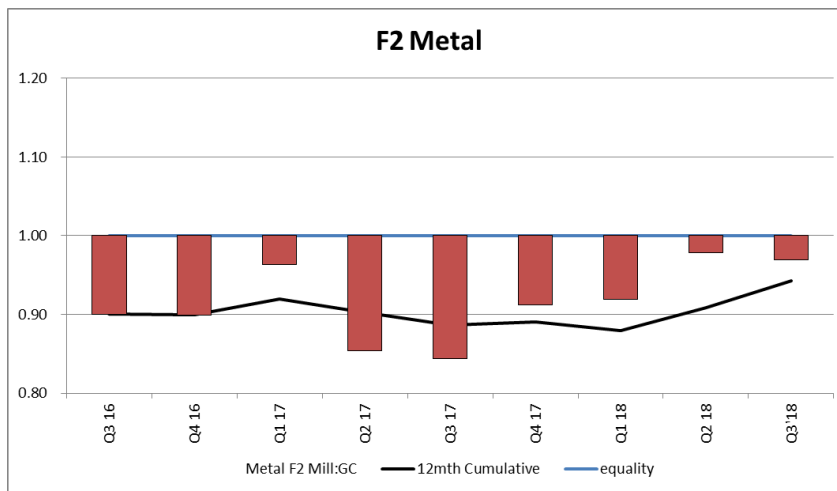
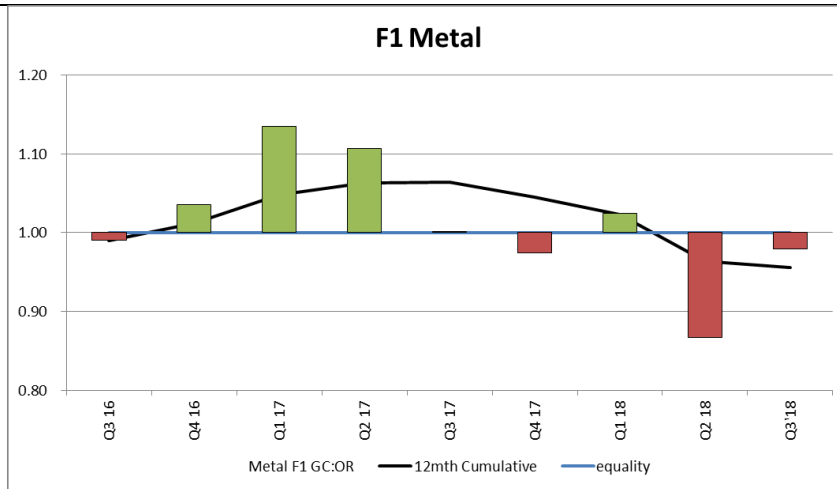
Criteria	Status
Section 3 Estimating and Reporting of Mineral Resources	
assumptions	<p>movement.</p> <ul style="list-style-type: none"> • During block regularisation, internal dilution is included to produce full block estimates. • Further information on mining factors is provided in Section 4 of this table. • No other mining factors have been applied to the Mineral Resources.
Metallurgical factors or assumptions.	<ul style="list-style-type: none"> • Currently the processing of oxide copper mineralisation has not been studied to pre-feasibility or feasibility study level. The inclusion of oxide copper Mineral Resources is based on the assumption that processing of very similar ores at Tintaya was completed successfully in the past where a head grade of greater than 1.5% Cu was required for favourable economics. This assumption has been used at this stage for the oxide copper mineralisation. • Sulphide and partially oxidised material is included in the Mineral Resources which is expected to be converted to Ore Reserves and treated in the onsite concentrator facilities. • No other metallurgical factors have been applied to the Mineral Resources.
Environmental factors or assumptions	<ul style="list-style-type: none"> • Environmental factors are considered in the Las Bambas life of asset work, which is updated annually and includes provision for mine closure. • Geochemical characterisation undertaken in 2007, 2009 and 2017 indicate the majority of the waste rock from Ferrobamba and Chalcobamba deposits to be Non-Acid Forming (NAF) and that no acid rock drainage from the waste rock dumps from these two pits should be expected. Waste rock samples from Sulfobamba were found to contain higher concentrations of sulphur and that 30% to 40% of waste rock could be Potentially Acid Forming (PAF). Suitable controls will be implemented for all PAF waste rock, including investigating opportunities for backfill into pit voids. Additional geochemical characterisation work is ongoing. • Tailings generated from processing of Ferrobamba and Chalcobamba were determined to be NAF. Geochemical characterisation of tailings generated from processing of Sulfobamba ores is currently under assessment, however for environmental assessment purposes it was assumed to have PAF behaviour. Current Life of Asset schedules have Ferrobamba tailings processing scheduled for several years after Sulfobamba tailings are processed. A closure plan was submitted and approved by the regulator in 2016 and describes the encapsulation method for Sulfobamba tailings. • Based on the current TSF design and the design assumptions for dry settled density and beach angle, the TSF at Las Bambas has a final capacity of 784Mt of tailings from processing 800Mt. Three studies have been conducted looking at increasing tailings storage capacity at Las Bambas: <ul style="list-style-type: none"> ○ Tailings characterisation test work to assess final settled density and beach slope in current TSF. ○ Options assessment to increase capacity at TSF currently under construction. ○ Pre-feasibility study for an additional TSF.
Bulk density	<ul style="list-style-type: none"> • Bulk density is determined using the Archimedes' principle (weight in air and weight in water method). Samples of 20cm in length are measured at a frequency of approximately one per core tray and based on geological domains. The density

Criteria	Status
Section 3 Estimating and Reporting of Mineral Resources	
	<p>measurements are considered representative of each lithology domain.</p> <ul style="list-style-type: none"> • Bulk density measurement occurs at the external, independent assay laboratory. The core is air dried and whole core is immersed in wax prior to bulk density determination to ensure that void spaces are accounted for. • Density values in the Mineral Resources models are estimated using Ordinary Kriging within the lithology domain shapes. Un-estimated blocks were assigned a density value based on an expected value of un-mineralised rock within each geological domain.
Classification	<ul style="list-style-type: none"> • Mineral Resource classifications used criteria that required a certain minimum number of drillholes. The spatial distribution of more than one drillhole ensures that any interpolated block was informed by sufficient samples to establish grade continuity. As well, drillhole spacing specific to rock type (skarn vs. porphyry) were used to classify each Mineral Resources category. • Drillhole spacing for classification were based on an internal Ferrobamba drillhole spacing study undertaken in 2015. Results from the study indicate: <ul style="list-style-type: none"> ○ Measured Mineral Resources: 25m x 25m drillhole spacing in the skarn, 50m x 50m drillhole spacing for the porphyry. ○ Indicated Mineral Resources: 50m x 50m drillhole spacing in the skarn, 100m x 100m drillhole spacing for the porphyry. ○ Inferred Mineral Resources are generally defined as twice the spacing of Indicated Mineral Resources with regard to each rock type. • Only copper estimated values were used for classification. Estimation confidence of deleterious elements such as arsenic was not considered for classification purposes. • The Mineral Resource classification applied appropriately reflects the Competent Person's view of the deposit.
Audits or reviews	<ul style="list-style-type: none"> • Historical models have all been subject to a series of internal and external reviews during their history of development. The recommendations of each review have been implemented at the next update of the relevant Mineral Resource estimates. • Several extensive reviews were undertaken as part of the MMG due diligence process for the purchase of Las Bambas. These reviews included work done by Runge Pincock Minarco (RPM), which resulted in the published Competent Person report in 2014. In addition significant review work was carried out by AMEC. No fatal flaws were detected in these reviews and all recommendations were considered and addressed in the 2015 Mineral Resources update and all subsequent updates. • A self-assessment of all 2018 Mineral Resource modelling was completed by the Competent Person using a standardised MMG template. No fatal flaws were detected in the review. Areas previously identified for improvement have been addressed and include: <ul style="list-style-type: none"> ○ Mineral Resource classification for the Ferrobamba block model uses a wireframe shape to constrain the final Mineral Resource category. ○ Acid soluble copper results are used to model an oxidation type domain. This is in turn used to constrain the acid soluble copper estimate. ○ An external third party audit was undertaken in 2018 on the 2017 Mineral Resource by AMC Consultants

Criteria	Status																																																															
Section 3 Estimating and Reporting of Mineral Resources																																																																
Discussion of relative accuracy / confidence	<ul style="list-style-type: none"> There is high geological confidence of the spatial location, continuity and estimated grades of the modelled lithologies within the Mineral Resources. Minor, local variations are expected to occur on a sub-25m scale that is not detectable by the current drill spacing. Global declustered statistics of the composite databases on a domain basis were compared against the block model. Block model estimates were within 10% of the composite database. Local swath plots were undertaken for each deposit. All plots showed appropriate smoothing of composite samples with respect to estimated block grades. The Las Bambas Mineral Resource estimates are considered suitable for Ore Reserve estimation and mine design purposes. The Mineral Resources model was evaluated using the discrete Gaussian change of support method for copper in most domains. Based on the grade tonnage curves generated, the Mineral Resources model should be a reasonable predictor of tonnes and grade selected during mining. Reconciliation of the last 12 months of production indicates that the mine planning block model has under-called the ore control model (F1) by 4% for copper metal. This comprises a 9% under-call of grade and a 12% over-call of tonnage. <table border="1" data-bbox="491 981 1295 1361" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th>2018 Block Model</th> <th>Factor</th> <th>Grade</th> <th>Tonnes</th> <th>Metal</th> </tr> </thead> <tbody> <tr> <td rowspan="3">Year to June 2017</td> <td>F1</td> <td>1.13</td> <td>0.94</td> <td>1.06</td> </tr> <tr> <td>F2*</td> <td>1.00</td> <td>0.90</td> <td>0.90</td> </tr> <tr> <td>F3*</td> <td>1.14</td> <td>0.84</td> <td>0.96</td> </tr> <tr> <td rowspan="3">Year to June 2018</td> <td>F1</td> <td>1.09</td> <td>0.88</td> <td>0.96</td> </tr> <tr> <td>F2*</td> <td>0.95</td> <td>0.95</td> <td>0.91</td> </tr> <tr> <td>F3*</td> <td>1.04</td> <td>0.84</td> <td>0.88</td> </tr> <tr> <td rowspan="3">Jul16 to Jun'18</td> <td>F1</td> <td>1.11</td> <td>0.91</td> <td>1.01</td> </tr> <tr> <td>F2*</td> <td>0.98</td> <td>0.92</td> <td>0.91</td> </tr> <tr> <td>F3*</td> <td>1.09</td> <td>0.84</td> <td>0.92</td> </tr> <tr> <td rowspan="3">All</td> <td>F1</td> <td>1.10</td> <td>0.92</td> <td>1.01</td> </tr> <tr> <td>F2*</td> <td>0.98</td> <td>0.93</td> <td>0.91</td> </tr> <tr> <td>F3*</td> <td>1.07</td> <td>0.86</td> <td>0.92</td> </tr> </tbody> </table> <p data-bbox="502 1364 1129 1391" style="text-align: center;">* includes +3% adjustment to Mill grade due to known assay bias</p> <table border="1" data-bbox="491 1391 1209 1480" style="margin-left: auto; margin-right: auto;"> <tbody> <tr> <td>F1</td> <td>Grade Control / Ore Reserve</td> </tr> <tr> <td>F2</td> <td>Mill / Ore Control</td> </tr> <tr> <td>F3</td> <td>Mill / Ore Reserve</td> </tr> </tbody> </table> <ul style="list-style-type: none"> The F3 (Mill / Reserve) reconciliation indicates that the Reserve model has over-called metal by 12% for the year ended June 2018. This is a significant departure from the reconciliation observations at the end of June 2017 which showed a 4% metal overcall when comparing the 2018 block model. Further analysis using the F2 reconciliation factor (Mill / Grade Control) for the year ending June 2018 shows that metal sent to the mill is 9% lower than estimated by the mine. 	2018 Block Model	Factor	Grade	Tonnes	Metal	Year to June 2017	F1	1.13	0.94	1.06	F2*	1.00	0.90	0.90	F3*	1.14	0.84	0.96	Year to June 2018	F1	1.09	0.88	0.96	F2*	0.95	0.95	0.91	F3*	1.04	0.84	0.88	Jul16 to Jun'18	F1	1.11	0.91	1.01	F2*	0.98	0.92	0.91	F3*	1.09	0.84	0.92	All	F1	1.10	0.92	1.01	F2*	0.98	0.93	0.91	F3*	1.07	0.86	0.92	F1	Grade Control / Ore Reserve	F2	Mill / Ore Control	F3	Mill / Ore Reserve
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Criteria	Status
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Section 3 Estimating and Reporting of Mineral Resources



- The Competent Person considers the accuracy and confidence of this Mineral Resource estimate is considered sufficient quality for global Mineral Resource and Ore Reserve reporting by the Competent Person.

3.2.3 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Mineral Resources statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Rex Berthelsen, confirm that I am the Competent Person for the Las Bambas Mineral Resources section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a Fellow of The Australasian Institute of Mining and Metallurgy
- I have reviewed the relevant Las Bambas Mineral Resources section of this Report to which this Consent Statement applies.

I am a full time employee of MMG Ltd. at the time of the estimation.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest.

I verify that the Las Bambas Mineral Resources section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Las Bambas Mineral Resources.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Las Bambas Mineral Resources - I consent to the release of the 2018 Mineral Resources and Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resources and Ore Reserves Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

5/12/2018

Rex Berthelsen HonFAusIMM(CP) (#109561)

Date:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resources and Ore Reserves Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Manfred Wimberger
Winchelsea, VIC

Signature of Witness:

Witness Name and Residence: (e.g. town/suburb)

3.3 Ore Reserves – Las Bambas

3.3.1 Results

The 2018 Las Bambas Ore Reserves are summarised in Table 5. All data reported here is on a 100% asset basis. MMG's attributable interest in Las Bambas is 62.5%.

Table 5 2018 Las Bambas Ore Reserves tonnage and grade (as at 30 June 2018)

Las Bambas Ore Reserves									
	Tonnes	Copper	Silver	Gold	Mo	Contained Metal			
	(Mt)	(% Cu)	(g/t Ag)	(g/t Au)	(ppm)	Copper (kt)	Silver (Moz)	Gold (Moz)	Mo (kt)
Ferrobamba Primary Copper¹									
Proved ⁴	504	0.62	2.9	0.05	197	3,133	46	0.9	99
Probable	287	0.68	3.7	0.07	179	1,962	34	0.6	51
Total	791	0.64	3.2	0.06	191	5,096	80	1.5	151
Chalcobamba Primary Copper²									
Proved	56	0.54	1.8	0.02	144	302	3	0.04	8
Probable	139	0.72	2.7	0.03	135	995	12	0.15	19
Total	195	0.67	2.5	0.03	137	1,298	16	0.19	27
Sulfobamba Primary Copper³									
Probable	59	0.81	5.9	0.03	161	479	11	0.1	10
Total	59	0.81	5.9	0.03	161	479	11	0.1	10
Primary Copper Stockpiles									
Proved	2.3	0.41	1.7	-	158	9.5	0.13	-	0.36
Total	2.3	0.41	1.7	-	158	9.5	0.13	-	0.36
Total Contained Metal						6,882	107	1.7	187

1 0.19% to 0.26% Cu cut-off grade based on rock type and recovery

2 0.21% to 0.28% Cu cut-off grade based on rock type and recovery

3 0.24% to 0.28% Cu cut-off grade based on rock type and recovery

Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors.

Contained metal does not imply recoverable metal

3.3.2 Ore Reserves JORC 2012 Assessment and Reporting Criteria

The following information provided in Table 6 complies with the 2012 JORC Code requirements specified by "Table-1 Section 4" of the Code. Each of the items in this table has been summarised as the basis for the assessment of overall Ore Reserves risk in the table below, with each of the risks related to confidence and/or accuracy of the various inputs into the Ore Reserves qualitatively assessed.

Table 6 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Las Bambas Ore Reserve 2018

Assessment Criteria	Commentary																								
Mineral Resource estimates for conversion to Ore Reserves	<ul style="list-style-type: none"> • Mineral Resource block models have been provided by the Mineral Resource Competent Person. The block models contain descriptions for lithology, Mineral Resources Classification, mineralisation, ore type, and other variables described in model release memorandums. These block models were used for the pit optimisation purpose using reasonable assumptions for cost and metal prices, GEOVIA Whittle was the software package used for this purpose. <table border="1" data-bbox="416 837 1401 1144"> <thead> <tr> <th data-bbox="416 837 644 882">MR block models</th> <th data-bbox="644 837 890 882">Ferrobamba</th> <th data-bbox="890 837 1136 882">Chalcobamba</th> <th data-bbox="1136 837 1401 882">Sulfobamba</th> </tr> </thead> <tbody> <tr> <td data-bbox="416 882 644 958">Completed by</td> <td data-bbox="644 882 890 958">Rex Berthelsen</td> <td data-bbox="890 882 1136 958">Rex Berthelsen</td> <td data-bbox="1136 882 1401 958">Anna Lewin / Rex Berthelsen</td> </tr> <tr> <td data-bbox="416 958 644 1003">Memorandum date</td> <td data-bbox="644 958 890 1003">11 April 2018</td> <td data-bbox="890 958 1136 1003">21 April 2017</td> <td data-bbox="1136 958 1401 1003">31 May 2017</td> </tr> <tr> <td data-bbox="416 1003 644 1057">Block model file</td> <td data-bbox="644 1003 890 1057">lb_fe_mor_1803.bmf</td> <td data-bbox="890 1003 1136 1057">lb_ch_mor_1701 v5.bmf</td> <td data-bbox="1136 1003 1401 1057">lb_sb_1704_mor_v2.asc</td> </tr> <tr> <td data-bbox="416 1057 644 1102">Block size (m)</td> <td data-bbox="644 1057 890 1102">20 x 20 x 15</td> <td data-bbox="890 1057 1136 1102">20 x 20 x 15</td> <td data-bbox="1136 1057 1401 1102">20 x 20 x 15</td> </tr> <tr> <td data-bbox="416 1102 644 1144">Model rotation</td> <td data-bbox="644 1102 890 1144">35°</td> <td data-bbox="890 1102 1136 1144">0°</td> <td data-bbox="1136 1102 1401 1144">0°</td> </tr> </tbody> </table> <ul style="list-style-type: none"> • The Measured and Indicated Mineral Resources quantities are inclusive and not additional to the Ore Reserves reported. 	MR block models	Ferrobamba	Chalcobamba	Sulfobamba	Completed by	Rex Berthelsen	Rex Berthelsen	Anna Lewin / Rex Berthelsen	Memorandum date	11 April 2018	21 April 2017	31 May 2017	Block model file	lb_fe_mor_1803.bmf	lb_ch_mor_1701 v5.bmf	lb_sb_1704_mor_v2.asc	Block size (m)	20 x 20 x 15	20 x 20 x 15	20 x 20 x 15	Model rotation	35°	0°	0°
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Site visits	<ul style="list-style-type: none"> • The Competent Person has visited the Las Bambas site twice in the past year. Each visit consisted of discussions with relevant people associated with Ore Reserve modifying factors including Geology, Grade Control, Geotechnical, Mine Planning and Mining Operations, Metallurgy, Tailings and Waste Storage, and Environmental Areas. The outcomes from the visits have included reaching a common understanding in those areas, in addition to achieving other specific purposes of each trip. Site visits were also carried out by contributing experts listed in the expert input table at the end of this document. 																								
Study status	<ul style="list-style-type: none"> • The Las Bambas Ore Reserve estimates were prepared on the basis of Feasibility and Pre-Feasibility level studies that include the following: <ul style="list-style-type: none"> ○ Bechtel Feasibility Study 2010; and ○ Las Bambas Mine Site 3 TSF Prefeasibility Study, MWH, 2015. • Additional work/studies include: <ul style="list-style-type: none"> ○ Glencore Mineral Resources and Ore Reserves Report 2013; ○ Audit of Las Bambas Ore Reserves 2013, by Mintec, Inc in October 2013; ○ MMG Competent Person Report prepared by Runge Pincock Minarco (RPM), June 2014; ○ MMG Las Bambas cut-Off Grade Report 2018; ○ Rock Mass Model Update by Golder (2017); ○ Structural Geology Mode Update by JFSGC (2017); ○ Hydrogeology Model Update by Itasca (2018); ○ Geotechnical guidance by Piteau (2009-2010); 																								

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	<ul style="list-style-type: none"> ○ Geotechnical work conducted by site personnel and Itasca, 2015 - 2017; ○ Sulfobamba Metallurgy Testing, 2015; ○ Tailings Storage Facility – Initial review of options to extend filing life, ATCW, 2015; ○ Technical review of future TSF, Khlon Crippen Berger, 2016; and ○ Conceptual Development of New Tailings Storage Facility, Ausenco 2018. ● 2018 Life of Asset (LoA) Low Case was produced as part of the MMG planning cycle demonstrates this is technically achievable and economically viable, and that material Modifying Factors have been considered. 																																																												
Cut-off parameters	<ul style="list-style-type: none"> ● MMG Board approved metal prices for the cut-off calculation have been provided by MMG Group Finance in accordance with the MMG MROR Standard. ● Costs were estimated based on information provided by the Las Bambas Finance Department. ● The breakeven cut-off (BCoG) 2018 has been calculated with updated metal prices and costs, and is applied to the Cut%. (Source: 2018 Las Bambas CoG Report). ● Cut-off grade has been determined for each ore-type within each deposit: <p>Cut-off grades by ore-type for Ferrobamba:</p> <table border="1" data-bbox="416 1081 1337 1189"> <thead> <tr> <th rowspan="2">COG Component</th> <th colspan="6">Ferrobamba by Ore Type</th> </tr> <tr> <th>FSSL</th> <th>FSSM</th> <th>FPSL</th> <th>FPSM</th> <th>FMSL</th> <th>FBRE</th> </tr> </thead> <tbody> <tr> <td>BCoG_{inpit}</td> <td>0.19%</td> <td>0.22%</td> <td>0.19%</td> <td>0.24%</td> <td>0.24%</td> <td>0.26%</td> </tr> </tbody> </table> <p>Cut-off grades by ore-type for Chalcobamba:</p> <table border="1" data-bbox="416 1240 1422 1348"> <thead> <tr> <th rowspan="2">COG Component</th> <th colspan="7">Chalcobamba by ORE TYPE</th> </tr> <tr> <th>CSSL</th> <th>CSSM</th> <th>CSML</th> <th>CSMM</th> <th>CPSL</th> <th>CPSM</th> <th>CBRE</th> </tr> </thead> <tbody> <tr> <td>BCoG_{inpit}</td> <td>0.21%</td> <td>0.24%</td> <td>0.21%</td> <td>0.22%</td> <td>0.21%</td> <td>0.26%</td> <td>0.28%</td> </tr> </tbody> </table> <p>Cut-off grades by ore-type for Sulfobamba:</p> <table border="1" data-bbox="416 1400 1305 1507"> <thead> <tr> <th rowspan="2">COG Component</th> <th colspan="5">Sulfobamba by ORE TYPE</th> </tr> <tr> <th>SSSL</th> <th>SSSM</th> <th>SPSL</th> <th>SPSM</th> <th>SBRE</th> </tr> </thead> <tbody> <tr> <td>BCoG_{inpit}</td> <td>0.24%</td> <td>0.28%</td> <td>0.24%</td> <td>0.27%</td> <td>0.24%</td> </tr> </tbody> </table>	COG Component	Ferrobamba by Ore Type						FSSL	FSSM	FPSL	FPSM	FMSL	FBRE	BCoG _{inpit}	0.19%	0.22%	0.19%	0.24%	0.24%	0.26%	COG Component	Chalcobamba by ORE TYPE							CSSL	CSSM	CSML	CSMM	CPSL	CPSM	CBRE	BCoG _{inpit}	0.21%	0.24%	0.21%	0.22%	0.21%	0.26%	0.28%	COG Component	Sulfobamba by ORE TYPE					SSSL	SSSM	SPSL	SPSM	SBRE	BCoG _{inpit}	0.24%	0.28%	0.24%	0.27%	0.24%
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Mining factors or assumptions	<ul style="list-style-type: none"> ● The method of Ore Reserves estimation included pit optimisation, final pit and phase designs, consideration of mining schedule and all modifying factors. Addition information is provided in this section. ● The mining method selected for the Las Bambas operation is open cut mining, which enables bulk mining of these large low to moderate grade mineral deposits that are outcropping to sub-cropping. Three deposits, Ferrobamba, Chalcobamba and Sulfobamba are each mined in separate open pits. Mining is by way of conventional truck and shovel operation. This method and selected mining equipment are appropriate for these deposits. ● The geotechnical recommendations were provided by the Geotechnical & Hydrogeology team at Las Bambas in coordination with MMG Group Technical Services. These recommendations are based on studies performed by Piteau (2009-2010), site personnel and Itasca (2015 to 2017). The pits are sectored by structural zones and geotechnical sectors. Mine designs slope angles are shown below in the corresponding tables. 																																																												

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	<ul style="list-style-type: none"> The geotechnical parameters used for the slopes are as follows: <p>Geotechnical recommendations for Ferrobamba</p> <table border="1" data-bbox="427 416 1331 1084"> <thead> <tr> <th>Design Sector</th> <th>Level</th> <th>Bench height (m)</th> <th>Bench Face Angle (BFA)</th> <th>Berm Width (m)</th> <th>Inter Ramp Angle (degrees)</th> <th>Interamp Height (m)</th> <th>Decoupling Berm width (m)</th> </tr> </thead> <tbody> <tr> <td>SW1 SW2 SO1 (PF1)</td> <td>Below 3720mRL</td> <td>15</td> <td>70</td> <td>9.7</td> <td>44.7</td> <td>120</td> <td>35</td> </tr> <tr> <td>SO2 (PF2)</td> <td>Below 3675mRL</td> <td>15</td> <td>70</td> <td>8.5</td> <td>47.1</td> <td>120</td> <td>35</td> </tr> <tr> <td>SE1 (PF3)</td> <td>Below 3960mRL</td> <td>30</td> <td>70</td> <td>14</td> <td>50.3</td> <td>120</td> <td>35</td> </tr> <tr> <td>EA1 (PF4)</td> <td>4020 - 3810mRL¹ Below 3810mRL</td> <td>30</td> <td>70</td> <td>17.1</td> <td>47</td> <td>210</td> <td>35</td> </tr> <tr> <td>CE1 (PF5)</td> <td>-</td> <td>30</td> <td>70</td> <td>11.2</td> <td>53.6</td> <td>210</td> <td>35</td> </tr> <tr> <td>N NE1 and NE2 (PF6)</td> <td>3900 - 3870mRL² Below 3975mRL</td> <td>30</td> <td>70</td> <td>15</td> <td>49.2</td> <td>210</td> <td>35</td> </tr> <tr> <td>NW1 and NW2 (PF7)</td> <td>3960 - 3870mRL² Below 3975mRL</td> <td>30</td> <td>70</td> <td>15</td> <td>49.2</td> <td>210</td> <td>35</td> </tr> </tbody> </table> <p>Geotechnical recommendations for Chalcobamba:</p> <table border="1" data-bbox="416 1162 1426 1518"> <thead> <tr> <th>Sector</th> <th>Level (m)</th> <th>BFA (°)</th> <th>H (BFA)</th> <th>Catch Bench</th> <th>IRA (°)</th> <th>Height Zone (m)</th> <th>Decoupling Height</th> <th>Decoupling Width</th> <th>Decoupling Number</th> <th>Angle By Zone</th> <th>Angle +decoupling</th> <th>OA (°)</th> <th>Total Height (m)</th> <th>Bench (number)</th> </tr> </thead> <tbody> <tr> <td rowspan="2">CH-S2</td> <td>4330-4450</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>120</td> <td>90</td> <td>35</td> <td>1</td> <td>45.7</td> <td>50.3</td> <td>44.1</td> <td>210</td> <td>8</td> </tr> <tr> <td>4450-4540</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>90</td> <td></td> <td></td> <td></td> <td>42.1</td> <td>47.7</td> <td></td> <td>6</td> <td>6</td> </tr> <tr> <td rowspan="2">CH-SE</td> <td>4255-4465</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>210</td> <td>90</td> <td>35</td> <td>1</td> <td>46.7</td> <td>49.3</td> <td>45.2</td> <td>300</td> <td>14</td> </tr> <tr> <td>4465-4555</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>90</td> <td></td> <td></td> <td></td> <td>42.1</td> <td>47.7</td> <td></td> <td>6</td> <td>6</td> </tr> <tr> <td rowspan="2">CH-E</td> <td>4165-4435</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>270</td> <td>105</td> <td>35</td> <td>2</td> <td>44.1</td> <td>45.9</td> <td>43.6</td> <td>375</td> <td>18</td> </tr> <tr> <td>4435-4540</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>105</td> <td></td> <td></td> <td></td> <td>42.5</td> <td>47.3</td> <td></td> <td>7</td> <td>7</td> </tr> <tr> <td rowspan="2">CH-N</td> <td>4165-4360</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>195</td> <td>105</td> <td>35</td> <td>1</td> <td>46.6</td> <td>49.4</td> <td>45.1</td> <td>300</td> <td>13</td> </tr> <tr> <td>4360-4465</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>105</td> <td></td> <td></td> <td></td> <td>42.5</td> <td>47.3</td> <td></td> <td>7</td> <td>7</td> </tr> <tr> <td rowspan="2">CH-NW</td> <td>4165-4285</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>120</td> <td>90</td> <td>35</td> <td>1</td> <td>45.7</td> <td>50.3</td> <td>44.1</td> <td>210</td> <td>8</td> </tr> <tr> <td>4285-4375</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>90</td> <td></td> <td></td> <td></td> <td>42.1</td> <td>47.7</td> <td></td> <td>6</td> <td>6</td> </tr> <tr> <td rowspan="2">CH-W</td> <td>4165-4330</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>165</td> <td>90</td> <td>35</td> <td>1</td> <td>46.3</td> <td>49.7</td> <td>44.8</td> <td>255</td> <td>11</td> </tr> <tr> <td>4330-4420</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>90</td> <td></td> <td></td> <td></td> <td>42.1</td> <td>47.7</td> <td></td> <td>6</td> <td>6</td> </tr> <tr> <td rowspan="2">CH-SW</td> <td>4315-4435</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>120</td> <td>90</td> <td>35</td> <td>1</td> <td>45.7</td> <td>50.3</td> <td>44.1</td> <td>210</td> <td>8</td> </tr> <tr> <td>4435-4525</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>90</td> <td></td> <td></td> <td></td> <td>42.1</td> <td>47.7</td> <td></td> <td>6</td> <td>6</td> </tr> <tr> <td rowspan="2">CH-S1</td> <td>4315-4450</td> <td>70</td> <td>15</td> <td>8</td> <td>48.1</td> <td>135</td> <td>90</td> <td>35</td> <td>1</td> <td>45.9</td> <td>50.0</td> <td>44.4</td> <td>225</td> <td>9</td> </tr> <tr> <td>4450-4540</td> <td>65</td> <td>15</td> <td>8</td> <td>45</td> <td>90</td> <td></td> <td></td> <td></td> <td>42.1</td> <td>47.7</td> <td></td> <td>6</td> <td>6</td> </tr> </tbody> </table> <p>Geotechnical recommendations for Sulfbamba</p> <table border="1" data-bbox="416 1588 1426 1881"> <thead> <tr> <th>Sector</th> <th>Zone</th> <th>C. Lito</th> <th>Level (m)</th> <th>BFA (°)</th> <th>H (BFA)</th> <th>Catch bench</th> <th>IRA (°)</th> <th>Height Zone (m)</th> <th>Decoupling Height</th> <th>Decoupling Width</th> <th>Decoupling Number</th> <th>Angle by zone</th> <th>OA (°)</th> <th>Total Height (m)</th> <th>Bench (number)</th> </tr> </thead> <tbody> <tr> <td rowspan="2">SU-S</td> <td>Sup.</td> <td>71</td> <td>4565 - 4475</td> <td>65</td> <td>15</td> <td>8</td> <td>42</td> <td>90</td> <td>150</td> <td>35</td> <td>1</td> <td>38</td> <td>41</td> <td>255</td> <td>6</td> </tr> <tr> <td>Inf.</td> <td>40, 47</td> <td>4475 - 4310</td> <td>70</td> <td>15</td> <td>8</td> <td>45</td> <td>165</td> <td></td> <td></td> <td></td> <td>42</td> <td></td> <td>11</td> <td>11</td> </tr> <tr> <td rowspan="2">SU-E</td> <td>Sup.</td> <td>71</td> <td>4565 - 4445</td> <td>65</td> <td>15</td> <td>8</td> <td>42</td> <td>120</td> <td>150</td> <td>35</td> <td>1</td> <td>38</td> <td>42</td> <td>255</td> <td>8</td> </tr> <tr> <td>Inf.</td> <td>40, 47</td> <td>4445 - 4310</td> <td>70</td> <td>15</td> <td>8</td> <td>45</td> <td>135</td> <td></td> <td></td> <td></td> <td>42</td> <td></td> <td>9</td> <td>9</td> </tr> <tr> <td rowspan="2">SU-NE</td> <td>Sup.</td> <td>71</td> <td>4420 - 4345</td> <td>65</td> <td>15</td> <td>8</td> <td>42</td> <td>165</td> <td>150</td> <td>35</td> <td>1</td> <td>38</td> <td>42</td> <td>255</td> <td>11</td> </tr> <tr> <td>Inf.</td> <td>40</td> <td>4345 - 4165</td> <td>70</td> <td>15</td> <td>8</td> <td>45</td> <td>90</td> <td></td> <td></td> <td></td> <td>42</td> <td></td> <td>6</td> <td>6</td> </tr> <tr> <td>SU-N</td> <td>Sup.</td> <td>81</td> <td>4460 - 4310</td> <td>65</td> <td>15</td> <td>8</td> <td>44</td> <td>150</td> <td>150</td> <td></td> <td></td> <td>45</td> <td>45</td> <td>150</td> <td>10</td> </tr> <tr> <td rowspan="2">SU-W</td> <td>Sup.</td> <td>40</td> <td>4565 - 4505</td> <td>65</td> <td>15</td> <td>8</td> <td>42</td> <td>60</td> <td>150</td> <td>35</td> <td>1</td> <td>38</td> <td>41</td> <td>195</td> <td>4</td> </tr> <tr> <td>Inf.</td> <td>80, 81</td> <td>4505 - 4370</td> <td>70</td> <td>15</td> <td>8</td> <td>44</td> <td>135</td> <td></td> <td></td> <td></td> <td>41</td> <td></td> <td>9</td> <td>9</td> </tr> </tbody> </table> <ul style="list-style-type: none"> An extensive program of additional geotechnical data collection and analysis is currently being planned to commence in September 2018 for Ferrobamba and Chalcobamba. This will improve confidence in the slope design guidance at both of these deposits. The bulk of the findings from the data collection and analysis will be available for inclusion in the 2020 Ore Reserve slope design 	Design Sector	Level	Bench height (m)	Bench Face Angle (BFA)	Berm Width (m)	Inter Ramp Angle (degrees)	Interamp Height (m)	Decoupling Berm width (m)	SW1 SW2 SO1 (PF1)	Below 3720mRL	15	70	9.7	44.7	120	35	SO2 (PF2)	Below 3675mRL	15	70	8.5	47.1	120	35	SE1 (PF3)	Below 3960mRL	30	70	14	50.3	120	35	EA1 (PF4)	4020 - 3810mRL ¹ Below 3810mRL	30	70	17.1	47	210	35	CE1 (PF5)	-	30	70	11.2	53.6	210	35	N NE1 and NE2 (PF6)	3900 - 3870mRL ² Below 3975mRL	30	70	15	49.2	210	35	NW1 and NW2 (PF7)	3960 - 3870mRL ² Below 3975mRL	30	70	15	49.2	210	35	Sector	Level (m)	BFA (°)	H (BFA)	Catch Bench	IRA (°)	Height Zone (m)	Decoupling Height	Decoupling Width	Decoupling Number	Angle By Zone	Angle +decoupling	OA (°)	Total Height (m)	Bench (number)	CH-S2	4330-4450	70	15	8	48.1	120	90	35	1	45.7	50.3	44.1	210	8	4450-4540	65	15	8	45	90				42.1	47.7		6	6	CH-SE	4255-4465	70	15	8	48.1	210	90	35	1	46.7	49.3	45.2	300	14	4465-4555	65	15	8	45	90				42.1	47.7		6	6	CH-E	4165-4435	70	15	8	48.1	270	105	35	2	44.1	45.9	43.6	375	18	4435-4540	65	15	8	45	105				42.5	47.3		7	7	CH-N	4165-4360	70	15	8	48.1	195	105	35	1	46.6	49.4	45.1	300	13	4360-4465	65	15	8	45	105				42.5	47.3		7	7	CH-NW	4165-4285	70	15	8	48.1	120	90	35	1	45.7	50.3	44.1	210	8	4285-4375	65	15	8	45	90				42.1	47.7		6	6	CH-W	4165-4330	70	15	8	48.1	165	90	35	1	46.3	49.7	44.8	255	11	4330-4420	65	15	8	45	90				42.1	47.7		6	6	CH-SW	4315-4435	70	15	8	48.1	120	90	35	1	45.7	50.3	44.1	210	8	4435-4525	65	15	8	45	90				42.1	47.7		6	6	CH-S1	4315-4450	70	15	8	48.1	135	90	35	1	45.9	50.0	44.4	225	9	4450-4540	65	15	8	45	90				42.1	47.7		6	6	Sector	Zone	C. Lito	Level (m)	BFA (°)	H (BFA)	Catch bench	IRA (°)	Height Zone (m)	Decoupling Height	Decoupling Width	Decoupling Number	Angle by zone	OA (°)	Total Height (m)	Bench (number)	SU-S	Sup.	71	4565 - 4475	65	15	8	42	90	150	35	1	38	41	255	6	Inf.	40, 47	4475 - 4310	70	15	8	45	165				42		11	11	SU-E	Sup.	71	4565 - 4445	65	15	8	42	120	150	35	1	38	42	255	8	Inf.	40, 47	4445 - 4310	70	15	8	45	135				42		9	9	SU-NE	Sup.	71	4420 - 4345	65	15	8	42	165	150	35	1	38	42	255	11	Inf.	40	4345 - 4165	70	15	8	45	90				42		6	6	SU-N	Sup.	81	4460 - 4310	65	15	8	44	150	150			45	45	150	10	SU-W	Sup.	40	4565 - 4505	65	15	8	42	60	150	35	1	38	41	195	4	Inf.	80, 81	4505 - 4370	70	15	8	44	135				41		9	9
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Assessment Criteria	Commentary
	<p>guidance.</p> <ul style="list-style-type: none"> • The 2018 Mineral Resources model for Ferrobamba and Chalcobamba have been used for the updated 2018 Ore Reserves. The Mineral Resources models for Chalcobamba and Sulfobamba remained the same as 2017. All models were regularised to 20m x 20m x 15m. <p>The pit optimisation was developed for the three open pits based on the 2018 Mineral Resource block models, the strategy for the final pit selection was based on the NPV by pit shell at revenue factor 1 (RF=1.0). RF 1.0 pit shell is used in all assets across the MMG Group. Final pit designs that incorporate more practical mining considerations were carried out using those optimisation shells.</p> <ul style="list-style-type: none"> • Dilution and recovery have been accounted for in the regularised block model used for the Ore Reserves estimate. Hence, the Ore Reserves estimate has applied no further factoring. • The reconciliation result has indicated that there could be up to 6% variance between metal contained in reserve model and metal contained in mill feed that is attributable to ore loss in the mining process. This loss is due to a range of factors including high powder factors to increase fragmentation in 2017, limited mining fronts as the pit is opened up, the associated need to blast ore and waste together and blast movement. A program to address these issues is in progress and key improvement milestones have been set. These programs include improving blasting practices/designs, monitoring blast movement, accurate positioning of shovels, better design of ore polygons and other remediations. • Some improvement in the reconciliation between grade control model and mill feed has been demonstrated since blasting practices have been refined. As a result, both the metal and ore loss indicator have shown a trend improvement closer to 100% mining recovery. However, the assumption of 100% recovery will need to be shown to be sustainable, once the abovementioned improvements have been fully implemented and assessed. • Additional studies for mining dilution and recovery will be undertaken to evaluate the effectiveness of the whole program and when more reconciliation data is available. • Since commercial production commenced, the Ore Reserve has remained well within the acceptable estimation tolerance of +/- 15% for Proven Ore Reserve over a single quarter. • In the pit, the minimum mining width is 70m; the Small Mining Unit (SMU) has been set at 20m x 20m x 15m. • Inferred Mineral Resource material has not been included in the pit optimisation or in the Ore Reserves estimates. • The main mining infrastructure includes; crusher, overland conveyor, tailings and waste storage facilities, stockpiles, roadways/ramps, workshops and so forth. • All infrastructure requirements are established for Ferrobamba. Further capital investment is required for infrastructure to support the needs of Chalcobamba and Sulfobamba.

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> The required infrastructure for Chalcobamba pit have been identified and included in the current approved Environment Impact Assessment (EIA), with 50% of the north waste dump not located within the property boundary. Another location that is fully within the property boundary has been identified and used in the LoA planning; however, it is yet to be evaluated by environmental/legal/exploration areas. In 3rd EIA amendment approval drilling for studies has been included and the 4th EIA amendment will include principal components for Chalcobamba (crushing and conveyor), with waste dump fully within the property boundary. The planned SulFOBamba infrastructure has been identified within the Las Bambas mining concession, however the infrastructure and deposit are not located within the area of MMG land ownership.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> The metallurgical process is a conventional froth flotation concentrator and thickener to produce two separate Cu and Mo concentrates and is appropriate for the style of mineralisation. Metallurgical copper concentration process comprises the following activities; crushing, grinding and flotation, producing copper and molybdenum concentrates. Copper concentrates contain gold and silver as by-products. Las Bambas Project commenced commercial production on 1 July 2016. Extensive comminution and flotation test work has been conducted and metallurgical recoveries determined for different rock types and different mining areas. Bulk samples and pilot scale tests have been conducted on representative samples of the deposits. For the Ferrobamba deposit, nearly all of the tests were completed by the G&T laboratory in Canada as part of Feasibility Study, though a small number of additional confirmatory tests were included from more recent testing by ALS in Peru. For Chalcobamba, all of the tests were completed by G&T and reported in the Feasibility Study. For SulFOBamba, the data analysed were those from testing at G&T in 2015. Arsenic minerals identified in the orebody are being mapped and monitored in the mining process. The level of Arsenic in Las Bambas concentrates remains low by market standards and concentrate quality continues to be very acceptable for processing by smelters internationally. The recovery equations have been provided by the Metallurgical Group at Las Bambas in coordination with MMG Group Technical Services. The equations were generated based on metallurgical test work, from diamond drilling sample data in each pit. It should be noted that the copper recovery is a function of the ratio of acid soluble copper (CuAS) to total copper (CuT), which is a determining factor for the recovery. The copper recovery is determined by the following equations. All assumptions are validated annually with plant performance data. <p style="text-align: center;">Ferrobamba:</p> <p style="text-align: center;">For all the materials except marble:</p>

Assessment Criteria	Commentary																				
	<p>$Cu Recovery (\%) = (96.0-94.0*(CuAS/CuT) + 1.0$</p> <p>For marble:</p> <p>$Cu Recovery (\%) = (96.0-94.0*(CuAS/CuT) - 13 + 1.0$</p> <p>Chalcobamba:</p> <p>$Cu Recovery (\%) = 94.4-90.0*(CuAS/CuT) + 1.0$</p> <p>Sulfobamba:</p> <p>$Cu Recovery (\%) = 89.2 - 80.4*(CuAS/CuT) + 1.0$</p> <p>An improvement in recovery of 1.0% has been added to account for ongoing metallurgical improvement work since the start of operation.</p> <ul style="list-style-type: none"> The recovery of Mo, Ag, Au, has been provided by Metallurgical Group at Las Bambas. <table border="1" data-bbox="539 842 1297 994"> <thead> <tr> <th colspan="2">Metal</th> <th>Ferrobamba</th> <th>Chalcobamba</th> <th>Sulfobamba</th> </tr> </thead> <tbody> <tr> <td>Mo</td> <td>%</td> <td>55.5</td> <td>55.5</td> <td>55.5</td> </tr> <tr> <td>Ag</td> <td>%</td> <td>75.0</td> <td>75.0</td> <td>75.0</td> </tr> <tr> <td>Au</td> <td>%</td> <td>71.0</td> <td>71.0</td> <td>71.0</td> </tr> </tbody> </table> <ul style="list-style-type: none"> Benchmarking of data from four other mines in South America has been completed and the recovery algorithms that describe performance at these mines compared with those used for the three Las Bambas deposits. The four other mines were Tintaya, Toquepala, Cerro Verde and Antamina. 	Metal		Ferrobamba	Chalcobamba	Sulfobamba	Mo	%	55.5	55.5	55.5	Ag	%	75.0	75.0	75.0	Au	%	71.0	71.0	71.0
Metal		Ferrobamba	Chalcobamba	Sulfobamba																	
Mo	%	55.5	55.5	55.5																	
Ag	%	75.0	75.0	75.0																	
Au	%	71.0	71.0	71.0																	
Environmental	<ul style="list-style-type: none"> The Environmental Impact Study for the Las Bambas Project was approved on 7 March 2011 by the Peruvian Government with directorial resolution N°073-2011-MEM/AAM. The construction of the project processing facilities including Tailings Storage Facility at Las Bambas was approved 31 May 2012 by the General Directorate of Mining through Resolution N°178-2012-MEM-DGM/V. The Mine Closure Plan for the Las Bambas Project was approved 11 June 2013 through Directorial Resolution N°187-2013-MEM-AAM. As per the Peruvian regulatory requirements, an update of the Mine Closure Plan was approved 28 September 2016, through Directorial Resolution N°288-2016-MEM-DGAAM. A first amendment to the Environmental Impact Study was approved 14 August 2013 through Directorial Resolution N°305-2013-MEM-AAM, whereby amendments to the Capacity of the Chuspipi water reservoir and changes to the environmental monitoring program were approved. On 26 August 2013 the relocation of the molybdenum circuit (molybdenum plant, filter plant and concentrate storage shed) from the Antapaccay region to the Las Bambas project area was approved by the environmental regulator through Directorial Resolution N°319-2013-MEM-AAM, after assessment of the technical report showed that the environmental impacts of the proposed changes were not significant. On 6 November 2013, through Directorial Resolution N°419-2013-MEM-DGM/V, the General Directorate of Mining approved the amendment of the construction permit for the processing facilities to allow the construction of the molybdenum circuit at the Las Bambas project area. 																				

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> • Minor changes to the project layout were approved 13 February 2014 through Directorial Resolution N°078-2014-MEM-DGAAM and 26 February 2015, through Directorial Resolution N°113-2015-MEM-DGAAM. • On 17 November 2014, the second modification of the Study of Environmental Impact was approved with Directorial Resolution N° 559-2014-EM/DGAAM, whereby changes to the water management infrastructure and changes in the transport system from concentrate slurry pipeline to bimodal transport (by truck and train) were approved. • A second amendment to the construction permit for processing facilities was approved through Directorial Resolution N°419-2015-MEM-DGM/V to allow changes to the design of the tailings storage facility and changes to the water management system and auxiliary infrastructure. • Environmental approval for minor changes to project layout was approved 1 June 2016 through Directorial Resolution N°177-2016-MEM-DGAAM. • On 6 October 2018, the third amendment to the Environmental Impact Study was approved through Directorial Resolution 00016-2018-SENACE-PE-DEAR, to allow changes to the molybdenum plant, included haul road Ferrobamba to Chalcobamba, impacts and measure management in public transport, other ancillary infrastructure and changes to the environmental management plan. • Geochemical characterisation studies on waste rock samples were conducted in 2007 and 2009/2010 as part of the Feasibility and Environmental Impact Studies, conclusions from these studies indicate that it should be expected that less than 2% of the waste rock from the Ferrobamba and Chalcobamba pits should be Potentially Acid Forming (PAF). No acid rock drainage from the waste rock dumps from these two pits should be expected. Waste rock samples from Sulfobamba were found to contain higher concentration of sulphur and that 30% to 40% of waste rock could be PAF. • Further geochemical characterisation studies on waste rock and tailings samples are currently underway to support the Environmental Impact Study Modification. • The operation of the Ferrobamba waste rock dump was approved on 29th September 2015 by the General Directorate of Mining through Directorial Resolution N°1780-2015-MEM/DGM. • Currently, Las Bambas has four water use licenses: <ul style="list-style-type: none"> ○ License for underground water obtained with Directorial Resolution 0519-2015-ANA / AAA.XI.PA, for a volume up to 9,460.800 m³ / year. ○ License for non-contact water obtained with Directorial Resolution 0518-2015-ANA / AAA.XI.PA, for a volume up to 933.993 m³ / year. ○ License for contact water obtained with Directorial Resolution 0520-2015-ANA / AAA.XI.PA, for a volume up to 4,730,400 m³ / year. License for contact water obtained with Directorial Resolution 0957-2016-ANA / AAA.XI.PA, for a volume up to 4,730,400 m³ / year. ○ License for fresh water obtained with Directorial Resolution 0778-2016-ANA / AAA.XI.PA, for a volume up to 23,501,664 m³ / year.

Assessment Criteria	Commentary
Infrastructure	<p>Las Bambas has the following infrastructure established on site:</p> <ul style="list-style-type: none"> • Concentrator currently in operation. • Based on the current TSF design and the design assumptions for dry settled density and beach angle, the TSF currently under construction at Las Bambas has a final capacity of 784Mt of tailings from processing 800Mt. Three studies have been conducted looking at increasing tailings storage capacity at Las Bambas: <ul style="list-style-type: none"> ○ Tailings characterization test work to assess final settled density and beach slope in current TSF. ○ Options assessment to increase capacity at TSF currently under construction. ○ Pre-feasibility study for an additional TSF at Tambo valley. • Camp accommodation for staff • Water supply is sufficient for site and processing, sourced from the following: rainfall and runoff into Chuspipi dam, groundwater wells, contact waters, recirculating water in the process plant. Pump station from Challhuahuacho River off-take structure. • Transport of the copper concentrate is performed by trucks, covering a distance of 380km, to the Imata Village, then it is transported by train, covering a distance of 330km, up to Matarani Port in Arequipa region. Transport of the molybdenum concentrate will be performed by trucks all the way from Las Bambas site to Matarani Port, covering a distance of 710Km. This method is also used temporarily for some of the copper concentrate. • There are principal access roads that connect Las Bambas and national routes, Cotabambas to Cusco and Cotabambas to Arequipa. • High voltage electrical power is sourced from the national grid Cotaruse – Las Bambas, with a capacity of 220Kv. • The majority of staff working at the operation are from the region immediately surrounding the project. • Technical personnel are mostly sourced from within Peru. The operation has a limited number of expatriate workers. Additional support is provided by MMG office's in Lima and Melbourne Group office personnel. • Chalcobamba pit operation requires additional purchase of land to the North side of the lease (Waste dump 2). However, an alternative location is being evaluated that does not require land purchase; this is what the LoA planning is based on currently. Sulfobamba pit operation requires additional purchase of land for the pit and other infrastructure.
Costs	<ul style="list-style-type: none"> • Las Bambas Project commenced commercial production on 1 July 2016; future additional capital costs such as TSF 2 expansion are mainly based on pre-feasibility studies, taking into account of additional information now available during two years of operation. The operating costs used for Ore Reserves estimation are based on the 2018 Budget (2018-2020) and 2017 Life of Asset (LoA) (2021 onwards) as per Corporate (MMG) guidelines and other considerations. Specifically: <ul style="list-style-type: none"> ○ Average costs are calculated by using the first 3 years budget plus

Assessment Criteria	Commentary
	<p>remaining LoA estimated costs year by year;</p> <ul style="list-style-type: none"> ○ Necessary adjustments required for the input prices and consumption rates, updated during the budget process, are made to establish connection between the budget and LoA; and ○ Approved cost savings from identified initiatives and improvements to be delivered over the life of mine are incorporated. <ul style="list-style-type: none"> • No deleterious elements are expected in the concentrates that would result in smelter penalties. • Metal prices and exchange rates are the same as those reported in the section for cut-off grade parameters. These Board approved prices and rates are provided by MMG Corporate and are based on external company broker consensus and internal MMG strategy. • Transportation charges are based on quotations from local companies. • Treatment and refining charges (TC/RC's) are based on marketing actuals and projections. Royalties payable are based on information provided by the Finance and Commercial Group at Las Bambas. • Sustaining capital costs, together with mining costs and processing costs have been included in the pit optimisation. The sustaining capital costs are principally related to TSF construction and equipment replacement. The inclusion or exclusion of these costs in the Ore Reserves estimation process has been done following MMG guidelines according the objective of each capital expenditure in the operation.
Revenue factors	<ul style="list-style-type: none"> • All mining input parameters are based on the Ore Reserves estimate LoA Low Case production schedule. All cost inputs are based on tenders and estimates from contracts in place as with net smelter returns (NSR) and freight charges. These costs are comparable with the regional averages. • The gold and silver revenue is via a credit at the refinery. • TC/RC's have been included in the revenue calculation for the project.
Market assessment	<ul style="list-style-type: none"> • MMG considers that the outlook for the copper price over the medium and longer term is positive, supported by further modest demand growth which is expected to exceed increases in supply. • Global copper consumption growth will continue to be underpinned by rising consumption in China and the developing countries in Asia as these nations invest in infrastructure such as power grids, commercial and residential property, motor vehicles and transportation networks and consumer appliances such as air conditioners. • Supply growth is expected to be constrained by a lack of new mine projects ready for development and the requirement for significant investment to maintain existing production levels at some operations. • Las Bambas has life of mine agreements in place with MMG South America and CITIC covering 100% of copper concentrate production which is sold to these parties at arms' length international terms. These agreements ensure ongoing sales of Las Bambas concentrate.

Assessment Criteria	Commentary
Economic	<ul style="list-style-type: none"> • The costs are based on the 2018 LoA Low Case projections which are based on actual costs and 2018 Budget information. • The financial model of the Ore Reserves mine plan shows that the mine has a substantially positive NPV. The discount rate is in line with MMG's corporate economic assumptions. • Various sensitivity analyses on the key input assumptions were undertaken during mine optimisations and financial modelling. All produce robust positive NPVs.
Social	<ul style="list-style-type: none"> • Las Bambas project is located in the Apurimac region that has a population of approximately 456,000 inhabitants (Census 2014). The region has a University located in the city of Abancay, with mining programs that provide professionals to the operation. The project straddles two provinces of the Apurimac region, Grau and Cotabambas. • Las Bambas Project contributes to a fund - "FOSBAM" - that promotes activities for the sustainable development of the disadvantaged population within the project's area of influence, comprising the provinces Grau and Cotabambas – Apurimac. • Las Bambas Project and the local community entered into an agreement for the resettlement of the rural community of Fuerabamba, Convenio Marco. The construction the township of Nuevo Fuerabamba was completed in 2014 and the resettlement of all community families were completed in 2016. Currently, in joint work with the community, MMG are executing the commitments described in the framework agreement - Convenio Marco. • During the extraordinary general meeting in January 2010, Fuerabamba community approved the agreements contained in the so-called "compendium of negotiating resettlement agreements between the central negotiating committee of the community of the same name and representatives of Las Bambas mining project" that considers 13 thematic areas. • Las Bambas Project provides important support to the community in the areas of agriculture, livestock and health, education, and other social projects, which is well received. • Las Bambas has had periodic social conflict with communities along the public road used for concentrate transport and logistics. In response to these concerns Las Bambas has committed to key aspects of the Cotabambas Social Development Plan, has formalised dialogue processes with communities along the road; and is working to systematically improve the road conditions and reduce the impacts, while also maximising the social development opportunities available to these communities. • Las Bambas applies ICMM and other world class social standards.
Other	<ul style="list-style-type: none"> • Las Bambas owns 7,718Ha of land within the mining project. • The mining concession totals an area of 35,000 hectares, which includes the area containing the three mineral deposits and their corresponding infrastructures. • Only 10% of the concession of Las Bambas has been explored year to date.

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> • According to Directorial Resolution N°187-2013-MEM-DGM/V, dated May 2nd, 2013, the Pit Mining Plan and the waste dump was approved for the Las Bambas project. • Approval for the exploitation of the Ferrobamba pit was granted on 30th September 2015 through Directorial Resolution N° 1780-2015-MEM/DGM. • The title for the Beneficiation Concession and approval for the operation of the concentrator plant was granted on November 30th, 2015 through Directorial Resolution N° 2536-2015-MEM/DGM. • It is reasonable to expect that the future land acquisition and community issues will be materially resolved and government approvals will be granted within the required timeframe.
Classification	<ul style="list-style-type: none"> • The classification of Ore Reserves is based on the requirements set out in the JORC code 2012, based on the classification of Mineral Resources and the cut-off grade. The material classified as Measured and Indicated Mineral Resources within the final pits and is above the breakeven cut-off (BCoG CuT%) grade is classified as Proved and Probable Ore Reserves respectively. • The Competent Person considers this appropriate for the Las Bambas Ore Reserves estimate. • No Probable Ore Reserves have been derived from Measured Mineral Resources.
Audit or Reviews	<ul style="list-style-type: none"> • The 2014 Ore Reserves were reviewed by Runge Pinock Minarco for the MMG Competent Person's Report. • The 2018 Ore Reserve estimates have been reviewed and validated by Edgard Mendoza, Las Bambas Long Term Planning Superintendent; in coordination with Group Technical Services. • An external third party audit was undertaken in 2018 on the 2017 Ore Reserve by AMC Consultants. The audit concluded that the 30 June 2017 Ore Reserve was prepared to an acceptable standard at the time it was completed. The audit also identified some minor improvements to the estimation process and one potentially material issue in the application of mining ore recovery. It states that: "AMC understands there are several projects presently underway to minimise ore loss and dilution. These should be monitored and any residual discrepancy between the Ore Reserve model and the mill claim should be considered in the Ore Reserve process." • The mining ore recovery was discussed in mining factors and assumptions section of this report. An interim review of the reconciliation results will be conducted in March 2019.
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> • The principal factors that can affect the confidence on the Ore Reserves are: <ul style="list-style-type: none"> ○ Proved Ore Reserves are considered to have a relative accuracy of +/- 15% within a volume equivalent to 3 months of production while Probable Ore Reserves are considered to have a relative accuracy of +/- 15% within a volume equivalent to 12 months of production. ○ Geotechnical risk related to slope stability due to uncertainties in the geomechanical / hydrology models, rock mass blast damage, and increase in mining rate.

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> ○ Metallurgical recovery model uncertainty due to operational variability. In the best case scenario, this would represent variability of +/- 2% and in the worst scenario +/- 5% to metal recovery. ○ Increases in rising operating costs for mining and processing. ○ Increase in selling cost due to the transportation (truck and rail) cost increases. ○ Capital costs variation for the new or expansion of current TSF. Also land acquisition and/permitting delays for additional TSF needs. ○ Mining dilution and recovery adjustments as results of future reconciliation studies when more operational data become available. ○ The political context can impact in the schedule of the approvals of studies and good relation with the communities must be maintained ○ Change in environmental legislation, could be more demanding.

3.3.3 Expert Input Table

A number of persons have contributed key inputs to the Ore Reserves determination. These are listed below in Table 7.

In compiling the Ore Reserves the Competent Person has reviewed the supplied information for reasonableness, but has relied on this advice and information to be correct.

Table 7 Contributing experts – Las Bambas Ore Reserves

EXPERT PERSON / COMPANY	AREA OF EXPERTISE
Rex Berthelsen, Group Manager Technical Governance, MMG Ltd (Melbourne)	Mineral Resource models
Amy Lamb, Principal Metallurgist, MMG Ltd (Melbourne)	Updated processing parameters and production record
Luis Tejada, Superintendent Geotechnics and Hydrogeology, MMG Ltd (Las Bambas)	Geotechnical parameters
Christian Holland, Principal Geotechnical Engineering, MMG Ltd (Melbourne)	
Edgard Mendoza, Long Term Planning Superintendent, MMG Ltd (Lima)	Cut-off grade calculations Whittle/MineSight optimisation and pit designs
Jorge Valverde, Technical Services Manager, MMG Ltd (Las Bambas)	Production reconciliation
David Machin, Principal Water and Tailings Engineer, MMG Ltd (Melbourne)	Tailings Management
Giovanna Huaney, Environmental Superintendent, MMG Ltd (Las Bambas)	Environmental/Social/Permitting
Ramiro Zuñiga, Business Evaluation Specialist, MMG Ltd (Lima)	Economics Assumptions
Steve Whitehead, General Manager Marketing, MMG Ltd (Melbourne)	Marketing

3.3.4 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Ore Reserve statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Yao Wu, confirm that I am the Competent Person for the Las Bambas Ore Reserve section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a Member of The Australasian Institute of Mining and Metallurgy
- I have reviewed the relevant Las Bambas Ore Reserve section of this Report to which this Consent Statement applies.

I am a full time employee of MMG Ltd. at the time of the estimation.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest.

I verify that the Las Bambas Ore Reserve section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Las Bambas Ore Reserve.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Las Bambas Ore Reserves - I consent to the release of the 2018 Mineral Resources and Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

5/12/2018

Yao Wu MAusIMM(CP)(#108391)

Date:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Andrew Fowler
Lima, Peru

Signature of Witness:

Witness Name and Residence: (e.g. town/suburb)

4 KINSEVERE OPERATION

4.1 Introduction and setting

Kinsevere is located in the Katanga Province, in the southeast of the Democratic Republic of Congo (DRC). It is situated approximately 27 kilometres north of the provincial capital, Lubumbashi (Figure 4-1), at latitude S 11° 21' 30" and longitude E 27° 34' 00".

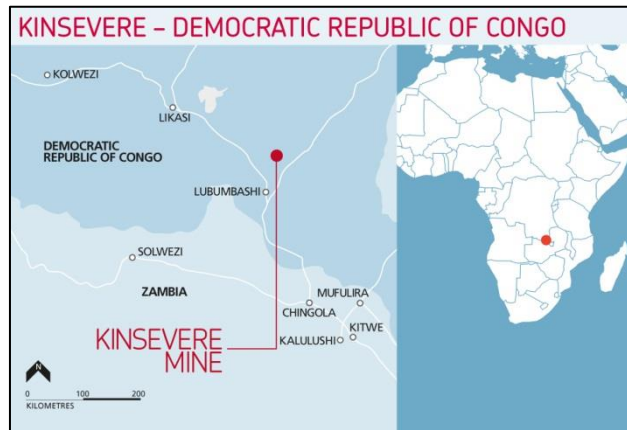


Figure 4-1 Kinsevere Mine location

Kinsevere is a conventional truck and excavator operation with atmospheric leaching of the oxide ore using a solvent extraction electro-winning (SX-EW) plant. The mine was started in 2006 using heavy media separation (HMS) and an electric arc furnace operation. The electric arc furnace was put on care and maintenance in 2008 with HMS then producing a direct shipping ore product grading 25% copper. The HMS was decommissioned in June 2011 when the Stage II SXEW plant was commissioned.

4.1.1 Results

The 2018 Kinsevere Mineral Resource are summarised in Table 8. The Kinsevere oxide Mineral Resource is inclusive of the Ore Reserve.

Table 8 2017 Kinsevere Mineral Resource tonnage and grade (as at 30 June 2018)

Kinsevere Mineral Resource					
				Contained Metal	
	Tonnes	Copper	Copper	Copper	Copper AS
	(Mt)	(% Cu)	(% CuAS¹)	('000)	('000)
Oxide Copper²					
Measured	2.0	4.3	3.8	88	77
Indicated	9.7	3.1	2.8	307	271
Inferred	1.8	2.4	2.1	43	38
Total	13.6	3.2	2.8	438	387
Transition Mixed Ore (TMO) Copper³					
Measured	1.3	2.9	1.2	38	16
Indicated	3.4	2.0	0.8	71	29
Inferred	0.4	1.9	0.8	7	3
Total	5.2	2.3	0.9	116	48
Primary Copper⁴					
Measured	6.1	2.7	0.2	167	10
Indicated	15.8	2.1	0.1	335	21
Inferred	2.0	1.7	0.1	35	2
Total	24.0	2.2	0.1	537	33
Stockpiles					
Indicated	10.2	2.2	1.4	221	146
Total	10.2	2.2	1.4	221	146
Kinsevere Total	52.9	2.5	1.2	1,313	614

¹ CuAS stands for Acid Soluble Cu

² 0.6% CuAS cut-off grade

³ if CuAs / Cu (Ratio) is less than or equal to 0.5 and greater than 0.3 a 0.6% Total Cu cut-off grade is applied; otherwise if Ratio is greater than 0.2 and less than or equal to 0.3 a 0.7% Total Cu cut-off grade is applied

⁴ 0.7% Total Cu cut-off grade

All Mineral Resources except stockpiles are contained within a US\$3.51/lb Cu pit shell

Contained metal does not imply recoverable metal.

Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors.

4.2 Mineral Resources JORC 2012 Assessment and Reporting Criteria

The following information provided in Table 9 complies with the 2012 JORC Code requirements specified by "Table-1 Section 1-3" of the Code.

Table 9 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Kinsevere Mineral Resource 2018

Criteria	Status
Section 1 Sampling Techniques and Data	
Sampling techniques	<ul style="list-style-type: none"> • The Mineral Resource uses a combination of reverse circulation (RC) drilling diamond drilling (DD). The RC drilling is predominately collected for grade control and the DD is used for exploration and resource delineation work. • DD core is sampled mostly as 1m intervals while samples in un-mineralised zones are sampled over 4m lengths. Sampling is predominantly performed by cutting half core, with half retained on site for future reference. For PQ drilling undertaken 2015-2017, quarter core was submitted for sampling. • Grade control drilling (RC) is composited into 2m samples collected after riffle splitting. • Each sample is crushed and pulverised to produce a pulp (>85% passing 75µm) prior to analysis at the site SGS laboratory. • Measures taken to ensure sample representivity include orientation of the drill holes as close as practical to perpendicular to the known mineralised structure. In addition field duplicates have been taken and analysed. • The sample types, nature, quality and sample preparation techniques are considered appropriate for the style of the Kinsevere mineralisation (sediment hosted base metal) by the Competent Person.
Drilling techniques	<ul style="list-style-type: none"> • RC drilling was used to obtain 2m composited RC chip samples. 284,533m or 78% of the sample data used in the Mineral Resource were from RC samples (5.5" hammer), of that 230,025m (63% of total meters) was from Grade Control drilling. • PQ and HQ size DD core was used to obtain nominal 1m sample lengths. DD core was not routinely oriented prior to the 2015 drilling campaign. 81,481m or 22% of the sample data used in the Mineral Resource were from DD samples. • 57,846m of RC Grade Control drilling was completed since the 2017 estimation and utilised in the 2018 estimate. • 7,329m of DD drilling was completed since the 2017 estimation and utilised in the 2018 estimate. The drilling is dominantly PQ with minor HQ. The recent DD drilling (2015 to 2017) was drilled to inform a Scoping, PFS and FS for the Sulphide Study. • In the view of the Competent Person sampling is of a reasonable quality to estimate the Mineral Resource.

Drill sample recovery	<ul style="list-style-type: none"> • DD core recovery recorded was typically above 90%, with only minor losses in competent ground (98% within competent ore zones). As expected, the recovery fell in unconsolidated ground such as weathered material close to surface and in vuggy zones of dolomitic rocks (average recovery approximately 85%, in this area). The vuggy zones are generally controlled by major structures within the dolomitic rocks and constitute a minor proportion of the overall resource. Voids in these areas can be present where recovery is minimal. Triple tube core barrels were used to maximize core recovery. DD core recovery and run depth are verified and checked by a geological technician at the drill site. This data is recorded and imported in the database. • RC drilling has been observed for sample recovery with adequate sample volume being returned. However, no quantitative measurements of recovery have been recorded. • There is no observed relationship between core loss and mineralisation or grade - no preferential bias has occurred due to any core loss.
Logging	<ul style="list-style-type: none"> • RC chips are logged by geologists directly into an Excel logging template, geological information captured includes: lithology, stratigraphy, weathering, oxidation, colour, texture, grain size, mineralogy and alteration. This data is then imported into the database. For DD core samples both geological and geotechnical information is logged. (lithology, stratigraphy, mineralisation, weathering, alteration, geotechnical parameters: strength, RQD, structure measurement, roughness and infill material) • All RC chip and DD core samples (100%) have been geologically logged to a level that can support appropriate Mineral Resource estimation. • Logging captures both qualitative descriptions such as geological details (e.g. rock type, stratigraphy) with some quantitative data (e.g. ore mineral percentages). Core photography is not known to have occurred prior to MMG ownership. Since MMG took control of the site all DD core is photographed. • The total length and percentage of the relevant intersections logged is 100%.
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> • DD core was split in half (NQ) or quartered (PQ) using a diamond saw. Sample lengths were cut as close to 1m as possible while also respecting geological contacts. Samples were generally 2kg to 3kg in weight. • RC samples are collected from a cyclone by a trained driller's assistant. If the sample was dry the sample was passed through a riffle splitter and collected into a pre-numbered calico bag. Residual material was sampled and sieved for collection into chip trays for logging and the remainder returned to the larger poly-weave bag. The splitter was cleaned using compressed air or a clean brush and tapped using a rubber mallet. If the sample was wet then the sample was dried in the laboratory oven before being split according to the procedure above (for dry samples). • Samples from individual drill holes were sent in the same dispatch to the preparation laboratory. • Representivity of samples was checked by sizing analysis and duplication at the crush stage. • Field duplicates were inserted at a rate of approximately 7% to ensure that the sampling was representative of the in-situ material collected. Field duplicates in current RC programs have shown acceptable levels of repeatability across all elements analysed. • These practices are industry standard and are appropriate for the grain size of the

	<p>material being sampled.</p> <ul style="list-style-type: none"> • RC and DD samples (pre-2015 for DD) were prepared on-site by the geology department, who provide pulp samples to the SGS analytical facility also on site at Kinsevere. The samples were oven dried at approximately 80°C, crushed to 85% passing -2mm using a jaw crusher and milled to 85% passing 75µm using one of three single sample LM2 vibratory pulverising mills. • Since 2017 DD drilling, core was processed at the onsite Exploration core yard. Sample preparation was conducted at this facility through an ALS managed Containerised Preparation Laboratory (CPL). Pulp samples were then sent to ALS Johannesburg for analysis. • The sample size for both RC and DD is considered appropriate for the grain size of the material being sampled.
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> • RC ore control samples are currently assayed at the onsite SGS Laboratory. <ul style="list-style-type: none"> ○ Following preparation, 50g pulp samples are routinely analysed for total and acid soluble copper, cobalt and manganese. ○ A 3 acid digest with AAS finish was used to analyse for total values. ○ A sulphuric acid digest with AAS finish was used to analyse for acid soluble copper. • All DD core samples prior to 2011 were assayed at: <ul style="list-style-type: none"> ○ ALS Chemex Laboratory, Johannesburg ○ McPhar Laboratory, Philippines ○ ACTLabs Laboratory, Perth ○ Samples were analysed for total copper and acid soluble copper with some having a full suite of elements analysed with a four acid digest and ICP-OES analysis. • From 2011, prepared samples were submitted to the ISO 17025 accredited SGS Laboratory in Johannesburg with the following assay scheme: <ul style="list-style-type: none"> ○ ICP-OES method with a 4-acid digest analysing 32 elements including copper from 0.5ppm to 1%. ○ ICP-OES method using alkali fusion is applied to over-range copper results. ○ ICP-AES with a 4-acid digest was used for calcium and sulphur analysis ○ XRF was used for uranium analysis. ○ Acid soluble copper using a sulphuric acid digest and AAS finish. • For 2015 to 2017 DD drilling, prepared samples were submitted to the ALS Laboratory in Johannesburg with the following assay scheme: <ul style="list-style-type: none"> ○ ICP-OES (ME-ICP61) method with a 4-acid digest analysing 33 elements plus OG triggers when Cu greater than 1% (OG62) ○ LECO analysed Total Carbon (C-IR07), Organic Carbon (C-IR17), Total Sulphur (S-IR08) and Sulphide Sulphur (S-IR07) ○ Acid soluble copper using a Sequential Leach (Cu-PKGPH06) finish. • No geophysical tools, spectrometers or handheld XRF instruments have been used in the analysis of samples external to the ALS laboratory for the estimation of Mineral Resources. • QAQC employs the insertion of Certified Reference Material (CRM) every 25 samples; blanks, field duplicates, coarse duplicates and pulp duplicates are taken/ inserted within every batch of 50 samples; and umpire laboratory checks are submitted for every batch of 20 samples to check accuracy, precision and repeatability of the assay result. Acceptable levels of accuracy and precision have been established. If control

	<p>samples do not meet an acceptable level the entire batch is re-analysed.</p> <ul style="list-style-type: none"> The analysis methods described above are appropriate for the style and type of mineralisation.
Verification of sampling and assaying	<ul style="list-style-type: none"> Significant intersections are verified by alternate company personnel following receipt of assay results and during the geological modelling process. Twinned pre-collars are present in the database. These were used to confirm and check geological intervals and/or assay intervals. Twin drill holes are not used in the Mineral Resource. Data is collected in Excel spread sheets and imported into industry standard databases that have built in validation systems and QAQC reporting systems. Raw data is imported in the database as received by the laboratory. Where data was deemed invalid or unverifiable it was excluded from the Mineral Resource estimation. There are no adjustments to the assay data.
Location of data points	<ul style="list-style-type: none"> Prior to 2011 all drill hole collars were located using a hand held GPS. Accuracy of GPS is +/- 5m for x and y coordinates and has poor accuracy of the z (elevation) coordinates. Elevations of these holes were later adjusted by using a LIDAR survey method. RC and DD holes collared post-2011 are surveyed by qualified surveyors. Down hole surveys have been carried out using Eastman single-shot cameras or Reflex EZ tools. Surveys are taken at variable intervals and stored in the database. Coordinates are in Kinsevere Mine Grid, which is related to WGS84 by the following translation: -8000000 m in northing and -22.3 m in elevation. A LIDAR survey was used to generate a topographic surface. This surface was also used to better define the elevation of drill hole collars. The LIDAR survey is considered to be of high quality and accuracy for topographic control.
Data spacing and distribution	<ul style="list-style-type: none"> Grade control RC drill pattern spacing is 5m x 15m, which is sufficient to adequately define lithology and mineralisation domain contacts and transition zones. The overall DD pattern spacing is between 25m and 75m, which is sufficient to establish the required degree of geological and grade continuity that is appropriate for the Mineral Resource. Between 2015 and 2017, diamond drilling aimed to infill target areas to 40m x 40m spacing and down to 20m x 20m in places. DD samples are not composited prior to being sent to the laboratory however the nominal sample length is generally 1m. RC samples are 2m intervals but compositing up to 4m has occurred in the past.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> The mineralisation strikes between north and north-west at Mashu / Central pits, and to, the east south east at Kinsevere Hill. All drill holes are oriented such that drill holes have a high angle of intersection with the dominant strike and dip of bedding and structures, with the local scale of mineralisation also considered. All drill holes are either oriented east or west with dips of 60° to sub-vertical. The combination of both east and west orientations likely minimises sampling bias, which, if present, is not considered material.
Sample security	<ul style="list-style-type: none"> Measures to provide sample security include: <ul style="list-style-type: none"> Adequately trained and supervised sampling personnel. Sea containers used for the storage of samples are kept locked with keys held

	<p>by the security department.</p> <ul style="list-style-type: none"> ○ Assay laboratory checks of sample dispatch numbers against submission documents.
Audit and reviews	<ul style="list-style-type: none"> • An independent audit of the Mineral Resource model was completed in June 2014, by the MSA Group Pty Ltd and was commissioned by MMG Limited (J2851 Kinsevere Mineral Resource Audit June 2014). No material errors were found and recommendations and suggestions have been incorporated into the current Mineral Resource Estimate. • An independent audit of the Mineral Resource model was completed in October 2016 and November 2017, by Pennywise Pty Ltd as part of an audit on the results of the Sulphide Scoping and Pre-Feasibility Study and was commissioned by MMG Limited. No material errors were found. • Internal visits by the Competent Person and MMG Group Office geologists to the site laboratory, sample preparation area and drill locations are undertaken at least annually. These inspections have not identified any material risks.
Section 2 Reporting of Exploration Results	
Mineral tenement and land tenure status	<ul style="list-style-type: none"> • The Kinsevere Mining Licence (PE 528) is located approximately 27 km north of Lubumbashi, the provincial capital of the Katanga Province, in the southeast of the Democratic Republic of the Congo (DRC). The PE 528 permit covers the three major deposits of Tshifufiamashi, Tshifufia and Kinsevere Hill/Kilongo • MMG has a Contrat d'Amodiation (Lease Agreement) with Gécamines to mine and process ore from the Kinsevere Project until 2024. A renewal application process for 15 year extension shall be submitted to DRC regulatory at least 1 year and no more than 5 years before the expiry date. • A Contrat d'Amodiation is provided for under the DRC Mining Code, enacted by law No 007/2002 of July 11, 2002. • A conversion of the neighbouring PR7274 to an exploitation permit was completed in 2018. Tenement amalgamation (of PE528 and PE7274). • There are no known impediments to operating in the area.

Exploration done by other parties

Summary of Previous Exploration Work by Gecamines and EXACO

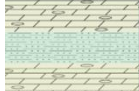

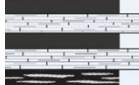


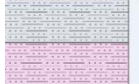

Deposit	Pitting	Trenching		Drilling	
	No (m depth)	No. (metres)	Significant Grades	No. holes (metres)	Significant Grades
Tshifufiamashi	11	16 (1,304 m)	5.8% Cu 0.2% Co over 50 m	37 (846 m)	10.5% Cu 0.72% Co over 22.2 m
Tshifufia Central	-	17 (1,106 m)	7.6% Cu 0.3% Co over 15 m	19 (950 m)	6.3% Cu 0.6% Co over 23 m
Tshifufia South	-	39 (278 m)	7.2% Cu 0.3% Co over 40 m	11 (497 m)	
Kinsevere Hill	7 (44 m max.)	11 (625 m)	6.6% Cu 0.2% Co over 20 m	10 (1,021 m)	3.99% Cu 0.22% Co over 14.6 m

- In 2004 Anvil Mining carried out intensive exploration drilling to define the deposits in Kinsevere.
- In 2012 MMG continued exploration aimed at identifying additional mineralisation beyond the Anvil Mining Mineral Resource.
- In 2013/2014 MMG Exploration have been conducting works around the Mine Lease within a 50 km radius of the known deposit to explore for additional high-grade oxide material.
- In 2015 MMG conducted a Scoping Study on the potential to process the copper sulphide ore at Kinsevere located beneath the current oxide Ore Reserves. As part of this study, 5 DD holes were drilled in early 2015. In August 2015, DD drilling recommenced as part of a follow on Pre-Feasibility Study to increase confidence in the copper sulphide Mineral Resource. This drilling was completed at the end of 2016 and included in the 2017 Resource Estimate.
- Drilling since May 2017 was used to inform the Sulphide Feasibility Study.

Geology

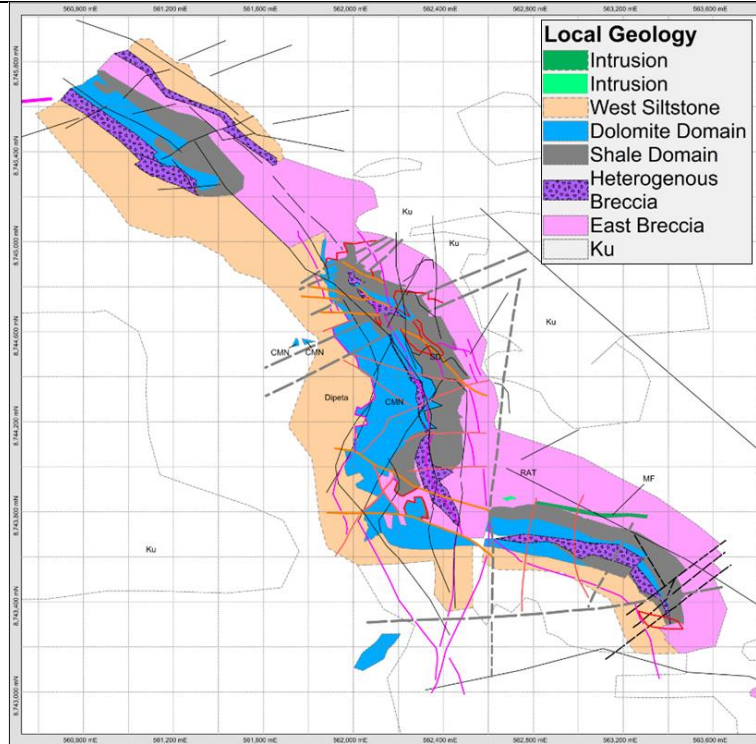
- The Kinsevere Copper deposit is a sedimentary hosted copper deposit. The deposit is hosted in moderately to steeply dipping Neoproterozoic sedimentary formation of the Roan group of the Katanga stratigraphy in the Mine Series subgroup of Katangan African Copper belt.
- On surface, the Kinsevere Copper deposit has been mapped as made of three separate Mine Series fragments (large breccia clasts of the Mine Series) whereby the first two fragments are situated along a major N-S oriented fracture and separated by a sinistral strike-slip fault, while the third fragment, called Kinsevere Hill, is situated along major NW-SE fracture and separated from the other fragments by another sinistral strike-slip fault. All these fragments are affected by fractures and breccias.
- The sulphide, transitional and oxide mineralisation in the Kinsevere copper deposit are either disseminated in recrystallised layers or infilling bedding plans, reactivated bedding, fractures and joints. Sulphide mineralisation includes chalcopyrite, bornite, chalcocite and pyrite. Oxide mineralization is dominated by malachite with lesser chrysocolla. A transitional zone exists between the primary and oxide zones with both a horizontal trend, controlled by ground water movements, and a sub vertical trend controlled by bedding and structures. Transitional copper species include chalcocite, cuprite, covellite and native copper. This zone is known as the TMO (transitional/mixed ore) zone.

Kinsevere Mine Series Stratigraphy

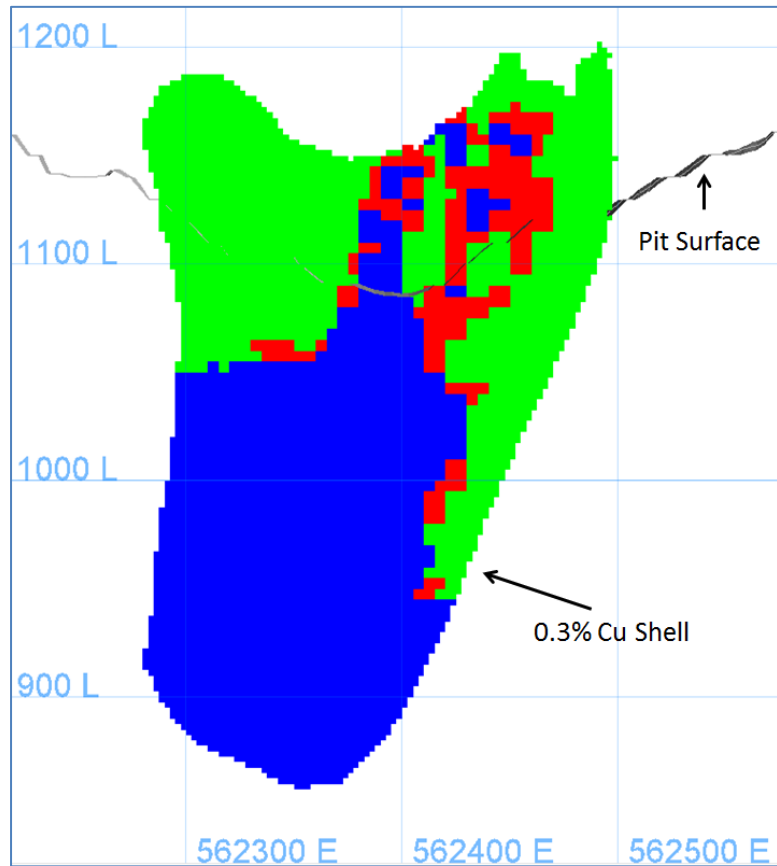
Schematic Kinsevere Strat Column	Domain code and name	Marker name + Code	Description	Katangan Correlates	Bm/Cc/Cpy/Cm
	SDOL Interbedded silicified dolomite and green siltstone	Green Siltstone GSL Silicified Dolomite SLD	Cream white to grey dolomites with dark silified bands/nodules, interbedded with green massive siltstones. Lower contact often structurally controlled. Strain partitioning between SDOL and LMU. Often contains entrained HBX (heterogeneous breccia zones).	Kambove Dolomite (R.2.3) Upper CMN	
	LMU Laminated Dolomite and Magnesite		Crinkly laminated, often coarsely re-crystallised and magnesite altered carbonate (likely after dolomite). Crystalline texture defined by cm scale magnesite/dolomite crystals with no apparent defined orientation. Carbonaceous laminae throughout.	Kambove Dolomite (R.2.3) Lower CMN	
	IDSH Interbedded dolomite and shale	Upper Nodular UNZ	Interbedded laminated dolomite and shale. Dolomites can be intensely magnesite altered. Especially in Central pit. Gradational unit into upper laminated dolomite unit. UNZ - Upper Nodular Zone defines the lower contact of this unit. Comprised of elongate and irregular carbonate concretions/pseudomorphs within a carbonaceous siltstone/shale.		
	ICSSL Calcareous Siltstone with Shale	Middle Nodular MNZ	Interbedded calcareous siltstone and shale. Siltstone often dolomitic with weak primary mineralisation. Shale interbeds often display strong veining with primary copper mineralisation - mostly as chalcocite. This unit can be quite thick throughout the Mashu region.	Shales Dolomites (R.2.3) (SD)	
	LSH Lower Shale Package	Grey Banded Shale GBS Lower Nodular LNZ	Shale dominated package; carbonaceous and variably magnesite altered. MNZ - S0 parallel, sheared carbonate pseudomorphs after evaporites. Frequently selectively replaced by Cu sulphides. GBS - Rhythmic, evenly spaced bands of alternating shale and calcareous siltstone. LNZ - Black shale with round circular, to ellipsoid shaped concretions (correlate; D-Strat). Lower contact with RSL often tectonic with abundant veining and mineralisation.	D.Strat	
	RSL Footwall Siltstone		Purple/red, ferruginous massive siltstone and/or green, sericitic massive siltstone. Both units can either be interbedded or gradational and contain; Ferroan dolomite veins, specular hematite, chalcocite near the upper contact with the LSH, mg-chlorite and talc.	R.A.T R1	
	RBX Footwall Breccia		Polymict heterogeneous breccia. Disseminated specular hematite.		

Drill hole information	<ul style="list-style-type: none"> • Within the database used, there are 876 Exploration drill holes (324 DD, 31 RC with DD tail and 560 RC) and 8,003 grade control drill holes (all RC). • No individual drill hole is material to the Mineral Resource estimate and hence this geological database is not supplied.
Data aggregation methods	<ul style="list-style-type: none"> • This is a Mineral Resource Statement and is not a report on exploration results hence no additional information is provided for this section. • No metal equivalents were used in the Mineral Resource estimation.
Relationship between mineralisation width and intercept lengths	<ul style="list-style-type: none"> • Mineralisation true widths are captured by interpreted mineralisation 3D wireframes. • Most drilling was at 50° to 60° angles in order to maximise true width intersections. • Geometry of mineralisation is interpreted as sub- vertical to vertical and as such current drilling allows true width of mineralisation to be determined.

Diagrams



Plan view of the Kinsevere deposit

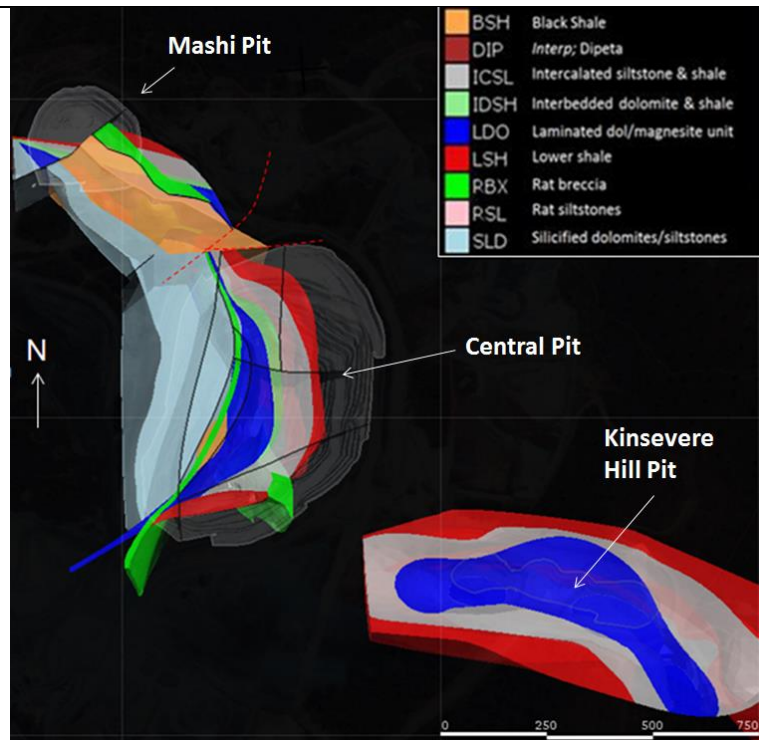


0.3% Cu Shell coded by Oxidation state (Green – Oxide / Red – TMO / Blue – Primary)

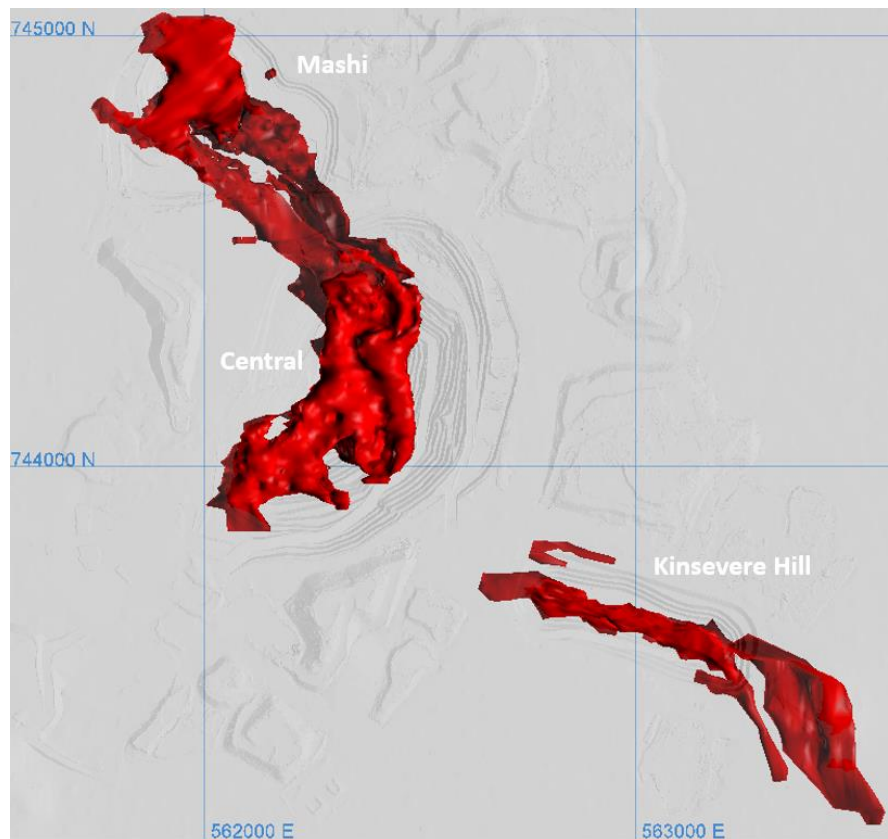
Typical cross section through Tshifufia (Central) pit showing mineralisation zones

Balanced reporting	<ul style="list-style-type: none"> This is a Mineral Resource Statement and is not a report on exploration results hence no additional information is provided for this section.
Other substantive exploration data	<ul style="list-style-type: none"> This is a Mineral Resource Statement and is not a report on exploration results hence no additional information is provided for this section.
Further work	<ul style="list-style-type: none"> The exploration focus will be within the Mine Lease and within a 50 km radius of the known deposit to explore for additional high-grade oxide material. RC and DD drilling as part of near mine extension is ongoing.
Section 3 Estimating and Reporting of Mineral Resources	
Database integrity	<ul style="list-style-type: none"> The following measures are in place to ensure database integrity: <ul style="list-style-type: none"> Drillhole data (RC and DD) is stored in two SQL databases with front end access provided by Geobank software. The grade control logging and assay data (RC) is managed by the onsite Geology team with support from the Group Technical Services database team in Melbourne. The exploration/resource logging data (RC and DD) is managed by the onsite Resource team with assay loading and support provided by the Group Technical Services database team in Melbourne. Data is entered directly into Geobank or Geobank Mobile using the database validation rules. These check for data consistency, missing intervals, overlaps, invalid codes and invalid values, thus maintaining data integrity. The databases offer secure storage and consistent data which is exposed to validation processes, standard logging and data recording lookup codes. The measures described above ensure that transcription or data entry errors are minimised. <ul style="list-style-type: none"> Data validation procedures include: <ul style="list-style-type: none"> Internal database validation systems and checks. Visual checks of exported drill holes in section and plan view, checking for accuracy of collar location against topography, and downhole trace de-surveying. External checks in Vulcan software prior to the data used for Mineral Resources. Checks on statistics, such as negative and unrealistic assay values. Any data errors were communicated to the Database team to be fixed in Geobank. Data used in the Mineral Resource has passed a number of validation checks both visual and software related prior to use in the Mineral Resource.
Site visits	<ul style="list-style-type: none"> The Competent Person visited on two occasions during 2017/18 (July 2017 and January 2018). Site visit work included: <ul style="list-style-type: none"> Visits to the ROM stockpiles, open pit mine, core yard, sample preparation and on-site assay laboratory. Discussions with geologists (mine and exploration), mine planning engineers and metallurgists.

<p>Geological interpretation</p>	<ul style="list-style-type: none"> • The geological interpretation is based on a combination of geological logging and geochemical assay data. There is a relatively high level of confidence in both geological and grade continuity within the upper zone of the deposit that is drilled to grade control density. There is less but still significant certainty in the geological interpretation in the lower portions of the Mineral Resource purely due to a lower drilling density however due to recent infill drilling and geological interpretation/knowledge the interpretation is considered reliable. • Both grade control RC and exploration DD and RC holes were used in the interpretation of the geological domains that are used in the Mineral Resource. • Wireframe solids were created for the Cu mineralisation (using a nominal 0.3% Cu cut-off). String envelopes were digitised along drill sections and were used to generate the wireframe surfaces. • Geological logging and geochemical data analysis was used to determine the lithological domains with wireframes created in Leapfrog Software. • Leapfrog software was used to create grade shell estimation domains for the following variables, Mg (using a 6% Mg cut-off), Ca (using a 9% Ca cut-off), Co (using a 0.08% Co cut-off) and Al (using a 2.5% Al cut-off). All cut-offs were determined from interrogation of histograms and probability plots • Indicator Kriging (IK) was used to determine oxide, TMO (transitional and mixed) and primary sulphide domains (or weathering domains), based on the CuAS/Cu ratio. • The resulting weathering, lithology, mineralisation (grade shell) domains were combined to code the drill hole data and the block model used for estimation. • On a local scale grade continuity is affected by minor stratiform lower grade zones that in places have been incorporated within the main deposit. This internal waste is better defined during the grade control drilling, and mined accordingly. Larger internal waste zones have been defined by wireframe interpretation. • Structural features (faults / fractures) provide an important control on the mineralisation and grade continuity.
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Plan View of Kinsevere Lithology Domains



Plan View of Kinsevere Cu>0.3% Mineralised Domains

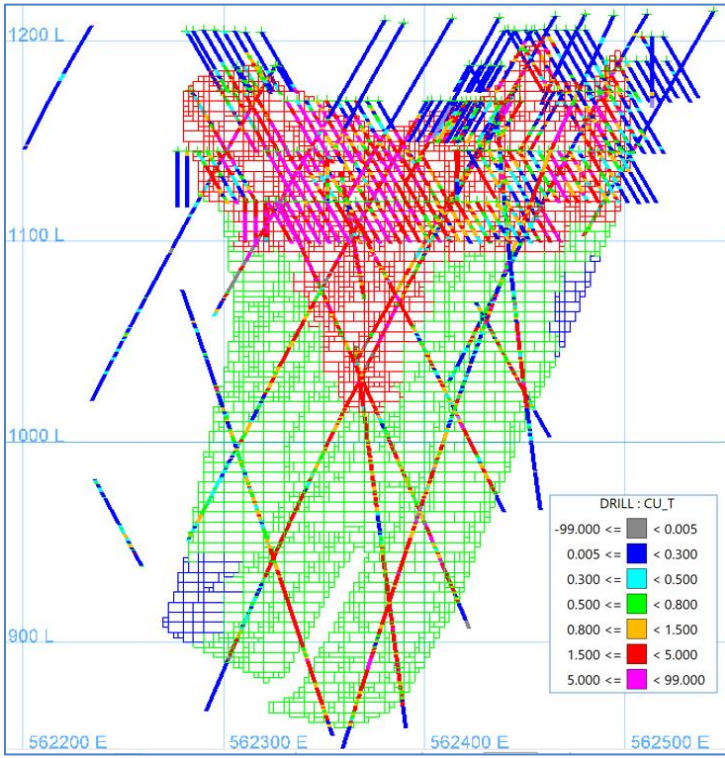
Dimensions

- The mineralisation strike length is approximately 1.3 km for the Tshifusia and Tshifufiamashi deposits while Kinsevere Hill has a 1km strike length. The mineralisation dips sub-vertically. Mineralisation extends to 400 m at depth and it can be up to 300m in width.

	<ul style="list-style-type: none"> • The mineralisation outcrops on Kinsevere Hill, and at the Tshifufiamashi deposit.
<p>Estimation and modelling techniques</p>	<ul style="list-style-type: none"> • Estimation applied mostly kriging interpolation within domains as outlined further in this section, and is considered appropriate for this style of mineralisation. • Mineral Resource modelling was conducted using Vulcan software. • Variograms updated for major elements including Cu, CuAS, Ratio, Ca, Mg, Al, Co, Mn and S. Variograms from 2017 were reviewed and unchanged for other elements. • The key estimation assumptions and parameters are as follows: <ul style="list-style-type: none"> ○ Cu, CuAS, CuAS/Cu (RATIO), Co, Al, Ca, Fe, Mg, Mn and S were estimated using Ordinary Kriging (OK). Uranium (U) was estimated by using an Inverse Distance to the power of 2 method (ID2). ○ RATIO was only estimated where the sample had a Cu > 0.2% and both a Cu and CuAS values were present, if criteria not met the RATIO value was recorded as absent. This Cu cut-off was applied due to reliability concerns (validated statistically) of the CuAS/Cu ratio as the primary assays approached detection limits. ○ Extreme grade values were managed by grade capping which was performed post compositing. Values greater than the selected cut value were set to the top cut (cap) value and used in the estimation. ○ Wireframes and surfaces of the topography; mineralised domains, together with IK domain are used to tag the drill holes and are used for statistical analysis and grade estimation. ○ Grade estimation was completed using a combination of hard and soft boundaries were applicable and based on interrogation of contact plots. A soft boundary is used between the estimation domains to model a diffuse grade profile across grade shell boundaries ○ Variables that were determined to not require independent grade shells were estimated within the Cu grade shell and generally sub-domained between the oxide, mixed and primary domains depending on the geostatistical analysis. ○ A series of local estimation domains (search ellipse and variogram orientations) were generated to honour the mineralisation strike variations thus improving the quality of the local estimate. ○ A composite length of 2m was used applied. Any residual intervals less than half the composite interval were appended to the previous sample interval. ○ No assumptions have been made about the correlation between variables. All variables are comparably informed and independently estimated. ○ Search parameters for Cu, CuAS, RATIO, Co, Al, Ca, Fe, Mg M and S estimate were derived from mineralisation domain variography. Quantitative Kriging Neighbourhood Analysis (QKNA) was undertaken on Cu to inform estimation parameters. U search parameters based on a generic search of 400 m x 400 m x 400 m, U grades higher than 250 ppm were distance limited to 20m. ○ First estimation pass search radius uses 80% of the variogram range. Over 90% of the blocks are generally informed in the first pass. The second search was set to 2 times the variogram range. ○ Minimum of 5 to 14 and a maximum of 12 to 30 samples (depending on element and/or domain) for each estimate. ○ The search neighbourhood was also limited to a maximum of 4 to 7 samples per drill hole depending on the domain to be estimated. ○ Discretisation was set to 4 x 8 x 2 (X, Y, Z). ○ Kriging variance (KV), kriging efficiency (KE) and kriging Slope of Regression (RS) of the Cu estimate were calculated during the estimation.

	<ul style="list-style-type: none"> • The 2017 and 2018 in-situ Mineral Resource models have been compared and show no material difference with metal content 2% higher for the 2017 model mainly due to drilling and subsequent re-interpretation in some areas. • The Comparison between the Mineral Resource and the mill feed grade is complicated by the operational strategy of treating high-grade ore and stockpiling lower-grade ore for later treatment. Generally there was a volume and metal reduction. • Kinsevere does not produce any by-products hence no assumptions regarding the recovery of by-products are made in the estimate or cut-off and reporting. • Parent block size of the Kinsevere block model is 10m x 20m x 5m with sub-blocking down to 2.5m. Estimation was into the parent block. The size of the blocks is appropriate to the spacing of drill holes. • No further assumptions have been made regarding modelling of selective mining units. • The block model and estimate has been validated in the following ways: <ul style="list-style-type: none"> ○ Visual checks in section and plan view against the drill holes. ○ Grade trend plots comparing the model against the drill holes.
Moisture	<ul style="list-style-type: none"> • Tonnes in the model have been estimated on a dry basis.
Cut-off parameters	<ul style="list-style-type: none"> • The oxide Mineral Resource has been reported above an acid soluble copper cut-off grade of 0.6% and an acid soluble copper to total copper ratio (Ratio) greater than or equal to 0.5. This is unchanged from the 2017 Mineral Resource. • For TMO Mineral Resource type, that defines transitional and mixed copper species (Ratio less than 0.5 and greater than or equal to 0.2), and has been split into oxide and sulphide components to match the expected processing streams. <ul style="list-style-type: none"> ○ Where Ratio is less than 0.5 and greater than 0.3, an acid soluble copper cut-off grade of 0.6% is applied (oxide). ○ Where Ratio is less than or equal to 0.3 and greater than 0.2, a total copper cut-off grade of 0.7% is applied (sulphide). ○ In 2017 all of TMO was reported above a total copper cut-off grade of 1.1% within a Ratio greater than or equal to 0.3 and less than 0.5. • The sulphide Mineral Resource has been reported above a total copper cut-off grade of 0.7% and a Ratio less than or equal to 0.2. This cut-off has dropped from the 2017 Mineral Resource which was 0.8% Cu due mainly to lower assumed processing costs. <ul style="list-style-type: none"> ○ The sulphide Mineral Resource is defined as having a Ratio less than 0.2 and this has changed from last year where less than 0.3 was used to define sulphides. • The reported Mineral Resources have also been constrained within a US\$3.51/lb pit shell. Both the sulphide and TMO cut offs have reduced this year due to a combination of lower assumed processing costs and increased recovery based on a potential ferric leach operation and all cut offs were assessed against a block by block Net Value calculation to confirm suitability. The reporting cut-off grade and the pit-shell price assumption are in line with MMG's policy on reporting of Mineral Resources which is prospective for future economic extraction.

	<p style="text-align: center;">Cross-section of Copper Mineral Resource model contained within the US\$3.51 lb pit shell</p>
Mining factors or assumptions	<ul style="list-style-type: none"> • Mining of the Kinsevere deposits is undertaken by the open pit method, which is expected to continue throughout the life of mine. • Mining selection has been considered in the calculation of cut-off grade parameters and in the constraint of mineral resources within the US\$3.51/lb pit shell. • No mining factors have been applied to the Mineral Resource.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> • The metallurgical process applied at the Kinsevere Operation applies acid leaching coupled with solvent extraction electro-winning (SXEW) technology to produce copper cathode plates for sale. • Resource cut-off grade reporting criteria is based on potential future economic extraction influenced by a ferric leach and flotation operation based on findings on a PFS study • Consideration of metallurgy has been included in the cut-off grade calculation, material type and in the construction of the US\$3.51/lb pit shell. • No metallurgical factors have been applied to the Mineral Resource.
Environmental factors or assumptions	<ul style="list-style-type: none"> • Environmental factors are considered in the Kinsevere life of asset work, which is updated annually and includes provision for mine closure. • The property is not subject to any environmental liabilities. • PAF and NAF criteria is controlled by the acid neutralising capabilities of the dolomitic CMN unit and the potential acid forming potential of the shale rich SD which is known to contain pyrite where a sulphur cut off is utilised.
Bulk density	<ul style="list-style-type: none"> • In-situ dry bulk density values are determined from 6,676 diamond core density measurements, 4 in-pit bulk sample measurements and 12 in-pit measurements from

	<p>specific lithologies.</p> <ul style="list-style-type: none"> • Bulk sample and in-pit measurements account for void spaces. • Bulk density was calculated using the wet and dry method: • $Bulk\ Density = \frac{Dry\ Sample\ Weight}{(Dry\ Sample\ Weight - Wet\ Sample\ Weight)}$ • Average in-situ bulk density values were assigned to the blocks within each domain. • There have only been minor immaterial changes from the values assigned for the 2017 Resource estimate within mineralised domains. • Weathering profiles were updated within the waste material for the 2018 Resource estimate and this has resulted in an approximate 10% increase in overall waste density from 2017. Waste weathering profiles were updated based on data from recent geotechnical drilling undertaken in the waste rock.
<p>Classification</p>	<ul style="list-style-type: none"> • Wireframes used for Mineral Resource classification are based on a combination of confidence in assayed grade, geological continuity and Kriging metrics (Kriging variance, efficiency and slope of regression). • In general, drilling within the Measured area is spaced from 15 x 15m to 25 x 25m, Indicated is 25 x 25m to 50 x 50m and Inferred ranges up to 80 x 80m or more. • The Mineral Resource classification reflects the Competent Persons view on the confidence and uncertainty of the Kinsevere Mineral Resource  <p>Cross section showing Kinsevere Mineral Resource classification and drilling density (Red-Measured, Green-Indicated, Blue-Inferred)</p>

Audits or reviews	<ul style="list-style-type: none"> • An external Mineral Resource audit was conducted by Jeremy Witley from MSA (The MSA Group) in June 2014. Overall the review stated that the estimate has been conducted in a competent and professional manner. Recommendations were incorporated into the 2015 Mineral Resource. • An independent audit of the Mineral Resource model was completed in October 2016 and November 2017, by Pennywise Pty Ltd as part of an audit on the results of the Sulphide Scoping Study and was commissioned by MMG Limited. No material errors were found. • MMG conducts annual internal reviews of Mineral Resource estimates. No significant issues were identified.
Discussion of relative accuracy / confidence	<ul style="list-style-type: none"> • Close-spaced grade control drilling within the Measured Mineral Resource areas provides suitable estimation on a local scale and supports the requirements of mining selectivity for the Kinsevere operation. • Estimates in the deeper primary copper mineralisation will not be as locally accurate, due to wider spaced drilling however the geological and grade interpretations are robust due to a high understanding of geological controls. The level of uncertainty is captured by the Indicated and Inferred Mineral Resource category. • Estimation of dry bulk density values needs to be evaluated to determine if achievable with the current number of samples. The method of assigning bulk density values is similar to the 2017 Mineral resource and is not considered to have any material impact on the reported mineralised tonnages. Density data is poorly sampled in waste rock and waste bulk density has increased by approximately 10% from 2017 due to re-interpretation of waste weathering domains.

4.2.1 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Mineral Resource statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Douglas Corley, confirm that I am the Competent Person for the Kinsevere Mineral Resource section of this Report and:

I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).

I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.

I am a Member of The Australasian Institute of Geoscientists

I have reviewed the relevant Kinsevere Mineral Resource section of this Report to which this Consent Statement applies.

I am a full time employee of MMG Ltd. at the time of the estimation.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest.

I verify that the Kinsevere Mineral Resource section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Kinsevere Mineral Resources.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Kinsevere Mineral Resources - I consent to the release of the 2018 Mineral Resources and Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

5/12/2018

Date:

Douglas Corley MAIG R.P.Geo. (#1505)

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Rex Berthelsen
Melbourne

Signature of Witness:

Witness Name and Residence: (e.g. town/suburb)

4.3 Ore Reserves - Kinsevere

4.3.1 Results

The 2018 Kinsevere Ore Reserves is based on the 2018 Mineral Resources model.

The 2018 Kinsevere Ore Reserves are summarised in Table 10.

Table 10 2018 Kinsevere Ore Reserves tonnage and grade (as at 30 June 2018)

Kinsevere Ore Reserves					
			Contained Metal		
	Tonnes (Mt)	Copper (% Cu)	Copper (% CuAS ¹)	Copper (^{'000} t)	Copper AS ¹ (^{'000} t)
Central Pit					
Proved	1.4	4.5	3.8	66	55
Probable	2.0	4.4	3.8	86	74
Central Pit Total	3.4	4.4	3.8	152	130
Mashi Pit					
Proved	0.4	4.1	3.6	18	16
Probable	1.6	3.7	3.3	58	51
Mashi Pit Total	2.0	3.8	3.3	76	66
Kinsevere Hill					
Proved	0.02	4.4	3.9	1	1
Probable	2.6	3.1	2.8	80	71
Kinsevere Hill Total	2.6	3.1	2.8	81	72
Stockpiles					
Probable	7.7	2.3	1.6	180	120
Stockpiles Total	7.7	2.3	1.6	180	120
Kinsevere Total	15.7	3.1	2.5	488	389

¹ AS= Acid Soluble

Cut-off grades were calculated at a US\$3.02/lb copper price and are based on a Net Value Script taking into account gangue acid consumption. The cut-off grade approximates 1.4% CuAS for ex-pit material and 1.0% CuAS for existing stockpiles reclaim.

Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors.

Contained metal does not imply recoverable metal.

The main differences from the 2017 Ore Reserves are:

- (i) Assumed copper price increased to US\$3.02/lb in 2018 from US\$2.96/lb in 2017.
- (ii) Mine and stockpile depletion.
- (iii) Mining dilution has increased to 10% in 2018 from 5% in 2017.
- (iv) Inclusion of 2.0 Mt of additional black shales stockpile material based on new drilling information; which now indicates they are processable.
- (v) Inclusion of 2.6 Mt of marginal oxide stockpile material. This stockpile is now economic when co-fed with the additional black shales stockpiles in the last few years of the production.

4.3.2 Ore Reserves JORC 2012 Assessment and Reporting Criteria

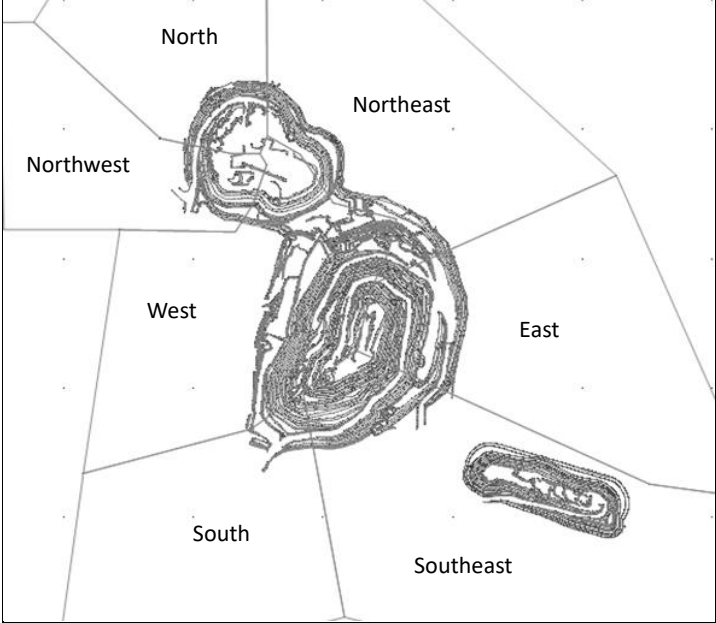
The following information provided in Table 11 complies with the 2012 JORC Code requirements specified by "Table-1 Section 4" of the Code. Each of the items in this table has been summarised as the basis for the assessment of overall Ore Reserves risk in the table below, with each of the risks related to confidence and/or accuracy of the various inputs into the Ore Reserves qualitatively assessed.

Table 11 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Kinsevere Ore Reserves 2018

Assessment Criteria	Commentary
Mineral Resource estimates for conversion to Ore Reserves	<ul style="list-style-type: none"> • The Mineral Resources are reported inclusive of the Ore Reserves. • The Ore Reserves includes Mineral Resources on stockpiles. • The sub-celled Mineral Resources block model named "kin_est_0518_bm_eng.bmf." and dated 26-06-2018 was used for pit optimisation and design purposes. • Mineral Resources block model based on Ordinary Kriging interpolation has been applied for the estimation of all elements. It has a parent block size of 10m x 20m x 5m with sub blocking down to 2.5m. • In-situ dry bulk density for the waste material has been changed since the 2017 Mineral Resources model to reflect more information obtained from updated weathering surfaces which extend into the non-mineralised areas. • Non-processable black shale stockpiles have been included in the Mineral Resources, based on new drill information; which now indicates they are processable.
Site visits	<ul style="list-style-type: none"> • The Competent Person visited the site in July 2017 and February, March, April, May and June, 2018. • Each visit consisted of discussions with relevant people associated with Ore Reserves modifying factors including geology, grade control, mine-to-mill reconciliation, mine dilution and mining recovery, geotechnical parameters, mine planning and mining operations, metallurgy, tailings and waste storage, and environmental and social disciplines. The outcomes from the visits have confirmed a common understanding of assumptions, calculation of the cut-off grades and development of the Life-of-Asset mine plan.
Study status	<ul style="list-style-type: none"> • The current mine and processing plant configuration has been in operation since September 2011. Ore Reserves are based on actual historical performance and cost data and projected based on the Life-of-Asset plan. • Life-of-Asset Low Case was produced as part of the MMG planning cycle. This Low Case informs the Ore Reserves – it demonstrates it is technically achievable and economically viable, while incorporating material Modifying Factors.
Cut-off parameters	<ul style="list-style-type: none"> • Breakeven cut-off grades were calculated at a US\$3.02/lb copper price and acid soluble to total copper ratio typically greater than or equal to 0.5. At a fixed gangue acid consumption of 16.5kg/t, the following approximate COG's are applied: <ul style="list-style-type: none"> ○ 1.4% CuAS for ex-pit material. ○ 1.0% CuAS for existing stockpiles reclaim. • A 1.0 Mt black shales stockpile with an acid soluble to total copper ratio of 0.4 has been included in the Ore Reserves based on new drilling information confirming that the CuAS grades are above cut-off grade. • The ex-pit COG estimates are based on a Net Value Script (NVS) calculation that

Assessment Criteria	Commentary
	<p>incorporates commodity price assumptions, gangue acid consumption and costs associated with current operating conditions.</p> <ul style="list-style-type: none"> • The NVS routine identifies material that is both suitable and potentially economic for processing in the Mineral Resources Model. This material is then considered for inclusion in the Ore Reserves process. • For the cost assumptions please see the "Costs" section. • For the price assumptions please see the "Revenue factors" section.
Mining factors or assumptions	<ul style="list-style-type: none"> • The method for Ore Reserves estimation included: pit optimisation, final pit and phase designs, consideration of mine and mill schedule, all modifying factors and economic valuation. • Kinsevere mine is an open pit operation that is mining and processing oxide copper ore. The operation uses a contract mining fleet of excavators and both rigid body and articulated dump trucks along with a fleet of ancillary equipment. • This mining method is appropriate for the style and size of the mineralisation. • The pit optimisation was based on the 2018 Mineral Resources block model and the strategy for the final pit selection was based on a revenue factor 1 (RF=1.0). The RF 1.0 pit shell is used across all assets in the MMG Group. Final pit designs incorporating further practical mining considerations were carried out using these optimisation shells. • Assumed mining dilution is 10% (was 5% in 2017 Ore Reserves) and mining recovery is maintained at 95%. Dilution modelling and reconciliation data supports these assumptions. A thorough mine-to-mill reconciliation review is proposed for 2019 to identify opportunities to reduce mining dilution. • Minimum mining width (bench size) is typically in excess of 45m but is ~35m in some isolated areas during stage development. • No Inferred Mineral Resources material has been included in optimisation and/or Ore Reserves reporting. • All required infrastructure is in place. A minor increase in mining rate is planned for 2018/2019, this increase is considered to be within the capacity of the existing fleet and mining contractor capability. This is a result of the aforementioned increase in Mineral Resources Model waste density. • The slope guidelines used for the 2018 Kinsevere Ore Reserves are as follows:

Assessment Criteria	Commentary																																																																																																											
	<table border="1" data-bbox="485 315 1286 1496"> <thead> <tr> <th data-bbox="485 315 600 427">Design Sector</th> <th data-bbox="600 315 727 427">Weathering Code</th> <th data-bbox="727 315 839 427">Overall Wall Angle (degrees)</th> <th data-bbox="839 315 951 427">Interamp Angle (degrees)</th> <th data-bbox="951 315 1062 427">Bench Face Angle (degrees)</th> <th data-bbox="1062 315 1142 427">Bench Height (meters)</th> <th data-bbox="1142 315 1286 427">Berm Width (m)</th> </tr> </thead> <tbody> <tr> <td data-bbox="485 427 600 775" rowspan="4">West Domain</td> <td data-bbox="600 427 727 472">W4 (free dig)</td> <td data-bbox="727 427 839 472">-</td> <td data-bbox="839 427 951 472">35</td> <td data-bbox="951 427 1062 472">50</td> <td data-bbox="1062 427 1142 472">10</td> <td data-bbox="1142 427 1286 472">6</td> </tr> <tr> <td data-bbox="600 472 727 629">W3 (free dig)</td> <td data-bbox="727 472 839 629">no greater than 27 degrees</td> <td data-bbox="839 472 951 629">-</td> <td data-bbox="951 472 1062 629">45</td> <td data-bbox="1062 472 1142 629">10</td> <td data-bbox="1142 472 1286 629">minimum of 6m - adjust bench width to meet Overall WALL angle criteria</td> </tr> <tr> <td data-bbox="600 629 727 707">W2 (drill/blast)</td> <td data-bbox="727 629 839 707">-</td> <td data-bbox="839 629 951 707">40</td> <td data-bbox="951 629 1062 707">70</td> <td data-bbox="1062 629 1142 707">10</td> <td data-bbox="1142 629 1286 707">8</td> </tr> <tr> <td data-bbox="600 707 727 775">W1/0 (drill/blast)</td> <td data-bbox="727 707 839 775">-</td> <td data-bbox="839 707 951 775">40</td> <td data-bbox="951 707 1062 775">70</td> <td data-bbox="1062 707 1142 775">10</td> <td data-bbox="1142 707 1286 775">8</td> </tr> <tr> <td data-bbox="485 775 600 1021" rowspan="4">North</td> <td data-bbox="600 775 727 819">W4 (free dig)</td> <td data-bbox="727 775 839 819">-</td> <td data-bbox="839 775 951 819">35</td> <td data-bbox="951 775 1062 819">50</td> <td data-bbox="1062 775 1142 819">10</td> <td data-bbox="1142 775 1286 819">6</td> </tr> <tr> <td data-bbox="600 819 727 887">W3 (free dig)</td> <td data-bbox="727 819 839 887">-</td> <td data-bbox="839 819 951 887">30</td> <td data-bbox="951 819 1062 887">50</td> <td data-bbox="1062 819 1142 887">10</td> <td data-bbox="1142 819 1286 887">9</td> </tr> <tr> <td data-bbox="600 887 727 954">W2 (drill/blast)</td> <td data-bbox="727 887 839 954">-</td> <td data-bbox="839 887 951 954">40</td> <td data-bbox="951 887 1062 954">70</td> <td data-bbox="1062 887 1142 954">10</td> <td data-bbox="1142 887 1286 954">8</td> </tr> <tr> <td data-bbox="600 954 727 1021">W1/0 (drill/blast)</td> <td data-bbox="727 954 839 1021">-</td> <td data-bbox="839 954 951 1021">40</td> <td data-bbox="951 954 1062 1021">70</td> <td data-bbox="1062 954 1142 1021">10</td> <td data-bbox="1142 954 1286 1021">8</td> </tr> <tr> <td data-bbox="485 1021 600 1267" rowspan="4">Northeast</td> <td data-bbox="600 1021 727 1066">W4 (free dig)</td> <td data-bbox="727 1021 839 1066">-</td> <td data-bbox="839 1021 951 1066">35</td> <td data-bbox="951 1021 1062 1066">50</td> <td data-bbox="1062 1021 1142 1066">10</td> <td data-bbox="1142 1021 1286 1066">6</td> </tr> <tr> <td data-bbox="600 1066 727 1133">W3 (free dig)</td> <td data-bbox="727 1066 839 1133">-</td> <td data-bbox="839 1066 951 1133">40</td> <td data-bbox="951 1066 1062 1133">60</td> <td data-bbox="1062 1066 1142 1133">10</td> <td data-bbox="1142 1066 1286 1133">6</td> </tr> <tr> <td data-bbox="600 1133 727 1200">W2 (drill/blast)</td> <td data-bbox="727 1133 839 1200">-</td> <td data-bbox="839 1133 951 1200">40</td> <td data-bbox="951 1133 1062 1200">70</td> <td data-bbox="1062 1133 1142 1200">10</td> <td data-bbox="1142 1133 1286 1200">8</td> </tr> <tr> <td data-bbox="600 1200 727 1267">W1/0 (drill/blast)</td> <td data-bbox="727 1200 839 1267">-</td> <td data-bbox="839 1200 951 1267">40</td> <td data-bbox="951 1200 1062 1267">70</td> <td data-bbox="1062 1200 1142 1267">10</td> <td data-bbox="1142 1200 1286 1267">8</td> </tr> <tr> <td data-bbox="485 1267 600 1496" rowspan="4">East/ Southeast / South/ Northwest</td> <td data-bbox="600 1267 727 1312">W4 (free dig)</td> <td data-bbox="727 1267 839 1312">-</td> <td data-bbox="839 1267 951 1312">35</td> <td data-bbox="951 1267 1062 1312">50</td> <td data-bbox="1062 1267 1142 1312">10</td> <td data-bbox="1142 1267 1286 1312">6</td> </tr> <tr> <td data-bbox="600 1312 727 1357">W3 (free dig)</td> <td data-bbox="727 1312 839 1357">-</td> <td data-bbox="839 1312 951 1357">40</td> <td data-bbox="951 1312 1062 1357">60</td> <td data-bbox="1062 1312 1142 1357">10</td> <td data-bbox="1142 1312 1286 1357">6</td> </tr> <tr> <td data-bbox="600 1357 727 1424">W2 (drill/blast)</td> <td data-bbox="727 1357 839 1424">-</td> <td data-bbox="839 1357 951 1424">43</td> <td data-bbox="951 1357 1062 1424">70</td> <td data-bbox="1062 1357 1142 1424">10</td> <td data-bbox="1142 1357 1286 1424">7</td> </tr> <tr> <td data-bbox="600 1424 727 1496">W1/0 (drill/blast)</td> <td data-bbox="727 1424 839 1496">-</td> <td data-bbox="839 1424 951 1496">46</td> <td data-bbox="951 1424 1062 1496">70</td> <td data-bbox="1062 1424 1142 1496">10</td> <td data-bbox="1142 1424 1286 1496">6</td> </tr> </tbody> </table> <ul data-bbox="544 1536 1501 1774" style="list-style-type: none"> ○ These guidelines take into account observed performance of the current exposures at Kinsevere and potential failure modes that could occur at bench, interamp and overall wall scale at Kinsevere. ○ Interamp and overall wall factors of safety from limit equilibrium analysis are in excess of 1.2. ○ The design sectors highlighted in the table above can be seen in plan view in the following figure. 	Design Sector	Weathering Code	Overall Wall Angle (degrees)	Interamp Angle (degrees)	Bench Face Angle (degrees)	Bench Height (meters)	Berm Width (m)	West Domain	W4 (free dig)	-	35	50	10	6	W3 (free dig)	no greater than 27 degrees	-	45	10	minimum of 6m - adjust bench width to meet Overall WALL angle criteria	W2 (drill/blast)	-	40	70	10	8	W1/0 (drill/blast)	-	40	70	10	8	North	W4 (free dig)	-	35	50	10	6	W3 (free dig)	-	30	50	10	9	W2 (drill/blast)	-	40	70	10	8	W1/0 (drill/blast)	-	40	70	10	8	Northeast	W4 (free dig)	-	35	50	10	6	W3 (free dig)	-	40	60	10	6	W2 (drill/blast)	-	40	70	10	8	W1/0 (drill/blast)	-	40	70	10	8	East/ Southeast / South/ Northwest	W4 (free dig)	-	35	50	10	6	W3 (free dig)	-	40	60	10	6	W2 (drill/blast)	-	43	70	10	7	W1/0 (drill/blast)	-	46	70	10	6
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Assessment Criteria	Commentary																	
																		
<p>Metallurgical factors or assumptions</p>	<ul style="list-style-type: none"> Kinsevere is an operating mine. The metallurgical process is a hydrometallurgical process involving grinding, tank leaching, counter-current decantation (CCD) washing, solvent extraction and electrowinning. The acid leach process has been operating successfully since start-up in September 2011. Copper recovery is determined by the equation: $Cu\ recovery\ (\%) = (0.96 * CuAS) / Cu$ <p>where CuAS refers to the acid soluble copper content of the ore which is determined according to a standard test. The CuAS value has historically been about 80% of the total copper value though the exact percentage varies with the ore type. Much of the non-acid soluble copper is present in sulphides which are not effectively leached in the tank leaching stage.</p> The reconciliation between expected and actual recovery is checked each month. The following table summarizes the outcomes for the last four quarterly periods. <table border="1" data-bbox="624 1529 1343 1778"> <thead> <tr> <th rowspan="2">Period</th> <th colspan="2">Recovery of Acid Soluble Copper (%)</th> </tr> <tr> <th>Predicted</th> <th>Actual</th> </tr> </thead> <tbody> <tr> <td>Q3 2017</td> <td>95.1</td> <td>96.2</td> </tr> <tr> <td>Q4 2017</td> <td>95.1</td> <td>97.3</td> </tr> <tr> <td>Q1 2018</td> <td>96.0</td> <td>96.7</td> </tr> <tr> <td>Q2 2018</td> <td>96.0</td> <td>97.1</td> </tr> </tbody> </table> The main deleterious components of the ore are carbonaceous (black) shales which increase solution losses in the washing circuit and dolomite which increases acid consumption in the leaching process. The effect of black shale is currently controlled by blending which is used to limit the percentage of this component in the feed to less than 35%. Total gangue acid consumption for Central and Kinsevere Hill South ore has been estimated based on the historic average consumption rates of 16.5kg/t of oxide 	Period	Recovery of Acid Soluble Copper (%)		Predicted	Actual	Q3 2017	95.1	96.2	Q4 2017	95.1	97.3	Q1 2018	96.0	96.7	Q2 2018	96.0	97.1
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Q4 2017	95.1	97.3																
Q1 2018	96.0	96.7																
Q2 2018	96.0	97.1																

Assessment Criteria	Commentary
	<p>ore.</p> <ul style="list-style-type: none"> • Kinsevere Hill North and Mashi contains higher levels of dolomite, and hence results in a higher acid consumption than Central ore. For this reason, based on laboratory testwork, the gangue acid consumption (kg/t ore) for Kinsevere Hill North and Mashi, where Ca \geq1%, is calculated as $43.8 \times \text{Ca} - 27.3$. For ore containing $<1\%$ Ca, the gangue acid consumption is assumed to be equal to the historical average of 16.5kg/t. • To prevent process issues, ore feed to the mill is blended to ensure the gangue acid consumption does not exceed 35kg/t. • For Ore Reserves, a processing capacity of 2.4Mtpa of ore and an electrowinning capacity of 80ktpa of copper cathode has been assumed. Both mill throughput and cathode production rates have been demonstrated as sustainable. • Kinsevere mine does not produce any by-products.
Environmental	<ul style="list-style-type: none"> • The 2018 Mining Code and Regulations introduced new pollution, installation and environmental taxes. The assessment of the new Code was still being assessed at the time of writing this document. • An update to the site's licence to operate, the Environment and Social Impact Assessment (ESIA), is underway to cover oxide operational changes including surface water management, stockpile management, pit extensions, and, new landfill. The 2019 ESIA will comply with the new DRC Mining Code and supporting Regulations/Schedules. It is due for submission to the Regulator in January 2019. Initial stakeholder consultation was conducted in Q2 2018. • A review of geochemical analysis of mining waste materials assessed over a two year period, was undertaken during 2017 to confirm the classification of Potential Acid Forming (PAF) material. The review resulted in a change to the PAF classification. The updated classification has reduced the volume of potentially acid generating material (separating non-acid generating materials from potentially acid generating materials), preserving clean waste for construction and rehabilitation requirements. • A review of the conceptual surface water management plan for the short and medium term has been completed. Remediation and civil works are planned to commence during the 2018 dry season. • Existing tailings storage facility (TSF 2) has design capacity to meet the 2018 Ore Reserves requirements.
Infrastructure	<ul style="list-style-type: none"> • The Kinsevere mine site is well established with the following infrastructure in place: <ul style="list-style-type: none"> ○ The plant is operational. ○ Labour is mostly sourced from Lubumbashi and surrounding villages with some expatriate support. There is an existing accommodation facility onsite. ○ There is sufficient water for the processing. ○ Copper cathode is transported off-site by truck. ○ Site has an access road that is partially sealed. ○ There is power supply from the national grid and from onsite generators. ○ The Ore Reserves do not require any additional land for expansion. ○ Tailings Storage Facility in place and future lifts are planned for. • Grid power in country can be intermittent; mitigation management is through

Assessment Criteria	Commentary
	<p>diesel based power generation. Future grid power availability is forecast to improve.</p> <ul style="list-style-type: none"> • Timely dewatering of the mining areas continues to be an important aspect of mining operations.
Costs	<ul style="list-style-type: none"> • Kinsevere is an operating mine and has historical costs that have been used to inform the 2018 Kinsevere Budget (January 2018 to December 2018), with the exception of the contract mining costs and costs arising from the new DRC Mining Code. • Mining costs are based on the 2018 contract mining costs. • Costs were added for items arising from the 2018 DRC Mining Code, namely: <ul style="list-style-type: none"> ○ Increased import duties. ○ Increased Special Tax on Expatriate Salaries. • Transportation charges used in the valuation are based on the actual invoice costs that MMG are charged by the commodity trading company per the agreement. • The processing costs include calculated gangue acid consumption. • The final product contains no deleterious elements. • US dollars have been used thus no exchange rates have been applied. • Weathering profiles have been updated to model in-pit blasting to inform the mining costs. • Since the final product is copper cathode (Grade A non LME registered) there are no additional treatment or refining or any other similar charges. • Sustaining capital costs have been included in the pit optimisation. The sustaining capital costs are principally related to the tailings storage facility lift construction and the process plant. The inclusion or exclusion of these costs in the Ore Reserves estimation is based on accepted industry practice. • Allowances have been made for royalties at the increased rate legislated in the 2018 DRC Mining Code. • A cash flow model was produced based on the mine and processing schedule and the aforementioned costs. • The Ore Reserves estimation has been based on the abovementioned costs.
Revenue factors	<ul style="list-style-type: none"> • For cost assumptions see section above – “Costs” • The assumed copper price is US\$3.02/lb which is used to inform the cut-off parameters (see cut-off section above). These prices are provided by MMG corporate, approved by the MMG Board, and are based on external company broker consensus and internal MMG analysis.
Market assessment	<ul style="list-style-type: none"> • MMG considers that the outlook for the copper price over the medium and longer term is positive, supported by further steady demand growth which is expected to exceed increases in supply. • Global copper consumption growth will continue to be underpinned by rising consumption in China and the developing countries in Asia as these nations invest in infrastructure such as power grids, commercial and residential property, motor vehicles and transportation networks and consumer appliances such as air

Assessment Criteria	Commentary
	<p>conditioners.</p> <ul style="list-style-type: none"> • Global copper demand will also rise as efforts are made to reduce greenhouse gas emissions through greater adoption of renewable energy sources for electricity supply and automotive power. • Supply growth is expected to be constrained by a lack of new mine projects ready for development and the requirement for significant investment to maintain existing production levels at some operations. • There is a life of mine off-take agreement with a trading company in place for all of Kinsevere’s copper cathode production. The off-take arrangement has been in place since the commencement of cathode production at site and has operated effectively. There is no reason to expect any change to this in future.
Economic	<ul style="list-style-type: none"> • The costs are based on historical actuals, the 2018 Kinsevere Budget and current contractor mining costs. • Revenues are based on historical and contracted realised costs and copper price as reported in the cut-off parameters section. • The Ore Reserves financial model demonstrates the mine has a substantially positive NPV. • The discount rate is in line with MMG’s corporate economic assumptions and is considered to be appropriate for the location, type and style of operation. • Standard sensitivity analyses were undertaken for the Ore Reserves work and support that the Ore Reserves estimate are robust.
Social	<ul style="list-style-type: none"> • Compensation has been paid and relocation of persons from the Kinsevere mining lease PE528 Mpundu lands is near complete. Existing processes are in place to oversee the compensation process, determine rates and deal with compensation disputes. The social development team in coordination with the Kipushi regional authorities (independent arbiter), have a defined process for engaging with communities and ensuring successful relocation outcomes are achieved. • A risk assessment was undertaken to assess the impact of the 2018 DRC Mining Code. A key social requirement was the establishment of a “Board of Trustees” responsible for managing the Endowment for the contribution to the community development projects, amounting to 0.3% of the turnover of the fiscal year. MMG will hold two positions on the board. • Social and Security teams are working together to mitigate security threats resulting from theft and other illegal activities by engaging the community to raise awareness of issues and garner support, improving security at the site. • Officials continue to be engaged in the management of artisanal miners from the region and site. Improved security management has been implemented in response to ongoing risk of incursion. • Being an election year MMG is avoiding matters of a political nature.
Other	<ul style="list-style-type: none"> • MMG has a Contrat d’Amodiation (Lease Agreement) with Gécamines to mine and process ore from the Kinsevere Project until 2024. A renewal application process for 15 year extension shall be submitted to DRC regulatory at least 1 year and no more than 5 years before the expiry date. • The PE 528 permit covers the three major deposits of Tshifufiamashi, Tshifufia and

Assessment Criteria	Commentary
	<p>Kinsevere Hill/Kilongo.</p> <ul style="list-style-type: none"> • A Contrat d'Amodiation is provided for under the DRC Mining Code, enacted by law No 007/2002 of July 11, 2002. • A conversion of the neighbouring PR7274 to an exploitation permit was completed in 2018. Tenement amalgamation (of PE528 and PE7274).
Classification	<ul style="list-style-type: none"> • The Ore Reserves classification is based on the JORC 2012 Code. The basis for the classification was the Mineral Resources classification and cut-off grade. The ex-pit material classified as Measured and Indicated Mineral Resources and is above 1.4% CuAS with an acid soluble to total copper ratio greater than or equal to 0.5, and is demonstrated to be economic to process, is classified as Proved and Probable Ore Reserves respectively. • Existing stockpile material at Kinsevere is classified as Indicated. Indicated Mineral Resources above 1.0% CuAS with an acid soluble to total copper ratio greater than or equal to 0.5, and is demonstrated to be economic to process, is classified as Probable Ore Reserves. • 1.0 Mt of Indicated Mineral Resources on a black shales stockpile with an acid soluble to total copper ratio of 0.4 has been included in the Ore Reserves based on new drill information confirming that the CuAS grade is above cut-off grade. • The Ore Reserves do not include any Inferred Mineral Resources.
Audit or Reviews	<ul style="list-style-type: none"> • An external Ore Reserves audit was completed in 2018 on the 2017 Ore Reserves. The work was carried out by AMC Consultants. Whilst some minor improvements were suggested, no material issues were identified. • The next external Ore Reserves audit is planned for completion in 2021 on the 2020 Ore Reserves.
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> • The most significant factors affecting confidence in the Ore Reserves are: <ul style="list-style-type: none"> ○ Variations to MMG's application of the 2018 DRC Mining Code. ○ Reliability of the grid power supply. ○ Gangue acid consumption estimates. ○ Increase in operating costs for mining and processing. ○ Geotechnical risk related to slope stability. ○ Effective management of both ground and surface water.

4.3.3 Expert Input Table

A number of persons have contributed key inputs to the Ore Reserves determination. These are listed below in Table 12.

In compiling the Ore Reserves the Competent Person has reviewed the supplied information for reasonableness, but has relied on this advice and information to be correct.

Table 12 Contributing experts – Kinsevere Mine Ore Reserves

EXPERT PERSON / COMPANY	AREA OF EXPERTISE
Doug Corley, Principal Resource Geologist MMG Ltd (Melbourne)	Mineral Resources model Stockpile Tonnes and Grade
Nigel Thiel, Principal Metallurgist, MMG Ltd (Melbourne)	Metallurgy
Christian Holland, Principal Geotechnical Engineering, MMG Ltd (Melbourne)	Geotechnical parameters
Dean Basile, Principal Mining Engineer, Mining One Consultants (Melbourne)	Whittle optimisation and review of Ore Reserves estimate
Jodi Wright, Principal Mining Engineer- Open Cut, MMG Ltd (Melbourne)	Mining costs, pit designs, mine and mill schedules, Ore Reserves estimate
Kinsevere Geology department	Production reconciliation
David Machin, Principal Water and Tailings Engineer, MMG Ltd (Melbourne)	Tailings Capacity
Knight Piésold	Tailings dam design
Claire Beresford, Senior Analyst, Business Evaluation, MMG Ltd (Melbourne)	Economic Assumptions and evaluation
Melanie Stutsel, General Manager Safety, Environment and Social Performance, MMG Ltd (Melbourne)	Environment
Narelle Woolfe, Group Manager Social Performance, MMG Ltd (Melbourne)	Social
Steve Whitehead, General Manager Marketing, MMG Ltd (Melbourne)	Marketing

4.3.4 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Ore Reserve statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Jodi Wright, confirm that I am the Competent Person for the Kinsevere Ore Reserves section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a Member of The Australasian Institute of Mining and Metallurgy
- I have reviewed the relevant Kinsevere Ore Reserves section of this Report to which this Consent Statement applies.

I am a full time employee of MMG Pty Ltd.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest.

I verify that the Kinsevere Ore Reserves section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Kinsevere Ore Reserves.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Kinsevere Ore Reserves - I consent to the release of the 2018 Mineral Resources and Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

5/12/2018

Jodi Wright MAusIMM(CP) (#209552)

Date:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Nicola Logan
Melbourne, VIC

Signature of Witness:

Witness Name and Residence: (e.g. town/suburb)

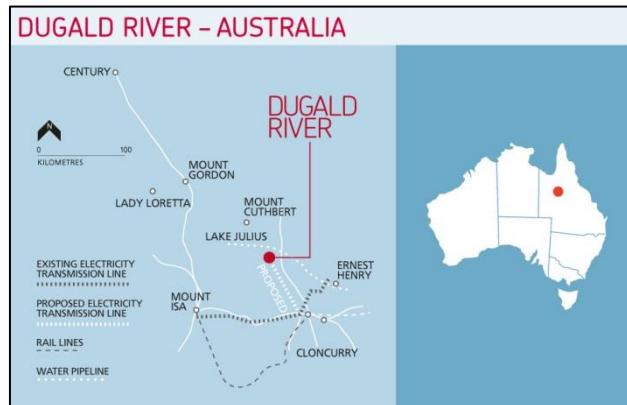
5 DUGALD RIVER PROJECT

5.1 Introduction and setting

The Dugald River project is located in northwest Queensland approximately 65km northwest of Cloncurry and approximately 85km northeast of Mount Isa (Figure 5-1). It is approximately 11km (by the existing access road) from the Burke Developmental Road, which runs from Cloncurry to Normanton.

It is an underground zinc-lead-silver deposit containing 56.5MT at 12.5% zinc, 1.8% lead and 27 g/t Ag (as of 30 June 2018 at a \$146/t NSR cut-off) and is wholly owned by a subsidiary of MMG Limited.

Figure 5-1 Dugald River project location



5.2 Mineral Resources – Dugald River

5.2.1 Results

The 2018 Dugald River Mineral Resources are summarised in Table 13. The Mineral Resource has been depleted to account for mining of ore by way of underground development of ore drives and stope production. The 2018 Mineral Resource has been reported above an A\$146/t NSR (*net smelter return*) cut-off.

Table 13 2018 Dugald River Mineral Resource tonnage and grade (as at 30 June 2018)

Dugald River Mineral Resource											
	Tonnes (Mt)	Copper (% Cu)	Zinc (% Zn)	Lead (% Pb)	Silver (g/t Ag)	Gold (g/t Au)	Contained Metal				
							Copper (‘000)	Zinc (‘000)	Lead (‘000)	Silver (Moz)	Gold (MoZ)
Primary Zinc¹											
Measured	8.7		12.9	2.3	73			1,132	204	20	
Indicated	24		12.6	2.0	30			3,071	487	23	
Inferred	24		12.1	1.5	8			2,835	346	6	
Total	57		12.4	1.8	27			7,038	1,037	49	
Stockpiles											
Measured	0.2		8.7	1.4	39			14	2.2	0.2	
Total	0.2		8.7	1.4	39			14	2.2	0.2	
Total Primary Zinc	57		12.4	1.8	27			7,052	1,039	49	
Primary Copper²											
Inferred	6.6	1.5				0.2	99				0.04
Total	6.6	1.5				0.2	99				0.04
Dugald River Total							99	7,052	1,039	49	0.04

¹ \$146/t NSR Cut-off, in-situ (less depletion and oxide material)

² 1% Cu Cut-off, in-situ (less depletion and oxide material)

Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors.

Contained metal does not imply recoverable metal

5.3 Mineral Resources JORC 2012 Assessment and Reporting Criteria

The following information provided in Table 14 complies with the 2012 JORC Code requirements specified by "Table-1 Section 1-3" of the Code.

Table 14 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Dugald River Mineral Resource 2018

Criteria	Status																																																																																																									
Section 1 Sampling Techniques and Data																																																																																																										
Sampling techniques	<ul style="list-style-type: none"> Diamond drilling (DD) was used to obtain an average 1m sample length while still respecting geological contacts. DD core was sampled either whole, ¾, ½, ¼. Once samples are selected by a geologist the samples are marked and the allocated sample ID's stored in the database. Table below shows samples collected at Dugald River for use in the Mineral Resource model by drill type, hole size and sample type. <table border="1" style="margin-left: 40px;"> <thead> <tr> <th>Drill Type</th> <th>Hole Size</th> <th>Sample Type</th> <th>Metres</th> <th>% of Total</th> </tr> </thead> <tbody> <tr> <td rowspan="20">DD & DD_UG</td> <td rowspan="2">BQ</td> <td>Whole Core</td> <td>254</td> <td>0.3%</td> </tr> <tr> <td>1/2 Core</td> <td>114</td> <td>0.1%</td> </tr> <tr> <td rowspan="2">LTK60</td> <td>Whole Core</td> <td>3,782</td> <td>4.2%</td> </tr> <tr> <td>1/2 Core</td> <td>2,903</td> <td>3.2%</td> </tr> <tr> <td rowspan="2">NQ3</td> <td>Whole Core</td> <td>6</td> <td>0.0%</td> </tr> <tr> <td>1/2 Core</td> <td>1,203</td> <td>1.3%</td> </tr> <tr> <td rowspan="3">NQ</td> <td>Whole Core</td> <td>3,139</td> <td>3.5%</td> </tr> <tr> <td>1/2 Core</td> <td>206</td> <td>0.2%</td> </tr> <tr> <td>1/4 Core</td> <td>42</td> <td>0.0%</td> </tr> <tr> <td rowspan="3">NQ2</td> <td>Whole Core</td> <td>21,156</td> <td>23.6%</td> </tr> <tr> <td>1/2 Core</td> <td>33,080</td> <td>36.9%</td> </tr> <tr> <td>1/4 Core</td> <td>51</td> <td>0.1%</td> </tr> <tr> <td rowspan="4">HQ</td> <td>Whole Core</td> <td>2,147</td> <td>2.4%</td> </tr> <tr> <td>3/4 core</td> <td>409</td> <td>0.5%</td> </tr> <tr> <td>1/2 Core</td> <td>1,014</td> <td>1.1%</td> </tr> <tr> <td>1/4 Core</td> <td>296</td> <td>0.3%</td> </tr> <tr> <td>HQ3</td> <td>1/2 Core</td> <td>4,885</td> <td>5.4%</td> </tr> <tr> <td rowspan="2">PQ</td> <td>Whole Core</td> <td>255</td> <td>0.3%</td> </tr> <tr> <td>Unknown</td> <td>Whole Core</td> <td>1,750</td> <td>2.0%</td> </tr> <tr> <td></td> <td></td> <td>1/2 Core</td> <td>444</td> <td>0.5%</td> </tr> <tr> <td></td> <td colspan="2"><i>DD – Sample Method not Recorded</i></td> <td>1,264</td> <td>1.4%</td> </tr> <tr> <td></td> <td colspan="2" style="text-align: center;">DD TOTAL</td> <td>77,136</td> <td></td> </tr> <tr> <td rowspan="3">RC</td> <td>100 & 150 mm</td> <td>Chips</td> <td>1,720</td> <td>1.9%</td> </tr> <tr> <td>Unknown</td> <td>Chips</td> <td>9,554</td> <td>10.7%</td> </tr> <tr> <td colspan="2" style="text-align: center;">RC TOTAL</td> <td>11,274</td> <td></td> </tr> <tr> <td>TOTAL</td> <td colspan="2"></td> <td>89,674</td> <td>100%</td> </tr> </tbody> </table>	Drill Type	Hole Size	Sample Type	Metres	% of Total	DD & DD_UG	BQ	Whole Core	254	0.3%	1/2 Core	114	0.1%	LTK60	Whole Core	3,782	4.2%	1/2 Core	2,903	3.2%	NQ3	Whole Core	6	0.0%	1/2 Core	1,203	1.3%	NQ	Whole Core	3,139	3.5%	1/2 Core	206	0.2%	1/4 Core	42	0.0%	NQ2	Whole Core	21,156	23.6%	1/2 Core	33,080	36.9%	1/4 Core	51	0.1%	HQ	Whole Core	2,147	2.4%	3/4 core	409	0.5%	1/2 Core	1,014	1.1%	1/4 Core	296	0.3%	HQ3	1/2 Core	4,885	5.4%	PQ	Whole Core	255	0.3%	Unknown	Whole Core	1,750	2.0%			1/2 Core	444	0.5%		<i>DD – Sample Method not Recorded</i>		1,264	1.4%		DD TOTAL		77,136		RC	100 & 150 mm	Chips	1,720	1.9%	Unknown	Chips	9,554	10.7%	RC TOTAL		11,274		TOTAL			89,674	100%
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	<ul style="list-style-type: none"> • Approximately 11% of the dataset was sampled using RC drilling techniques; however this is confined to pre-collar surface drilling and generally from regions outside of the mineralised zone. Approximately 22% of the total drilled meters were sampled. • Since 2010, samples are bagged, numbered and dispatched to ALS Mt Isa laboratory: <ul style="list-style-type: none"> ○ Until 2016 ,the sample was jaw crushed, 50% split, ○ Crushed using a Boyd crusher 70% nominal passing 2mm. Since 2018 all core samples are jaw crushed then 100% re-crushed using a Boyd crusher, 70% nominal passing 3.15mm ○ The sample is rotary split with 500-800g retained and pulverised to 85% passing 75µm. ○ All rejected material is collected and saved (Coarse – jaw crushed product, collected 2010 to 2016). ○ Pulps are then sent to ALS Brisbane for analysis. • For the 2007/2008 programme laboratory sample preparations involved drying, crushing (jaw and Boyd), and pulverising the ½ core sample to 85% passing 75µm. • No detailed information can be found for laboratory preparation prior to 2007, however a similar procedure is assumed. • Varieties of laboratories have been used over time, and have been summarised in the table below (over 85% of all assays have been through the ALS laboratories. <table border="1" data-bbox="480 1189 1337 1624"> <thead> <tr> <th>Date Range</th> <th>Laboratory</th> <th>Number of Samples</th> <th>%</th> </tr> </thead> <tbody> <tr> <td>2010 to current</td> <td>ALS</td> <td>58,618</td> <td>70.7%</td> </tr> <tr> <td rowspan="2">2001 to 2009</td> <td>ALS</td> <td>11,839</td> <td>14.3%</td> </tr> <tr> <td>Genalysis</td> <td>438</td> <td>0.5%</td> </tr> <tr> <td rowspan="8">Prior to 2001</td> <td>AAL</td> <td>234</td> <td>0.3%</td> </tr> <tr> <td>ALS</td> <td>1,533</td> <td>1.8%</td> </tr> <tr> <td>Amdel</td> <td>4,612</td> <td>5.6%</td> </tr> <tr> <td>Aminya</td> <td>224</td> <td>0.3%</td> </tr> <tr> <td>Analabs</td> <td>1821</td> <td>2.2%</td> </tr> <tr> <td>Pilbara</td> <td>2,167</td> <td>2.6%</td> </tr> <tr> <td>UNE</td> <td>7</td> <td>0.0%</td> </tr> <tr> <td>Unknown</td> <td>1,464</td> <td>1.8%</td> </tr> <tr> <td>TOTAL</td> <td></td> <td>82,957</td> <td>100.0%</td> </tr> </tbody> </table>	Date Range	Laboratory	Number of Samples	%	2010 to current	ALS	58,618	70.7%	2001 to 2009	ALS	11,839	14.3%	Genalysis	438	0.5%	Prior to 2001	AAL	234	0.3%	ALS	1,533	1.8%	Amdel	4,612	5.6%	Aminya	224	0.3%	Analabs	1821	2.2%	Pilbara	2,167	2.6%	UNE	7	0.0%	Unknown	1,464	1.8%	TOTAL		82,957	100.0%
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	<ul style="list-style-type: none"> • Since 2010 the four acid the digestion process used (ALS Brisbane) is as follows: <ul style="list-style-type: none"> ○ Approximately 0.25g of sample catch weighed into a Teflon test tube. ○ HNO₃ and HClO₄ are added and digested at 115°C for 15 minutes. ○ HF is added and digested at 115°C for 5 minutes. ○ The tubes are then digested at 185°C for 145 to 180 minutes. This takes the digest to incipient dryness (digest is not “baked”) ○ 50% HCl is added and warmed ○ Made to 12.5ml using 9.5ml 11% HCl. • The table below summaries the analytical method and digest used for all assays in the Mineral Resource estimate. As can be seen, the majority of assays have been determined by using a four acid digest with an ICP OES read. <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="2" rowspan="2">Base Metal Analysis</th> <th colspan="5">Analytical Method</th> <th rowspan="2">Total</th> </tr> <tr> <th>ICP OES</th> <th>ICP MS</th> <th>AAS</th> <th>XRF</th> <th>Not Recorded</th> </tr> </thead> <tbody> <tr> <td rowspan="5" style="text-align: center;">Digest</td> <td style="text-align: center;">Four Acid</td> <td style="text-align: right;">69,489</td> <td style="text-align: right;">34</td> <td style="text-align: right;">2,469</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">71,992</td> </tr> <tr> <td style="text-align: center;">Aqua Regia</td> <td style="text-align: center;">-</td> <td style="text-align: right;">8,339</td> <td style="text-align: right;">5</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">8,344</td> </tr> <tr> <td style="text-align: center;">Mixed Acid</td> <td style="text-align: right;">301</td> <td style="text-align: right;">165</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">466</td> </tr> <tr> <td style="text-align: center;">Perchloric</td> <td style="text-align: right;">84</td> <td style="text-align: center;">-</td> <td style="text-align: right;">147</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">231</td> </tr> <tr> <td style="text-align: center;">Not Recorded</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">231</td> <td style="text-align: right;">7</td> <td style="text-align: right;">1,686</td> <td style="text-align: right;">1,924</td> </tr> <tr> <td colspan="2" style="text-align: center;">Total</td> <td style="text-align: right;">69,874</td> <td style="text-align: right;">8,538</td> <td style="text-align: right;">2,852</td> <td style="text-align: right;">7</td> <td style="text-align: right;">1,686</td> <td style="text-align: right;">82,957</td> </tr> </tbody> </table> <ul style="list-style-type: none"> • Gold assaying at Dugald River began in 1988 once the discovery of the hanging-wall copper lode was identified. Varieties of different assay methods have been used, and are summarised in the table below. The majority of gold assays were done by ALS (Townsville), by Fire assay with an AAS read, with a 50g charge used since 2008. At total of 418 gold assays were completed using Aqua Regia with an AAS read (completed between 1990 and 1996). <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="2" rowspan="2">Gold Analysis</th> <th colspan="4">Analytical Method</th> <th rowspan="2">Total</th> </tr> <tr> <th>AR-AAS</th> <th>FA-AAS 30g</th> <th>FA-AAS 40g</th> <th>FA-AAS 50g</th> </tr> </thead> <tbody> <tr> <td rowspan="6" style="text-align: center;">Laboratory</td> <td style="text-align: center;">AAL</td> <td style="text-align: center;">-</td> <td style="text-align: right;">49</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">49</td> </tr> <tr> <td style="text-align: center;">ALS</td> <td style="text-align: center;">-</td> <td style="text-align: right;">266</td> <td style="text-align: center;">-</td> <td style="text-align: right;">5,846</td> <td style="text-align: right;">6112</td> </tr> <tr> <td style="text-align: center;">AMDEL</td> <td style="text-align: right;">418</td> <td style="text-align: center;">-</td> <td style="text-align: right;">36</td> <td style="text-align: right;">57</td> <td style="text-align: right;">511</td> </tr> <tr> <td style="text-align: center;">ANALABS</td> <td style="text-align: center;">-</td> <td style="text-align: right;">638</td> <td style="text-align: center;">-</td> <td style="text-align: right;">135</td> <td style="text-align: right;">773</td> </tr> <tr> <td style="text-align: center;">PILBARA</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">149</td> <td style="text-align: right;">149</td> </tr> <tr> <td style="text-align: center;">Not Recorded</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: center;">-</td> <td style="text-align: right;">138</td> <td style="text-align: right;">138</td> </tr> <tr> <td colspan="2" style="text-align: center;">Total</td> <td style="text-align: right;">418</td> <td style="text-align: right;">953</td> <td style="text-align: right;">36</td> <td style="text-align: right;">6325</td> <td style="text-align: right;">7,732</td> </tr> <tr> <td colspan="2" style="text-align: center;">Percentage of Total (%)</td> <td style="text-align: right;">5.4%</td> <td style="text-align: right;">12.3%</td> <td style="text-align: right;">0.5%</td> <td style="text-align: right;">81.8%</td> <td style="text-align: right;">100.0%</td> </tr> </tbody> </table> <ul style="list-style-type: none"> • There are no inherent sampling problems recognised. • Measures taken to ensure sample representivity include orientation of the drill holes as close as practical to perpendicular to the known mineralised structure, and the collection and analysis of field duplicates. 	Base Metal Analysis		Analytical Method					Total	ICP OES	ICP MS	AAS	XRF	Not Recorded	Digest	Four Acid	69,489	34	2,469	-	-	71,992	Aqua Regia	-	8,339	5	-	-	8,344	Mixed Acid	301	165	-	-	-	466	Perchloric	84	-	147	-	-	231	Not Recorded	-	-	231	7	1,686	1,924	Total		69,874	8,538	2,852	7	1,686	82,957	Gold Analysis		Analytical Method				Total	AR-AAS	FA-AAS 30g	FA-AAS 40g	FA-AAS 50g	Laboratory	AAL	-	49	-	-	49	ALS	-	266	-	5,846	6112	AMDEL	418	-	36	57	511	ANALABS	-	638	-	135	773	PILBARA	-	-	-	149	149	Not Recorded	-	-	-	138	138	Total		418	953	36	6325	7,732	Percentage of Total (%)		5.4%	12.3%	0.5%	81.8%	100.0%
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Drilling techniques	<ul style="list-style-type: none"> Drilling used for the Mineral Resource started in 1969 and continued until present. Within the database used there are 2,017 drill holes (579 from surface {combination of RC and DD} and 1,528 DD underground), summarised in the table below. Approximately 9% of the surface drilling data does not have drillhole diameters recorded. <table border="1" data-bbox="592 544 1225 1196"> <thead> <tr> <th>Hole Type</th> <th>Hole Diameter</th> <th>Meters</th> <th>% of Total</th> </tr> </thead> <tbody> <tr><td>DD</td><td>BQ</td><td>3,073</td><td>0.85%</td></tr> <tr><td>DD</td><td>HQ</td><td>34,881</td><td>9.61%</td></tr> <tr><td>DD</td><td>HQ2</td><td>519</td><td>0.14%</td></tr> <tr><td>DD</td><td>HQ3</td><td>18,767</td><td>5.17%</td></tr> <tr><td>DD</td><td>LTK60</td><td>5,291</td><td>1.46%</td></tr> <tr><td>DD</td><td>NQ</td><td>50,016</td><td>13.78%</td></tr> <tr><td>DD</td><td>NQ2</td><td>89,785</td><td>24.74%</td></tr> <tr><td>DD</td><td>NQ3</td><td>3,074</td><td>0.85%</td></tr> <tr><td>DD</td><td>PQ</td><td>720</td><td>0.20%</td></tr> <tr><td>DD</td><td>Not Recorded</td><td>22,726</td><td>6.26%</td></tr> <tr><td>DD_UG</td><td>LTK60</td><td>15,368</td><td>4.23%</td></tr> <tr><td>DD_UG</td><td>NQ2</td><td>105,517</td><td>29.07%</td></tr> <tr><td>DD_UG</td><td>NQ3</td><td>148</td><td>0.04%</td></tr> <tr><td>RC</td><td>100 mm</td><td>1,580</td><td>0.44%</td></tr> <tr><td>RC</td><td>150 mm</td><td>140</td><td>0.04%</td></tr> <tr><td>RC</td><td>Not Recorded</td><td>11,326</td><td>3.12%</td></tr> <tr><td>TOTAL</td><td></td><td>362,929</td><td>100.00%</td></tr> </tbody> </table> <p data-bbox="512 1205 1305 1229">DD = Surface diamond drilling, DD_UG = Underground diamond drilling, PD= Percussion drilling</p> <ul style="list-style-type: none"> Some Historical holes (drilled prior to 1969) and other listed drill holes were not used for this estimate due to poor sample quality and reliability. 	Hole Type	Hole Diameter	Meters	% of Total	DD	BQ	3,073	0.85%	DD	HQ	34,881	9.61%	DD	HQ2	519	0.14%	DD	HQ3	18,767	5.17%	DD	LTK60	5,291	1.46%	DD	NQ	50,016	13.78%	DD	NQ2	89,785	24.74%	DD	NQ3	3,074	0.85%	DD	PQ	720	0.20%	DD	Not Recorded	22,726	6.26%	DD_UG	LTK60	15,368	4.23%	DD_UG	NQ2	105,517	29.07%	DD_UG	NQ3	148	0.04%	RC	100 mm	1,580	0.44%	RC	150 mm	140	0.04%	RC	Not Recorded	11,326	3.12%	TOTAL		362,929	100.00%
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Drill sample recovery	<ul style="list-style-type: none"> Recovery recorded during core logging was generally 100%, with minor losses in broken / sheared and faulted ground. At times, triple tube drilling from surface has been used to maximise core recovery but this is not common. RQD (rock quality designation) data was logged and recorded in the database to measure the degree of jointing or fractures or core loss in the sample. Shearing and broken ground zones are located at the edges of the mineralisation zone and are not associated with locations of good grade interceptions. There is no relationship between core loss and mineralisation or grade - no sample bias has occurred due to core loss within broken/sheared ground. 																																																																								

Criteria	Status
Logging	<ul style="list-style-type: none"> • All core samples including RC pre-collars have been geologically logged (lithology, stratigraphy, weathering, alteration, geotechnical characteristics) to a level that can support the Mineral Resource estimation. • The logging captures both qualitative (e.g. rock type, alteration) and quantitative (e.g. mineral percentages) characteristics. Core photographs are available for most drill holes. All drill holes post-2008 have been photographed (wet and dry). • A representative sample of mineralised core is stored at -4°C in refrigerated containers to minimise oxidation for metallurgical testing. Non-mineralised core is stored on pallets in the yard. • Currently, all drill holes are logged using laptop computers directly into the drillhole database. Logging has occurred in the past onto paper log-sheets and was then transcribed into the database.

Criteria	Status
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> • Prior to 2007 various sub-sample techniques and sample preparation techniques were used for DD drilling including whole, $\frac{3}{4}$ (generally restricted to metallurgical samples) and $\frac{1}{2}$ and $\frac{1}{4}$ (for general samples) core, where sample length is generally 1 metre. Since 2007 DD core was halved using a circular diamond saw, density tested before being sent to analytical testing. Sample lengths were cut as close to 1m as possible while respecting geological contacts. From 2016 whole core is sent for analysis for any in-fill drilling campaigns. • For DD, the standard sampling length is 1m with a minimum of 0.2m and a maximum 1.5m within the mineralised zone was determined by lithology and visible mineralisation (i.e., samples were taken up to but not across lithological contacts, and obvious high grade zones were sampled separately from lower grade intervals). • The sample collection protocol for RC grade control drill holes has typically been as follows: <ul style="list-style-type: none"> ○ RC samples are collected from a cyclone at 2m intervals from pre-collar surface drilling. ○ If the sample was dry the sample was passed through a riffle splitter and collected into a pre-numbered calico bag. Residual material was sampled and sieved for chip trays and the remainder returned to the larger poly-weave bag. The splitter was cleaned using compressed air or a clean brush and tapped using a rubber mallet. If the sample was wet then the sample was dried before being split according to the procedure above (for dry samples). ○ Historical RC programmes were designed to test the 'un-mineralised' hanging wall material in DD pre-collars. 2m bulk composites stored at the drill site were sampled using the spear method. • The vast majority of drillhole intersections are orthogonal to the mineralisation and as such are representative. • The sample preparation of RC chips and DD core adheres to industry good practice. Samples are bagged, numbered and dispatched to the ALS Mount Isa laboratory. At the laboratory, each sample is weighed then crushed using a Boyd crusher to 70% nominal passing 3.15mm. The sample is rotary split (500-800g) and pulverised to in a LM2 to 85% passing 75 μm. All rejected material is collected and saved. Pulps are then sent to ALS Brisbane for analysis. • Prior to 2013, measures taken to ensure sampling is representative of the in-situ material collected included: <ul style="list-style-type: none"> ○ Field duplicates (quarter core) were sampled at a rate of 1 per 20 samples (approximately 4 per drill hole). • The sample types, nature, quality and sample preparation techniques are considered appropriate for the style of the Dugald River mineralisation (sediment/shear hosted base metal) by the Competent Person.

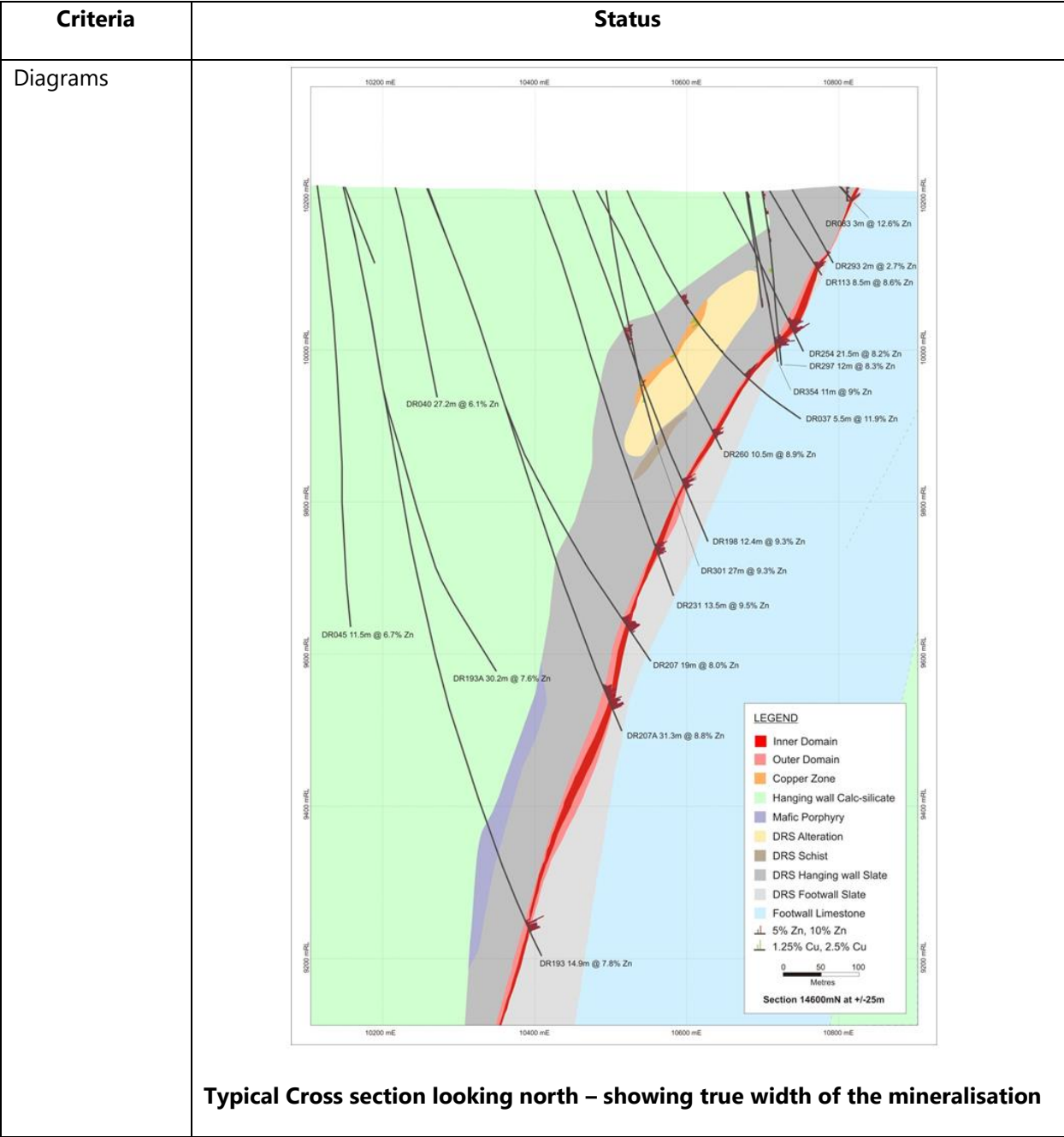
Criteria	Status
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> • The assaying methods currently applied at Dugald River are ICP-MS with a 4-acid digest which is used for the analysis of Zn, Pb, Ag, Fe, S, Mn and Cu which are estimated in the Mineral Resource. Total carbon (TotC) is analysed by Leco furnace. All of these analyses are considered total. • Gold assays are completed by Fire Assay with an AAS read, with a 50g charge used since 2008. • These assaying techniques are considered suitable for the Dugald River Mineral Resource. • No geophysical tools, spectrometers or handheld XRF instruments have been used in the analysis of samples external to the ALS laboratory for the estimation of Mineral Resources. • Certified reference materials (CRM) and blanks (coarse) were each submitted at the rate of 1:20. The selection and location of standards and blanks in the batch sequence is decided by the geologist on the basis of the logged mineralisation. • Batches that fail quality control criteria (such as standards reporting outside set limits) are entirely re-analysed. • Prior to 2015 duplicate sampling was performed by selecting from returned coarse rejects and resubmitted to ALS for analysis. • Since 2015 duplicates are taken by the laboratory every 20th sample alternating between a duplicate taken at the primary crushing stage or the pulverisation stage. Batches that return standard values above three standard deviations (3SD) are failed and all or part of the batch is re-analysed by the Laboratory (ALS).
Verification of sampling and assaying	<ul style="list-style-type: none"> • Verification of assay results was visually verified against logging and core photos by alternative company personnel. • No twinning of drill holes have occurred at Dugald River. However, close-spaced and crossing holes give comparable grade and width results • Core logging data was recorded directly into a Database (Geobank) by experienced geologists (geological information such as lithology and mineralisation) and field technicians (geotechnical information such as recovery and RQD). Where data was deemed invalid or unverifiable it was excluded from the Mineral Resource estimation. • No adjustments to the assay data is performed during import into the Geobank Database.

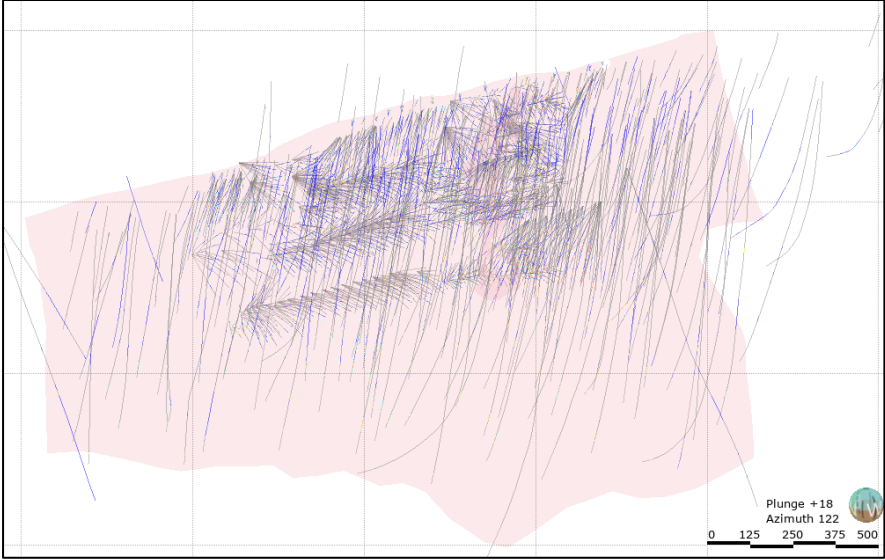
Criteria	Status
Location of data points	<ul style="list-style-type: none"> • All drill hole collars have been surveyed by licensed surveyors. Surface collars were surveyed in MGA94 and then converted to local mine grid. • Underground drill holes are marked up by surveying a collar pin at the designed collar point location which is supplied by the Geologists. <ul style="list-style-type: none"> ○ Currently the drillers obtain their azimuth for the hole by utilising an azimuth aligner which is calibrated weekly using a test bed that is has a fixed azimuth. ○ Upon completion of the drill program the collars of each drill hole are surveyed in local grid and saved into the drill hole register spreadsheet for the Geologists. ○ The equipment used underground to perform drillhole surveys is a Leica TS-15 total station. • For surface holes a collar point is marked out with a survey peg and then two pegs at the extremities of the drill pad are surveyed for the azimuth of the hole. <ul style="list-style-type: none"> ○ The drill rig lines up with these two pegs to drill on correct azimuth. ○ The drillers also use a true north azimuth tool to check the bearing. ○ The equipment used on surface for drill holes is a Trimble R8 RTK GPS. • Down-hole surveying has been undertaken using various methods including Eastman, Reflex and gyroscopic cameras. In general a spacing of 30m down hole between survey readings was used. Interference due to magnetite and pyrrhotite has been an issue. <ul style="list-style-type: none"> ○ During the 2007/2008 drilling program routine survey checks were undertaken on the reflex survey camera using an aluminium calibration stand positioned in a known orientation. ○ Since 2008 all drill holes are gyroscopically surveyed. ○ True North seeking azimuth tool has been used since 2017, to limit the effect of magnetic declination corrections. • The grid system used is MGA94, the conversion to local mine grid is rotated and scaled. The grid transformation is undertaken using a formula provided by the onsite surveyors. • A LIDAR survey flown in 2010 is used for topographic control on surface drilled drill holes. In the view of the Competent Person the LIDAR survey provides adequate topographic control.

Criteria	Status
Data spacing and distribution	<ul style="list-style-type: none"> • Drill spacing varies across the strike and dip of the mineralisation lode. The highest drill density in the ore body is 20m x 10m while the lowest drill density is greater than 100m x 100m spacing. • Locations drilled at 20m x 10m and up to 20m x 20m are adequate to establish both geological and grade continuity. Wider spaced drilling is adequate for definition of broader geological continuity but not sufficient for accurate grade continuity. • Underground mapping of faces is digitised and used in the interpretation and wire-framing process. • Drillhole data is concentrated within the top 300 m of the Mineral Resource with broader-spaced drilling at depth, due to the difficulty and cost involved in drilling deeper sections. • Drill spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource estimation procedure and classification applied. • Samples are not composited prior to being sent to the laboratory for analysis.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> • Geological mapping (both underground and surface) and interpretation show that the mineralisation is striking north-south and dips between 85 and 45 degrees towards the west. Hence drilling is conducted on east-west and west-east directions to intersect mineralisation across-strike. • Drilling orientation is not considered to have introduced sampling bias. Drill holes that have been drilled down dip and sub-parallel to the mineralisation have been excluded from the estimate.
Sample security	<ul style="list-style-type: none"> • Measures to provide sample security include: <ul style="list-style-type: none"> ○ Adequately trained and supervised sampling personnel. ○ Well maintained and ordered sampling sheds. ○ Cut core samples stored in numbered and tied calico sample bags. ○ Calico sample bags transported by courier to assay laboratory. ○ Assay laboratory checks of sample dispatch numbers against submission documents. ○ Assay data is returned as a .sif file via email and processed via the MMG assay loading software.
Audit and reviews	<ul style="list-style-type: none"> • The Dugald River database has been housed in various SQL databases. iOGlobal managed the database until the end of 2009 when the database was transferred and migrated to an MMG database. <ul style="list-style-type: none"> ○ Internal audits and checks were performed at this time. Any suspicious data was investigated and rectified or flagged and excluded. • No external independent audits have been performed on the database. • No external independent audits have been performed on the sampling techniques or the database. • Both ALS Mount Isa and Brisbane laboratories are audited on an annual basis by MMG personnel. From the most recent audit there were no material recommendations made.
Section 2 Reporting of Exploration Results	

Criteria	Status
Mineral tenement and land tenure status	<ul style="list-style-type: none"> • The Dugald River Mining Leases are wholly owned by a subsidiary of MMG Limited. • MMG holds one exploration lease and one mineral development lease in addition to the mining leases on which the Dugald River Mineral Resource is located. EPM12163 consists of 3 sub-blocks and covers an area of 20 sqkm to the west of the Dugald River deposit. ML2479 overlaps the eastern area of the EPM12163. • There are no known impediments to operating in the area.
Exploration done by other parties	<ul style="list-style-type: none"> • The History of the Dugald river zinc-lead deposit is summarised as follows: <p>Discovered in 1881, the first drilling programme in 1936 comprised three drill holes. The maiden Mineral Resource was reported in 1953 by Zinc Corporation. Drilling continued from 1970 through 1983 totalling 28 drill holes. CRA then re-estimated the Mineral Resource in 1987. Between 1989 and 1992 a further 200 drill holes were drilled, resulting from the discovery of the high-grade, north plunging shoot. Infrastructure, metallurgical and environmental studies were undertaken during this period. Between 1993 and 1996 irregular drilling was focused on the delineation of copper mineralisation in the hanging wall. In 1997 the project was transferred to Pasmenco, which had entered a joint venture with CRA in 1990. Re-compilation of the database, further delineation drilling, metallurgical test work, and the check assaying of old pulps was completed. Continued drilling between 2000 and 2009 with subsequent metallurgical studies culminated in a Feasibility Study. Structural analysis and a focused review on the northern copper zone in 2010 were completed. In 2011 the decline commenced which resulted in trial stoping. In 2014 some underground development was completed and drilling focused on confirming and extending continuity of the mineralisation within the Dugald River lode.</p>

Criteria	Status
Geology	<ul style="list-style-type: none"> • The Dugald River style of mineralisation is a sedimentary and shear hosted base metal deposit. The main sulphides are sphalerite, pyrite, pyrrhotite and galena with minor arsenopyrite, chalcopyrite, tetrahedrite, pyrrargyrite, marcasite and alabandite. • The deposit is located within a 3 km-4 km along strike north-south trending high strain domain named the Mount Roseby Corridor and is hosted by steeply dipping mid Proterozoic sediments of the Mary Kathleen Zone in the Eastern Succession of the Mount Isa Inlier. The host sequence is composed of the Knapdale Quartzite and the Mount Roseby Schist Group (which includes the Hangingwall calc-silicate unit, the Dugald River Slate and the Lady Clayre Dolomite). The sequence is an interbedded package of greenschist to amphibolite grade metamorphosed carbonate and siliclastic lithologies. • The main Dugald lode is hosted within a major N-S striking steeply west dipping shear zone which cross cuts the strike of the Dugald River Slate stratigraphy at a low angle. All significant zinc-lead-silver mineralisation is restricted to the main lode. Lesser-mineralised hanging wall and footwall lenses are present. Three main mineralisation textures/types are recognised, including banded, slaty breccia, and massive breccia. • The mineralogy of the Dugald lode is typical of a shale-hosted base metal deposit. The gangue within the lode is composed of quartz, muscovite, carbonates, K-Feldspar, clays, graphite, carbonaceous matter and minor amounts of calcite, albite, chlorite, rutile, barite, garnet, and fluorite. • The mineralised zone extends approximately 2.4 km in strike length and up to 1.4 km down dip.
Drill hole information	<ul style="list-style-type: none"> • 2,017 drill holes and associated data are held in the database (combination of RC and DD). • No individual hole is material to the Mineral Resource estimate and hence this geological database is not supplied.
Data aggregation methods	<ul style="list-style-type: none"> • This is a Mineral Resource Statement and is not a report on exploration results hence no additional information is provided for this section. • No metal equivalents were used in the Mineral Resource estimation. However the Mineral Resource has been reported above an A\$146 NSR calculated cut-off.
Relationship between mineralisation width and intercepts lengths	<ul style="list-style-type: none"> • Mineralisation true widths are captured by three-dimensionally modelled wireframes with drill hole intercept angles ranging from 90° to 40°. • The true thickness of the majority of the Mineral Resource is between 3m and 30m with the thickest zones occurring to the south.



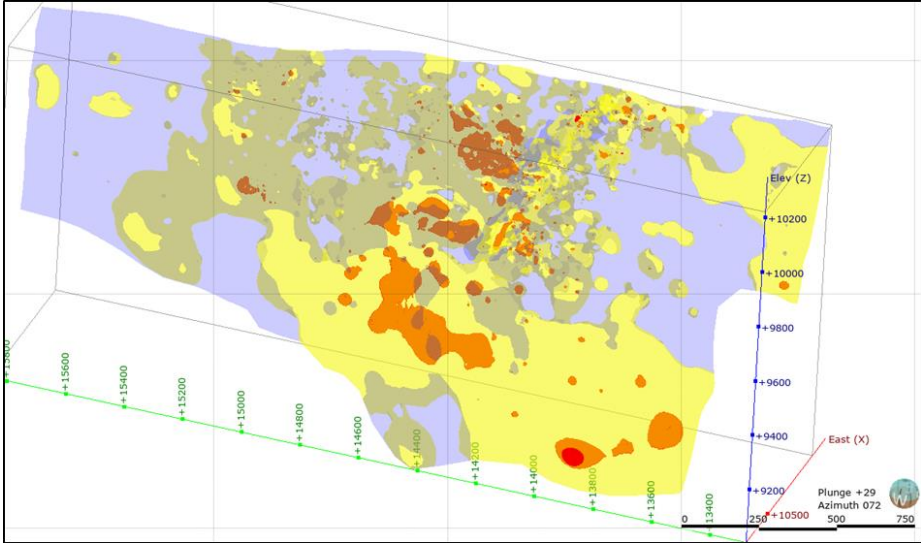
Criteria	Status
	 <p data-bbox="507 898 1326 965">Perspective View – looking SE of main mineralised zone with drill density</p>
Balanced reporting	<ul style="list-style-type: none"> <li data-bbox="411 1003 1406 1070">• This is a Mineral Resource Statement and is not a report on exploration results hence no additional information is provided for this section.
Other substantive exploration data	<ul style="list-style-type: none"> <li data-bbox="411 1111 1406 1178">• This is a Mineral Resource Statement and is not a report on exploration results hence no additional information is provided for this section.
Further work	<ul style="list-style-type: none"> <li data-bbox="411 1249 1406 1346">• MMG plans to continue to improve geological confidence and Mineral Resource classification through infill drilling programmes ahead of the mining schedule.

Criteria	Status
Section 3 Estimating and Reporting of Mineral Resources	
Database integrity	<ul style="list-style-type: none"> • The following measures are in place to ensure database integrity: <ul style="list-style-type: none"> ○ All data is stored in an SQL database that is routinely backed up. ○ All logging is digital and directly entered into the onsite Geobank database. Data integrity is managed by internal Geobank validation checks/routines that are administered by the Database Group and/or the site Geology Team. • The measures described above ensure that transcription or data entry errors are minimised. <ul style="list-style-type: none"> ○ Data validation procedures include: Database validation procedures are built in the database system to manage accurate data entry during logging and collection of data. ○ Prior to use in the Mineral Resource the data was checked externally by running Datamine macros on the drill hole file to check for end of hole depths, and sample overlaps. ○ Manual checks were carried out by reviewing the drill hole data in plan and section views.
Site visits	<ul style="list-style-type: none"> • The Competent Person visited site on various occasions through 2017 and 2018. Site visits included involvement with: <ul style="list-style-type: none"> ○ Assist with wireframe interpretation and methodology as applied in the 2018 Mineral Resource work. ○ Inspection of geological mapping plans. ○ Inspection of underground workings. ○ Inspection of drill holes and mineralisation interceptions.

Criteria	Status
Geological interpretation	<ul style="list-style-type: none"> • The mineralisation zone is modelled within a continuous corridor of zinc mineralisation. This zone is modelled based on zinc grade distribution and geological logging of mineralisation style. The mineralised envelope is determined by natural breaks in the grade distribution. There is good confidence on the geological continuity and interpretation of the deposit. <ul style="list-style-type: none"> ○ The mineralisation zone is further sub-divided into a high- and low-grade zinc domain. ○ The "inner" high-grade domain is the main Dugald River mineralisation lode, defined by high zinc grades associated with the massive sulphide assemblages. The high-grade domain boundary was selected by a grade boundary which is more representative of geology. ○ The "outer" zone defines the surrounding lower grade mineralisation with its associated assemblage of sulphide stringers and shoots of discontinuous massive and breccia sulphide textures. ○ Where possible a low grade (internal dilution) domain has been identified and modelled within the high grade domain. ○ There are 4 other smaller, sub-parallel zinc domains which have been identified with more closely spaced drilling, which generally follow the main mineralised lode (Domain 1) or structures associated with it. <div data-bbox="438 987 1378 1487" style="text-align: center;"> </div> <p data-bbox="408 1512 1340 1541">Perspective View - Five LGZN Domains (HGZN domains are within LGZN domains)</p>

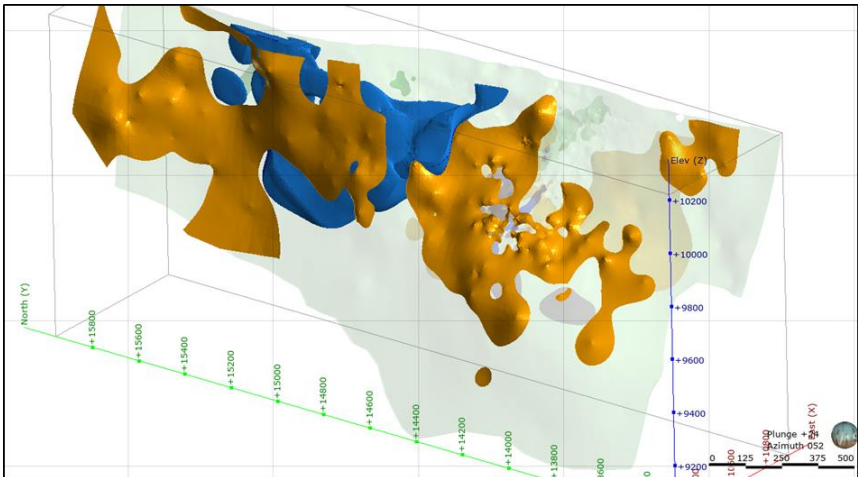
Criteria	Status
	<ul style="list-style-type: none"> <li data-bbox="411 304 1406 439">Separate domains were modelled for Pb, Ag and Mn mineralisation, after exploratory data analysis (EDA), have shown these elements are possibly due to a secondary mineralisation event; and are contained within the "outer" lower grade zinc domain. <div data-bbox="491 454 1326 947" style="text-align: center;"> </div> <p data-bbox="592 965 1225 994">Pb Domains – D1 (Blue – Low Grade / Red –High Grade)</p> <div data-bbox="472 1010 1345 1518" style="text-align: center;"> </div> <p data-bbox="443 1536 1374 1568">Ag Domains – D1 (Blue – Low Grade/ Yellow – Medium Grade / Red – High Grade)</p>

Criteria	Status
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Mn Domains – D1 (Blue – Low Grade/ Yellow – Medium Grade / Red – High Grade)

- Selection of the low/high grade zinc domain was based on geological observations and natural breaks within the mineralisation. An approx. zinc grade of 2 to 7% Zn was used to define the “outer” low grade zinc domains and a grade of greater than 7% Zn was used to define the “inner” high grade zinc domain.
- There is also a hanging-wall copper domain (relative to the zinc domains). The copper domain also has elevated gold which is associated with the copper. There are two types of mineralisation identified; a narrower vein style and a broader disseminated zone within a 0.1% Cu shell and an internal higher grade zone within a 0.3% Cu shell. The hanging wall copper domain generally runs parallel to the main zinc domain, though there some areas where there is some cross-over between the zinc and copper domains.



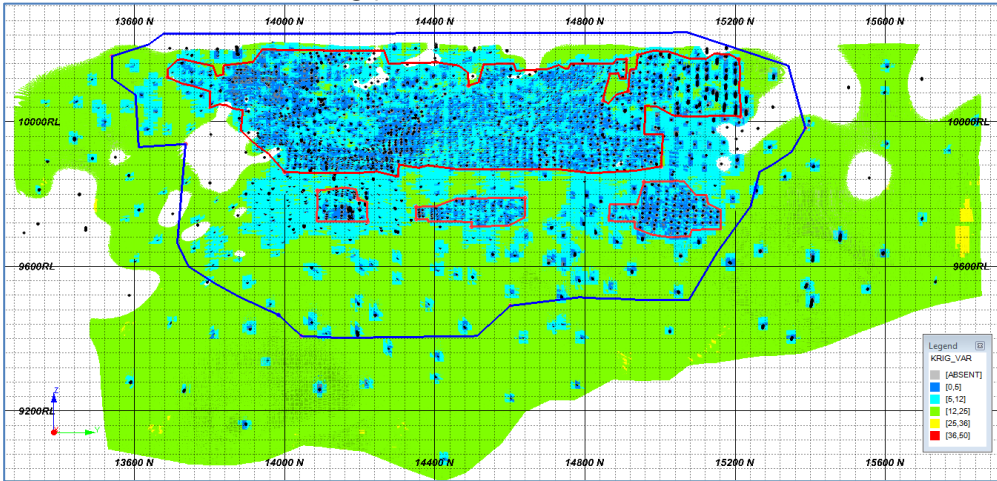
Hanging wall Copper Domain (Vein {orange}, 0.1% Cu shell & 0.3% Cu shell {dark blue}), relative to LG ZN Domains {shadowed}

Criteria	Status
	<div data-bbox="507 297 1337 719" style="text-align: center;"> </div> <p data-bbox="507 734 1412 831">Section looking north (14175mN left and 14325mN right), showing the Cu domain (coloured blocks), interaction with low grade Zn domain (dark wireframe shapes)</p> <ul data-bbox="411 853 1412 1077" style="list-style-type: none"> • Underground mapping of development drives for both access and ore drives were also used in assisting with the geological interpretation. • Globally the Dugald River deposit follows a reasonably predictable lens/sheet of mineralisation but with short-range (10m to 20m-scale) variations associated with localised structures that are suitably defined by close-spaced drilling within the Measured Mineral Resources.
Dimensions	<ul data-bbox="411 1099 1412 1458" style="list-style-type: none"> • The main Dugald lode (Domain 1) is hosted within a major N-S striking steeply west dipping shear zone which cross cuts the strike of the Dugald River Slate stratigraphy at a low angle. • The strike length of mineralisation is approximately 2,400 m. Dip varies between 85° and 40° to the west. • The true thickness of the majority of the Mineral Resource is between 3 m and 30 m with the thickest zones occurring to the south. • The mineralisation is open at depth. The deepest drill intersection of mineralised material is about 1,140 m below the surface.

Criteria	Status
Estimation and modelling techniques	<ul style="list-style-type: none"> • Mineral Resource modelling was completed using both Isatis and Vulcan software applying the following key assumptions and parameters: <ul style="list-style-type: none"> ○ Ordinary Kriging interpolation has been applied for the estimation of Zn, Pb, Ag, Mn, Fe, S, total carbon, Cu, Au and Bulk Density. This is considered appropriate for the estimation of Mineral Resources at Dugald River. ○ Extreme grades were treated by grade capping and were applied after compositing, with values greater than the selected 'cut value' being set to the top cut value and used in the estimation. Grade cap values were selected using a combination of both histogram and cumulative log probability plots. ○ Grade estimation was performed using a local varying anisotropy (Iva), which aligns and optimises the search direction of the estimate to the mineralised domain trend. ○ Hard boundary contacts were used to select samples used to estimate blocks in each of the mineralised zinc domains (high-grade and low-grade) as well as into individual domains for Ag, Mn and Pb. Hard boundaries were also used for hanging wall copper domain to estimate Cu and Au. ○ Variogram were modelled within each of the respective domain, these variogram ranges were then applied to the search parameters used in the estimation. ○ Orientation of the search ellipse was matched to the Iva, that is dip and dip direction at the local block was used in the estimation of the model. ○ Drillhole compositing resulted in nominal 1m intervals with residual composite intervals absorbed evenly into the composites resulting in no loss of sample intervals. ○ Separate variography and estimation were performed for Zn, Pb, Ag, Mn, Fe, S, bulk density, Cu, Au and total carbon, within each of their respective mineralised domains. ○ No assumptions have been made about the correlation between variables. All variables are comparably informed and independently estimated.

Criteria	Status
	<ul style="list-style-type: none"> ○ Interpolation was undertaken in two stages: <ul style="list-style-type: none"> ▪ Stage1: Ordinary Kriging applying two passes with varying search ellipse dimensions ▪ First pass is equal to 80 - 100% of the variogram range ▪ Second pass is equal to 2 x variogram range ▪ Stage 2: Assign blocks not estimated by the Ordinary Kriging 2 passes, the average grade of the respective domain. ○ A minimum number of 2 drill holes were used for all estimates. ○ Generally, the number of composite samples was restricted to a minimum of 6 and a maximum of 28 (Kriging Neighbourhood Analysis (KNA), was used to locally adjust on a mineralised domain basis). ○ Octant method was generally not applied to the Ordinary Kriging estimate, however from the KNA work some sectors (max of 2) were used to improve the estimate in some of the mineralised domains. ○ Block discretisation of 2 x 8 x 8 was applied. ● At the end of 2015 ~400Kt of Dugald ore (mined from trial stoping) was transported to the Century mine (also controlled by MMG) to be processed via the Century plant. A good correlation was found against the predicted block model data. ● Assumptions have been made regarding the recovery of all by-products in the NSR. ● Deleterious elements include manganese and carbon, which have been estimated in the block model. Ancillary elements estimated include Mn, Fe and S. ● Parent block size was set at 2.5 m x 12.5 m x 12.5 m (xyz) with sub-cells of x=0.5 m, y=0.5 m, z=0.5 m. Sub-cells were assigned parent block values. The parent block size assumes mining selectivity at the stope level. <ul style="list-style-type: none"> ○ In areas if intense drilling (10 x 20m), the estimate was performed with parent block set to 2.5 m x 6.25 m x 6.25 m (xyz) with sub-cells of x=0.5 m, y=0.5 m, z=0.5 m. Sub-cells were assigned parent block values. This block size is used to better estimate local variance with increased information. ○ Background waste is estimated with parent block size of 10 m x 50 m x 50 m (xyz), this was to reduce the total block model size. ● No external dilution has been applied to block grades. However, parent block size has assumed mining selectivity at a stope level. No other selective mining unit size assumptions were made in the estimation process. ● 2018 block model validation included the following steps: <ul style="list-style-type: none"> ○ Comparison against the previous 2017 block model including visual comparison of plans and cross-sections, tonnes grade curves, cumulative probability plots and trend plots. ○ Comparison against drillhole data using visual comparison of plans and cross-sections, statistics by domain, cumulative probability plots and swath plots.
Moisture	<ul style="list-style-type: none"> ● Tonnes in the model have been estimated on a dry basis.
Cut-off	<ul style="list-style-type: none"> ● The Mineral Resource is reported above an A\$146/t NSR (net smelter return)

Criteria	Status
parameters	cut-off. The selection of the A\$146/t NSR cut-off defines mineralisation which is prospective for future economic extraction. The reporting cut-off grade is in line with MMG's policy on reporting of Mineral Resources which is prospective for future economic extraction.
Mining factors or assumptions	<ul style="list-style-type: none"> • Mining at Dugald River is planned to be underground with the long-hole open stoping method favoured. Currently the deposit is accessed by two declines. • No external dilution has been applied to block grades. However, parent block size has assumed mining selectivity at a stope level. • The Mineral Resource has been depleted to account for mining.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> • The Dugald River deposit metallurgy process involves crushing and grinding followed by floatation and filtration to produce separate zinc and lead concentrates for sale. • Deleterious elements include manganese and carbon, which have been estimated in the block model. • Manganese percentage in the zinc concentrate is calculated as a post-processing step to allow the generation of a value that can be used for the Ore Reserve. • Manganese percentage in the zinc concentrate is calculated by way of an algorithm contained within the NSR script.
Environmental factors or assumptions	<ul style="list-style-type: none"> • Dugald River operates under Environmental Authority EPML00731213 issued by the Department of Environment Heritage Protection on 12 August 2012 and amended on 16 September 2016. • Non-acid forming (NAF) and Potentially Acid Forming (PAF) waste rock are distinguished by a north-south striking Limestone and Undifferentiated Black Slate lithological boundary respectively. Volumes are estimated and managed in accordance with site procedures. Waste rock storage space on surface is limited. The north mine area will allow for the return of waste rock as backfill and the south mine is backfilled with paste fill generated from tailings. • PAF/NAF classification is based on the work by Environmental Geochemistry International (EGI) in 2010. Subsequent follow-up test work onsite confirms EGI's conclusions.
Bulk density	<ul style="list-style-type: none"> • Bulk density is determined using the weight in air and water method. Frequency of samples is at least 1 determination per core tray and based on geological domains. The current database consists of 15,942 bulk density measurements. • Dugald River rock is generally impermeable requiring no coatings for reliable measurements. • Bulk density in the model has been estimated using Ordinary Kriging. Density estimation is constrained within the defined mineralisation domains. <ul style="list-style-type: none"> • Un-estimated blocks were assigned a bulk density value based on a stoichiometric formula (see below). <p>Bulk Density (assigned) = $(3.8*A/100) + (7.3*B/100) + (4.6*C/100) + (2.573*D/100)$</p> <ul style="list-style-type: none"> ○ Sphalerite content $A = 1.5*Zn\%$

Criteria	Status
	<ul style="list-style-type: none"> ○ Galena content $B = 1.15 * Pb\%$ ○ Pyrrhotite/Pyrite content $C = (Fe\% - (0.15 * Zn\%)) * 1.5$ ○ Gangue $D = 100 - A - B - C$ ○ SG of sphalerite = 3.8 ○ SG of Galena = 7.3 ○ SG of Pyrrhotite/pyrite = 4.6 ○ SG of gangue = 2.573 ○ Fe content in Sphalerite = 10% ● A bulk density of 2.75 g/cm³ has been assumed for the waste host domain.
Classification	<ul style="list-style-type: none"> ● 2018 Classification incorporates a combination of Kriging variance (KV), Kriging efficiency (KE), Kriging slope of regression (RS), drilling density and location of underground development (presence of underground geological mapping). ● Mineral Resource categories are generally based on: <ul style="list-style-type: none"> ○ Measured: < 20 m drill spacing, RS>0.85 plus grade control drilling. ○ Indicated: > 20 m to <100 m drill spacing, RS<0.6. ○ Inferred: > 100 m drill spacing, within mineralised domain ● The Competent Person reviewed the distribution of KV, KE and RS in long section view and generated three-dimensional wireframes to select Measured, Indicated and Inferred blocks. These wireframes also take into consideration the location of the underground development and presence of geological mapping and the 20 m x 20 m underground drilling. The use of wireframes ensured that contiguous areas of like classification were generated thus avoiding the "spotted dog" pattern of classified blocks. ● The Mineral Resource classification reflects the Competent Persons view on the confidence and uncertainty of the Dugald River Mineral Resource. ● Below is a long section looking east of the Dugald River mineralisation lode showing blocks coloured by Kriging variance (KV) and the Measured, Indicated and Inferred wireframes used in selecting the Mineral Resource classification. <ul style="list-style-type: none"> ○ Measured = red ○ Indicated = blue ○ Inferred = remaining portion  <p style="text-align: center;">Long-section of the Dugald River Block Model, blocks coloured by Kriging</p>

Criteria	Status
	variance
Audits or reviews	<ul style="list-style-type: none"> • No external independent audits have been performed in 2018. However, two external audits have been completed in recent years including Pennywise Ltd in 2015 and Lewis Mineral Resource Consultants Pty Ltd in 2013. All issues identified have been corrected in the current Resource model. • An internal MMG review has been carried on the current 2018 Mineral Resource estimate. This involved personnel from both Corporate and Dugald River sites. No material items to the Mineral Resource have been identified.
Discussion of relative accuracy / confidence	<ul style="list-style-type: none"> • The Competent Person is of the opinion that the current block estimate provides a good estimate of tonnes and grades at a global scale. In locations where grade control drilling of approximately 10mN x 20mRL spacing has been completed the Competent Person has a high level of confidence in the local estimate of both tonnes and grades. • No change of support adjustments have been performed to the model. • Commercial production at Dugald River began 1 May 2018, so there is limited production data to compare Mineral Resource confidence against actual mined tonnes and grades of the deposit. • Tonnes and grade checks comparing the 2017 and 2018 Mineral Resource models to check for tonnes and grade variability and accuracy as a function of increase drilling density has been undertaken. The following is noted: <ul style="list-style-type: none"> ○ Drilling density of <20m spacing is required to estimate tonnes and grade accuracy with an acceptable level of confidence.

5.3.1 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Mineral Resource statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Douglas Corley, confirm that I am the Competent Person for the Dugald River Mineral Resource section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a Member of The Australasian Institute of Geoscientists
- I have reviewed the relevant Dugald River Mineral Resource section of this Report to which this Consent Statement applies.

I am a full time employee of MMG Ltd. at the time of the estimation.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest.

I verify that the Dugald River Mineral Resource section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Dugald River Mineral Resources.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Dugald River Mineral Resources - I consent to the release of the 2018 Mineral Resources and Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Douglas Corley MAIG R.P.Geo. (#1505)

5/12/2018

Date: _____

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Signature of Witness:

Rex Berthelsen
Melbourne, VIC

Witness Name and Residence: (e.g. town/suburb)

5.4 Ore Reserves – Dugald River

5.4.1 Results

The 2018 Dugald River Ore Reserve are summarised in Table 15.

Table 15 2018 Dugald River Ore Reserve tonnage and grade (as at 30 June 2018)

Dugald River Ore Reserves							
	Tonnes (Mt)	Zinc (% Zn)	Lead (% Pb)	Silver (g/t Ag)	Contained Metal²		
					Zinc (‘000)	Lead (‘000)	Silver (Moz)
Primary Zinc¹							
Proved	6.7	11.6	2.1	65	783	142	14
Probable	21.7	11.7	2.0	30	2,539	435	21
Total	28.5	11.7	2.0	38	3,322	578	35
Stockpiles							
Proved	0.2	8.7	1.4	39	14	2	0.2
Total	28.6	11.7	2.0	38	3,336	580	35

1 Cut-off grade is based on Net Smelter Return (NSR) after Royalties, expressed as a dollar value of A\$146/t.

2 Contained metal does not imply recoverable metal.

Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors.

5.5 Ore Reserves JORC 2012 Assessment and Reporting Criteria

The following information provided in Table 16 complies with the 2012 JORC Code requirements specified by "Table-1 Section 4" of the Code.

Table 16 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Dugald River Ore Reserve 2018

Assessment Criteria	Commentary																																
Mineral Resources estimate for conversion to Ore Reserves	<ul style="list-style-type: none"> The Mineral Resources are reported inclusive of the Mineral Resources used to define the Ore Reserves. The Mineral Resources model used the MMG March 2018 Mineral Resources model. (dr0318m_rese.dm) Risks associated with the model are related to orebody complexity seen underground, but not reflected in the Mineral Resources model due to the spacing of the drill holes that inform the model. The 2018 Geotechnical model was used to estimate the hanging wall (HW) thickness, tonnes and grade of the unplanned dilution applied to the 2018 stope shapes. 																																
Site visits	<ul style="list-style-type: none"> The Competent Person for the Dugald River Ore Reserve frequently visited the site during 2017/2018 reporting period. 																																
Study status	<ul style="list-style-type: none"> The mine is an operating site with on-going detailed Life of Asset planning. 																																
Cut-off parameters	<ul style="list-style-type: none"> The breakeven cut-off grade (BCOG) and Mineral Resources cut-off grade (RCOG) have been calculated using average three years of the 2018 Budget costs. The operating costs, both fixed and variable, have been attributed on a per tonne basis using the planned mine production rate of 1.75Mtpa The Net Smelter Return (NSR) values are based on metal prices, exchange rates, treatment charges and refinery charges (TC's & RC's), government royalties and metallurgical recoveries. The NSR value for both BCOG and RCOG is to the mine gate and includes sustaining capital for the 2018 Ore Reserves. Infill diamond drilling has been included as part of the growth capital, not as the sustaining capital For 2018 Ore Reserves (OR) and Life of Asset (LoA), the break-even cut-off grade (BCOG) has been used to create the stope and level by level evaluation. <table border="1"> <thead> <tr> <th>Category of Cut-off</th> <th>Ave Bud Jul18-Dec20 AU\$/t processed</th> <th>2017 (Average 2020-2029) AU\$/t processed</th> <th>Diff</th> </tr> </thead> <tbody> <tr> <td>BCOG</td> <td>146</td> <td>134</td> <td>12</td> </tr> <tr> <td>SCOG</td> <td>128</td> <td>120</td> <td>8</td> </tr> <tr> <td>DCOG</td> <td>74</td> <td>97</td> <td>-23</td> </tr> <tr> <td>ICOG</td> <td>79</td> <td>74</td> <td>4</td> </tr> <tr> <td>MCOG</td> <td>33</td> <td>47</td> <td>-14</td> </tr> <tr> <td>RCOG</td> <td>146</td> <td>134</td> <td>12</td> </tr> <tr> <td>TCOG</td> <td>155</td> <td>158</td> <td>-3</td> </tr> </tbody> </table>	Category of Cut-off	Ave Bud Jul18-Dec20 AU\$/t processed	2017 (Average 2020-2029) AU\$/t processed	Diff	BCOG	146	134	12	SCOG	128	120	8	DCOG	74	97	-23	ICOG	79	74	4	MCOG	33	47	-14	RCOG	146	134	12	TCOG	155	158	-3
Category of Cut-off	Ave Bud Jul18-Dec20 AU\$/t processed	2017 (Average 2020-2029) AU\$/t processed	Diff																														
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TCOG	155	158	-3																														

Assessment Criteria	Commentary
Mining factors or assumptions	<ul style="list-style-type: none"> • A detailed design of the 2018 OR was used to report Mineral Resources conversion to an Ore Reserves. • The 2018 Geotechnical Equivalent Linear Overbreak Slough (ELOS) model was used to estimate the HW thickness, tonnes and grade of the planned dilution applied to the 2018 stope shapes. • The orebody is split into a north and south mine, due to its 2 km strike length and a low-grade zone in the outer side of the orebody. • The north mine is narrow (average ~5 m true width) and sub-vertical. The south mine is wider than the north mine with a flexural zone in the centre. The south mine is narrow and steep in the upper zone (~top 200 m from surface) and lower zone (~below 700 m from surface). The central zone is flatter and thicker than the upper and lower zones. • Mining methods for the mine are Sub-Level Open Stopes (SLOS) in the South Mine and modified Avoca stoping in the North Mine with a 25m level interval and variable stope strike length of 15 m to 30m. • The stopes are broken into the following categories: <ul style="list-style-type: none"> ○ Longitudinal SLOS, for any stopes less than 11 m wide horizontally. ○ Transverse SLOS, made up of 20 m strike SLOS mined full width of the ore-body. ○ Crown pillar SLOS, for the top level of each panel where stoping occurs directly below a previously mined area. ○ Modified Avoca stopes for the North Mine • The stopes were created by applying the Mineable Shape Optimiser (MSO) software in Deswik CAD to the 2018 Mineral Resources model (dr0318m_resefull.dm) that were created in Datamine. • The parameters used to create the stope shapes were: <ul style="list-style-type: none"> ○ All Mineral Resources categories included ○ 25 m level interval ○ Variable strike length ○ Minimum mining width (MMW) of 2.5 m ○ The minimum dip of 45 degrees for Footwall (FWL) and 37 degrees for Hangingwall (HW) ○ Minimum waste pillar between parallel stopes of 5m ○ A\$146/t BCOG applied to create initial stope shapes. • Several aspects of dilution were considered, planned dilution, fill dilution, FW dilution and HW dilution. Planned dilution was included in the MSO stope shapes and covers localised variations in dip and strike as well as minimum mining width. FW dilution was included where ore development was wider than the stope width. No additional FW dilution was applied as the initial stope shapes took into account minimum mining widths and dip.

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> • The HW dilution was calculated for each stope based on the Geotechnical conditions and thicknesses of the HW materials. The site has compiled a detailed HW dilution model as dilution varies across the ore-body according to the HW conditions. • Fill Dilution and Stope Recovery Factors: <ul style="list-style-type: none"> ○ Floor 0.15 m and wall fill ranges from 0.3 m to 0.5 m dilution. ○ Recoveries Crown stopes 65%, Longitudinal and Transverse 95%. • Development grades were diluted by the application of a grade factor of 95% to all ore development grades estimated from the corresponding stope grades. • No Inferred Mineral Resources are included in the Ore Reserves. • The underground (UG) mine is accessed via two declines. The mine is split into two parts – north and south, and thus it has two separate declines for the UG access. As at 30 June 2018, there is 2,886 m of decline in place. Also, there are 20,890 m of lateral development in place. • Currently, three raise-bored ventilation shafts are in place: <ul style="list-style-type: none"> ○ The southern Fresh Air Raise (FAR) – at 3.5 m diameter and 130 m depth; ○ The southern Return Air Raise (RAR) – at 5.0 m diameter and 198 m depth; ○ The northern FAR at 3.5 m diameter and 172 m depth (currently being used as RAR). • There is also a RAR longhole winze (LHW) system in the south mine – at 18.9 m square and 116 m long and a RAR long hole winze system in the north mine at 18.9 m square and 129 m long. • Two escape raises are in place: <ul style="list-style-type: none"> ○ South mine escape way at 1.8 m diameter and 222 m depth ○ North mine escape way at 1.8 m diameter and 93 m depth • Mining mobile fleet is planned to include 3 twin-boom jumbos, 3 cable bolting rigs, 6 loaders, 8 dump trucks, 2 long-hole drill rigs, 2 shotcrete rigs, 3 Transmixers, 4 charge-up vehicles, 3 raise-bore drill rigs, 3 integrated tool carriers, and light vehicle fleet.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> • The metallurgical process for treatment of Dugald River ore involves crushing and grinding followed by selective flotation to produce separate lead and zinc concentrates. This process is conventional for this style of mineralisation and is used worldwide. • The flow sheet was extensively tested at bench scale with over 200 tests being completed on a wide range of samples. • Locked cycle testing, as a way to assess the continuous run in a laboratory scale, was performed on five different samples. The results were favourable, and are summarised in Table 21 below. <p style="text-align: center;">Results of locked cycle testing</p>

Assessment Criteria	Commentary																																																																							
	<table border="1" data-bbox="552 318 1318 542"> <thead> <tr> <th rowspan="2">Sample</th> <th colspan="2">Pb Conc, % Pb</th> <th colspan="2">Pb Rec, %</th> <th colspan="2">Zn Conc, % Zn</th> <th colspan="2">Zn Rec, %</th> </tr> <tr> <th>OCT</th> <th>LCT</th> <th>OCT</th> <th>LCT</th> <th>OCT</th> <th>LCT</th> <th>OCT</th> <th>LCT</th> </tr> </thead> <tbody> <tr> <td>2014 bulk sample</td> <td>61.2</td> <td>59.6</td> <td>67.7</td> <td>79.5</td> <td>55.6</td> <td>52.5</td> <td>88.8</td> <td>92.8</td> </tr> <tr> <td>DU0209</td> <td>56.0</td> <td>53.8</td> <td>68.6</td> <td>81.7</td> <td>52.1</td> <td>52.2</td> <td>87.6</td> <td>88.7</td> </tr> <tr> <td>DU0279</td> <td>61.4</td> <td>65.3</td> <td>69.5</td> <td>89.6</td> <td>50.8</td> <td>51.4</td> <td>87.0</td> <td>89.0</td> </tr> <tr> <td>DU0275</td> <td>54.6</td> <td>47.0</td> <td>51.1</td> <td>72.8</td> <td>50.0</td> <td>52.1</td> <td>86.8</td> <td>87.8</td> </tr> <tr> <td>2015 bulk sample</td> <td>61.9</td> <td>46.5</td> <td>52.2</td> <td>73.7</td> <td>54.8</td> <td>52.1</td> <td>89.7</td> <td>91.7</td> </tr> <tr> <td>Average</td> <td>59.0</td> <td>54.4</td> <td>61.8</td> <td>79.5</td> <td>52.6</td> <td>52.1</td> <td>88.0</td> <td>90.0</td> </tr> </tbody> </table> <ul style="list-style-type: none"> • Two separate plant trials were conducted for processing of Dugald River ore, using the existing facilities at the Century processing plant. 458,000 tonnes of Dugald River ore was processed during the trials. The results obtained from these plant trials were incorporated into the final plant design. • The Dugald River processing facility was commissioned with production commencing in October 2017, with nameplate throughput reached after 7 months of operation (May 2018). Both lead and zinc concentrate produced at Dugald River meet saleable grade and impurity specifications. • Dugald River plant operating data has been analysed to establish the metallurgical factors used for Ore Reserve calculations. Key parameters are: <ul style="list-style-type: none"> • Lead Concentrate Grade Pb% = 63.0% • Lead recovery to a lead concentrate according to the equation: Pb recovery Pb Conc (%) = 49.4 + 10.2 X Pb% • Silver recovery to a lead concentrate according to the equation: Ag recovery Pb Conc (%) = 0.5746 x Pb recovery Pb Conc • Zinc Concentrate Grade Zn% = 50.8% • Zinc recovery to a zinc concentrate according to the equation: Zn recovery Zn Conc (%) = $\frac{[100 - \text{ZnLoss PF Conc} - \text{ZnLoss PB Conc}] \times \text{Zn Recovery Constant Zn Conc}}{100}$ <p>Where</p> <ul style="list-style-type: none"> • ZnLossPF Conc = -29.16 + 1.1216 X C% + 0.4557 x Fe% + 0.2655 x SiO2% + 0.2854 x Zn% + 0.2039 x C RecoveryPF Conc • C Recovery PF Conc = 60 • ZnLoss PB Conc = -1.591 + 7.7215 x Pb%/Zn% + 0.0287 x Pb Recovery PB Conc • Zn Recovery Constant Zn Conc = 94.7%* • Plant operating data from May to July 2018 indicates the Zn Recovery Constant Zn Conc was 91%. The increase to 94.7% reflects the expected improvement in recovery as the plant is optimised post ramp up. • Ag Recovery Zn Conc = $\frac{[100 - \text{AgLoss PF Conc} - \text{Ag Recovery Pb Conc}] \times \text{Ag Recovery Constant Zn Conc}}{100}$ 	Sample	Pb Conc, % Pb		Pb Rec, %		Zn Conc, % Zn		Zn Rec, %		OCT	LCT	OCT	LCT	OCT	LCT	OCT	LCT	2014 bulk sample	61.2	59.6	67.7	79.5	55.6	52.5	88.8	92.8	DU0209	56.0	53.8	68.6	81.7	52.1	52.2	87.6	88.7	DU0279	61.4	65.3	69.5	89.6	50.8	51.4	87.0	89.0	DU0275	54.6	47.0	51.1	72.8	50.0	52.1	86.8	87.8	2015 bulk sample	61.9	46.5	52.2	73.7	54.8	52.1	89.7	91.7	Average	59.0	54.4	61.8	79.5	52.6	52.1	88.0	90.0
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Average	59.0	54.4	61.8	79.5	52.6	52.1	88.0	90.0																																																																

Assessment Criteria	Commentary
	<p>Where</p> <ul style="list-style-type: none"> • AgLossPF Conc = 1.71 + 1.137 x ZnLoss% PF Conc • AG Recovery Constant Zn Conc = 6.966 x e(0.0234 x ZnRecovery Constant Zn Conc) • Where Zn%, Pb%, Fe%, Mn%, C% and SiO2% refer to the relevant assays of the ore • A full check has been completed for possible deleterious elements, and the only two that are material to economic value are Fe and Mn in the Zn concentrate. It is for this reason that the algorithms to predict these components have been developed using Dugald River operating data: • Iron assay of zinc concentrate according to the equation: % Fe in Zn concentrate = $\frac{6.4357+0.4918 \times (3.7885 \times \text{Mn \%})}{0.72}$ • Manganese assay of zinc concentrate according to the equation: % Mn in Zn concentrate = 3.7885 x Mn%
Geotechnical	<ul style="list-style-type: none"> • Ground conditions at Dugald River are generally good to fair with isolated areas of poor ground associated with shear zones and faults. • Development ground support at this stage in the mine life of Dugald River focuses on static stability requirements with surface support matched to the ground conditions, e.g. mesh for good ground/ short design life and Fibrecrete for poor ground and long-term design life (e.g. decline). • Stope stability is strongly influenced by the presence and proximity of hangingwall shear zones which are associated with very poor ground conditions. • The trial stoping conducted at Dugald was used to calibrate the geotechnical stope dilution model from which guidance on stope dimensions (strike/ hydraulic radius) and estimates of stope dilution could be made. • The life of mine mining sequence is modelled using MAP3D (a linear-elastic method) to provide guidance on favourable sequences that will minimise the adverse effects of induced stress.
Environmental	<ul style="list-style-type: none"> • Dugald River operates under Environmental Authority EPML00731213 issued by the Department of Environment, Heritage Protection on 12 August 2012 and amended on 7 June 2013. • Non-Acid Forming (NAF) and Potentially Acid Forming (PAF) waste rock are distinguished by a north-south striking Limestone and Undifferentiated Black Slate lithological boundary respectively. Volumes are estimated and managed by site procedures. With limited stockpile space on the surface, all PAF waste rock store temporary on the surface but used as rockfill underground and only store NAF waste rock on the surface.

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> The north mine area uses of waste rock as backfill, and the south mine backfilled with paste fill generated from tailings.
Infrastructure	<ul style="list-style-type: none"> Currently, the DR mine is operating by using an electricity grid with standby diesel generators if needed. Northwest Queensland is now connected to the state electricity grid, feed on Mica Creek gas-fired power station on the southern outskirts of Mount Isa. Gas supplied via the Carpentaria pipeline, with a compression station in Bellevue. Based on the current production schedule, DR site manning numbers peak at 530 people in 2022. Cloncurry airport is used by commercial and charter airlines flying to and from Townsville, Cairns and Brisbane and operates as both a commercial and fly-in-fly-out (FIFO) airport. Existing surface infrastructure includes: <ul style="list-style-type: none"> An 11 km sealed access road from the Burke Developmental Road, which includes an emergency airstrip for medical and emergency evacuation use; A permanent camp; Telstra communication tower A temporary contractors mobile equipment facility; Ore and waste stockpile pads; Contaminated run-off water storage dams; Office facilities; Office buildings, including emergency medical facilities; A core shed; Alternatively, power generation a fuel farm and Genset; Bore water fields; Major infrastructure has been completed that includes a processing plant, Past Plant, tailings storage facility, permanent mobile equipment workshop, recreational facilities, power supply lines and raw water supply pipeline.
Costs	<ul style="list-style-type: none"> The estimation of capital cost for the Dugald River project was derived from first principles in the 2018 LoA schedule and the process to be refined through operation reviews. The MMG commercial department estimated the mining operating costs for the OR evaluation using first-principles. Deleterious elements Mn (and to a lesser extent Fe) are to be controlled by metallurgical blending. It is expected that the feed for flotation will be blended to maintain Mn (and to a lesser extent Fe) within the contractual range for concentrate sales and thus not expected to attract additional costs and penalties.

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> • The MMG finance department supplies the commodity price assumptions. The Dugald River Ore Reserve applied the January 2018 guidance. • The long-term exchange rate used the January 2018 Long-Term MMG guidance and assumptions supplied by the MMG Business Evaluation department. • The road freight and logistics for domestic and export sales have been updated using the costs from the 2018 budget. The additional costs for storing and ship loading of concentrate in Townsville are included. For the 2018 Ore Reserves, the storage and ship loading cost has been added to the freight and logistics cost for export. The freight and logistics costs for the domestic sale of concentrate include of the sea freight cost based on an agreement with Sun Metals. • Treatment and refining charges are based on MMG's estimate as contracts currently under review. • Queensland State Government royalties payable are prescribed by the Minerals Resources Regulation 2013 and are based on a variable ad valorem rate between 2.5% to 5.0% depending on metal prices.
Revenue factors	<ul style="list-style-type: none"> • Realised Revenue Factors (Net Smelter Return after Royalty) • As part of the 2018 Ore Reserves process, the net smelter return (after royalty) (NSR) has been revised with the latest parameters and compared against the previous 2017 NSR calculation that was used for the 2017 Ore Reserve. • The NSR is used to convert the various zinc, lead and silver grades into a single number for cut-off estimation and determining if the rock is ore or waste. • Freight and logistic charges have increased by 30% due to the increase in road and rail freight cost from Dugald to Townsville when compared to 2017 OR. • The MMG finance department provides assumptions of commodity prices and exchange rates.
Market assessment	<ul style="list-style-type: none"> • Although the rate of growth of global zinc consumption is slowing, demand is still expected to increase by 1-2%pa over the medium term, with growth mainly coming from China the world's developing nations. • Stocks of refined zinc are currently at historically low levels after several years where production was constrained by limited mine production and concentrate availability. The low mine production resulted from a period of low metal prices and the closure of several major mines due to resource exhaustion. • Zinc mine production is now recovering as new mine projects and restarted operations such as Dugald River, Lady Loretta, Gamsberg and New Century come to the market during 2018 and 2019.

Assessment Criteria	Commentary
	<p>Beyond these projects, there is uncertainty surrounding future new supply, while there is also limited growth in new smelting capacity. Increasingly stringent environmental regulations in China also restrict supply growth in that region.</p> <ul style="list-style-type: none"> • New projects tend to be more economically challenging than existing or recently closed operations due to a range of factors including grade, size and location. • The combination of current low stocks, reasonable demand growth prospects and limitations on future supply should be supportive of the zinc price over the medium term. • Smelters have well accepted Dugald River zinc concentrate quality in China, Australia and Korea who have received the product during 2018. There is substantial demand from smelters and traders for long-term contracts for the supply of the product which underpin sales from 2019 onwards.
Economic	<ul style="list-style-type: none"> • Economic modelling of the total mining inventory shows positive annual operating cash flows. Applying the revised costs, metal prices and exchange rate (MMG January 2018 Long-Term economic assumptions) returns a positive NPV. MMG uses a discount rate supported by MMG's Weighted Average Cost of Capital (WACC) and adjusted for any country risk premium (as applicable) based on an internal evaluation of the country risk for the location of the deposit. • All evaluations were done in real Australian (AU) dollars.
Social	<ul style="list-style-type: none"> • The nearest major population centre for the Mine is Cloncurry with a population of approximately 4,000, and the largest employers are mining, mining-related services and grazing. • Regarding Native Title, the Kalkadoon # 4 People filed a claim in December 2005 covering an area which includes the project area, water pipeline corridor and part of the power line corridor. This claim over 40,000 square kilometres of land was granted in 2011. • MMG has concluded a project agreement with the Kalkadoon People dated 6 April 2009. Under this agreement, the claimant group for the Kalkadoon are contractually required to enter into an s31 Native Title Agreement under the Native Title Act 1993. The agreement sets out the compensation payments and MMG's obligations for training, employment and business development opportunities if/when the project is commissioned. MMG has developed an excellent working relationship with the Kalkadoon claimant group. MMG has instituted the MMG/KCPL Liaison Committee, which meets at least twice yearly and addresses the Kalkadoon agreement obligations for both parties. An official 'Welcome to Country' ceremony was held for MMG in late March 2012. • The Mitakoodi and Mayi People filed a claim in October 1996 and covered an area that includes part of the power line corridor. While

Assessment Criteria	Commentary																	
	<p>the Mitakoodi have not yet been granted Native Title, MMG continues to liaise with them as a stakeholder due to the 'last claimant standing' legal tenement.</p> <ul style="list-style-type: none"> MMG has registered an Indigenous Cultural Heritage Management Plan (CHMP) which covers the entire project area and has undertaken all necessary surveys and clearances for all disturbed groundwork undertaken on site to date without any issues or complications. The CHMP was developed in consultation with the Kalkadoon # 4 People. 																	
Other	<ul style="list-style-type: none"> There is no identified material naturally occurring risks. The legal agreements are in place. There are no outstanding material legal agreements. The grade of the zinc concentrate is dependent on the Fe and Mn content of the sphalerite, but this dependence is taken into account by the algorithms presented earlier. The government agreements and approvals are in place. There are no unresolved material matters on which the extraction of the Ore Reserves is contingent. 																	
Tailings	<ul style="list-style-type: none"> The Dugald River Tailings Storage Facility (TSF) has been modified from the previously proposed design to align with changes in mine production profiles and paste fill requirements. The new design proposes integrated tailings, and process water facility continues to supply a large portion of the site's annual processing water demand via the Decant Return system. It proposed that the peak operational throughput of the processing plant now be 2.0 Mtpa, with an average of 35% of the tailings being sent to paste and the remaining 65% thickened to a solids density of 40 % solids. Previous assumptions saw peak mill throughput peak at 1.5 Mtpa for the modelled base case and 1.75 Mtpa for the upside case. The water balance model was run to identify the likely water volumes needing to be managed within the integrated facility and to provide an indication as to the likely rates that may need to supply from the Lake Julius pipeline. The table below shows the tailing storage required for the High Case that includes the capacity required for 2018 Ore Reserves. <p style="text-align: center;">TAILINGS PRODUCTION & REQUIRED TSF CAPACITY</p> <table border="1" data-bbox="512 1794 1358 2024"> <thead> <tr> <th>Design Topic</th> <th>Criterion</th> <th>Value</th> </tr> </thead> <tbody> <tr> <td rowspan="4">Production Data</td> <td>Total Resource (Milled Ore)</td> <td>38.2 Mt</td> </tr> <tr> <td>Life of Asset (LoA)</td> <td>27 years</td> </tr> <tr> <td>Total Tailings Production</td> <td>28.5 Mt</td> </tr> <tr> <td>Proportion of Tailings to Underground Paste Backfill</td> <td>62%</td> </tr> <tr> <td rowspan="2">TSF Capacity</td> <td>Total Tailings to TSF</td> <td>10.9 Mt</td> </tr> <tr> <td>Design TSF Tailings Capacity</td> <td>12.6 Mt</td> </tr> </tbody> </table>	Design Topic	Criterion	Value	Production Data	Total Resource (Milled Ore)	38.2 Mt	Life of Asset (LoA)	27 years	Total Tailings Production	28.5 Mt	Proportion of Tailings to Underground Paste Backfill	62%	TSF Capacity	Total Tailings to TSF	10.9 Mt	Design TSF Tailings Capacity	12.6 Mt
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Assessment Criteria	Commentary
Classification	<ul style="list-style-type: none"> • Ore Reserves are reported as Proved and Probable. • Only Measured (13%) and Indicated (45%) Mineral Resources have been used to inform the Proved and Probable Ore Reserves. No Inferred Mineral Resources are included in the Ore Reserves.
Audits or reviews	<ul style="list-style-type: none"> • No external audits have been undertaken for the 2017 Ore Reserves. MMG personnel have been involved in reviewing the Ore Reserves process. • An External Review or Audit has been scheduled for 2019.
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> • Ore Reserves Risks that may materially change/effect; • The geological understanding of the grade continuity concerning diamond drill spacing. • The geotechnical risk associated with hanging-wall instability and mining dilution. • Mining infrastructure analysis requires further work on underground trucking, ventilation and power constraints. • Metallurgical risks (recovery and concentrate grades) require additional testing to confirm scale up reliability, metallurgical performance and reagent consumption. • Close spaced drilling is applied to a locally defined tonnage and grade before mining selection. Ore Reserves are based on all available relevant information. • Ore Reserves accuracy and confidence that may have a material change in modifying factors are discussed above.

5.5.1 Expert Input Table

Some persons have contributed vital inputs to the Ore Reserves determination. These are listed below in Table 17.

In compiling the Ore Reserves, the Competent Person has reviewed the supplied information for reasonableness but has relied on this advice and information to be correct.

Table 17 Contributing Experts – Dugald River Ore Reserves

EXPERT PERSON / COMPANY	AREA OF EXPERTISE
Douglas Corley, Principal Geologist MMG Ltd (Melbourne)	Geological Mineral Resources
Joshua Annear, Group Manager Business Evaluation, MMG Ltd (Melbourne)	Economic Assumptions
Steve Whitehead, General Manager Marketing, MMG Ltd (Melbourne)	Marketing, Sea freight and TC/RC
Nigel Thiel, Principal Metallurgist, MMG Ltd (Melbourne)	Metallurgy
Angus J Henderson, Snr Manager Commercial & Business Support, MMG Ltd (Australian Operations)	Mining capital and Operating Costs
Christian Holland, Principal Geotechnical Engineer, MMG Ltd (Melbourne)	Geotechnical
Karel Steyn, Principal Mining Engineer, MMG Ltd (Melbourne)	Mining Parameters, Cut-off estimation, Mine Design and Scheduling
Donna Noonan, Principal Closure Planning, MMG Ltd (Melbourne)	Mine Closure and Remediation

5.5.2 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Ore Reserves statement has been compiled by the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Karel Steyn, confirm that I am the Competent Person for the Dugald River Ore Reserves section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having more than five years experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a Member of The Australasian Institute of Mining and Metallurgy
- I have reviewed the relevant Dugald River Ore Reserves section of this Report, to which this Consent Statement applies.

I am a full-time employee of MMG Ltd. at the time of the estimate.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest.

I verify that the Dugald River Ore Reserves section of this Report is based on and reasonably and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Dugald River Ore Reserves.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code, 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Dugald River Ore Reserve - I consent to the release of the 2018 Mineral Resources and Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Karel Steyn MAusIMM (#309192)

5/12/2018

Date:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Rex Berthelsen
Melbourne, VIC

Signature of Witness:

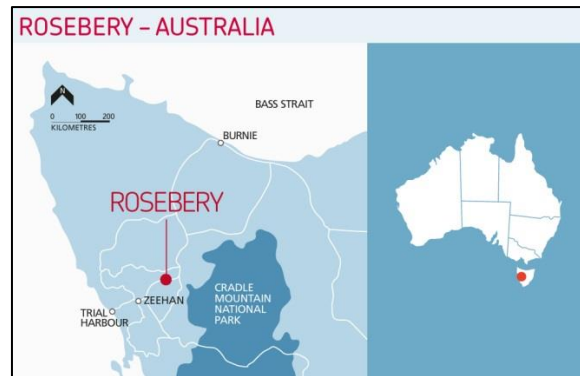
Witness Name and Residence: (e.g. town/suburb)

6 ROSEBERY

6.1 Introduction and Setting

- 3 The Rosebery base and precious metals mining operation is held by MMG Australia Limited and is located within Lease ML 28M/1993 (4,906ha), on the West Coast of Tasmania approximately 120km south of the port city of Burnie (Figure 6-1). The main access route to the Rosebery mine from Burnie is via the B18 and the Murchison Highway (A10).

Figure 6-1 Rosebery Mine location



The Rosebery Operation consists of an underground mine and surface mineral processing plant. The mining method uses mechanised long-hole open-stopping with footwall ramp access. Mineral processing applies sequential flotation and filtration to produce separate concentrates for zinc, lead and copper. In addition, the operation produces gold/silver doré bullion. Rosebery milled approximately 990kt of ore for the year ending 30 June 2018.

6.2 Mineral Resources – Rosebery

6.2.1 Results

The 2018 Rosebery Mineral Resources are summarised in Table 18. The Rosebery Mineral Resources is inclusive of the Ore Reserves.

Table 18 2018 Rosebery Mineral Resources tonnage and grade (as at 30 June 2018)

Rosebery Mineral Resources							Contained Metal				
	Tonnes (Mt)	Zinc (% Zn)	Lead (% Pb)	Copper (% Cu)	Silver (g/t Ag)	Gold (g/t Au)	Zinc ('000 t)	Lead ('000 t)	Copper ('000 t)	Silver (Moz)	Gold (Moz)
Rosebery											
Measured	6.4	8.5	2.9	0.21	113	1.3	548	188	13	23.3	0.3
Indicated	5.6	7.6	2.4	0.23	91	1.2	426	136	13	16.5	0.2
Inferred	6.0	7.4	2.8	0.28	89	1.4	443	165	17	17.2	0.3
Total	18.0	7.9	2.7	0.24	98	1.3	1,417	489	43	57.0	0.8
Stockpiles											
Measured	0.04	9.4	0.2	3.6	138	1.5	3	0	1	0	0.0
Total	0.04	9.4	0.2	3.6	138	1.5	3	0	1	0	0.0
Grand Total	18.1	7.9	2.7	0.24	98	1.3	1,420	490	43	57.1	0.8

Cut-off grade is based on Net Smelter Return (NSR), expressed as a dollar value of A\$167/t in the Lower Mine and A\$179 in the Upper Mine.

Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors.

Contained metal does not imply recoverable metal.

6.2.2 Mineral Resources JORC 2012 Assessment and Reporting Criteria

The following information provided in Table 19 complies with the 2012 JORC Code requirements specified by "Table-1 Section 1-3" of the Code.

Table 19 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Rosebery Mineral Resources 2018

Criteria	Status
Section 1 Sampling Techniques and Data	
Sampling techniques	<ul style="list-style-type: none"> Diamond drilling (DD) was used to obtain an average 1m sample that is half core split, crushed and pulverised to produce a pulp (>85% passing 75µm). DD core is selected, marked and ID tagged for sampling by the logging geologist. Sample details and ID are stored in the SQL database for correlation with returned geochemical assay results. Prior to May 2016, pulps were delivered to the ALS laboratory in Burnie, Tasmania for XRF analysis. Post May 2016 half core samples are delivered to the ALS laboratory in Burnie for sample preparation and XRF analysis. Analysis moved to the ALS Townsville laboratory in October, 2016. There are no inherent sampling problems recognised. Measures taken to ensure sample representivity include sizing analysis and duplication at the crush stage.
Drilling techniques	<ul style="list-style-type: none"> The drilling type is diamond core drilling from underground using single or double tube coring techniques. As of January 2014, drill core is oriented on an ad hoc basis. Drilling undertaken from 2012 is LTK48, LTK60, NQ, NQ2, NQTK, BQTK and BQ in size. Drilling in the reporting period is BQTK and NQ2. Historical (pre-2012) drillholes are a mixture of sizes from AQ, LTK (TT), BQ, NQ, HQ and PQ.
Drill sample recovery	<ul style="list-style-type: none"> Diamond drill core recoveries average 96%. Drill crews mark and define lost core intervals with blocks. Sample recovery is measured and recorded in the drillhole database. If excess core loss occurs in a mineralised zone the hole is re-drilled. The drilling process is controlled by the drill crew and geological supervision provides a means for maximising sample recovery and ensures suitable core presentation. No other measures are taken to maximise core recovery. There is no observable correlation between recovery and grade. Preferential loss/gains of fine or coarse materials are not significant and do not result in sample bias as the nature of mineralisation is massive to semi-massive sulphide, diamond core sampling is applied, and recovery is very high.
Logging	<ul style="list-style-type: none"> 100% of diamond drill core has been geologically and geotechnically logged to support Mineral Resources estimation, mining and metallurgy studies. Geological and geotechnical logging is mostly qualitative (some variables are quantitative). Logging is undertaken using laptop computers which store data directly to the drillhole database. All drill core is photographed, with photos labelled and stored on the Rosebery

Criteria	Status
	server.
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> • All samples included in the Rosebery Mineral Resources estimate are from diamond drill core. Drill core is longitudinally sawn to give half-core samples within intervals directed by the logging geologist. The remaining half-core is kept and stored in the original sample tray. Un-sampled core is now stored; prior to 2014 the un-sampled core was discarded. The standard sampling length is one metre with a minimum length of 40cm and maximum of 1.5m. • From 2005 until 2010 geological samples have been processed in the following manner: Dried, crushed and pulverised to 80% passing 75µm. Sizing analysis is carried out on 1:20 pulps. • From 2010 until 2016 geological samples have been processed in the following manner: Dried, crushed to 2mm; cone split to give primary and duplicate samples with the remainder rejected. Pulverised to 80% passing 75µm. Sizing analysis is carried out on 1:20 pulps. Samples despatched to ALS Burnie. • From 2016 geological samples have been processed at ALS Burnie in the following manner: Dried, crushed to 25mm, pulverised to 85% passing 75µm. Sizing analysis is carried out on 1:20 pulps. Samples are generally not split prior to pulverisation provided they weigh less than 3.5kg. The resulting pulps are bagged, labelled and boxed for despatch to ALS Brisbane and ALS Townsville. • Sample representivity is checked by sizing analysis and duplication at the crush stage. An issue with the sample preparation at ALS Burnie was recently identified by analysis of sample duplicate results. The investigation identified a problem with the coarse crush component of the sample preparation procedure at ALS Burnie. The error has been determined to have not materially impacted the accuracy or precision of the Rosebery samples and was rectified shortly after discovery. • The sample types, nature, quality and sample preparation techniques are considered appropriate for the style of the Rosebery mineralisation by the Competent Person.
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> • From 2005 until 2010 the assay methods undertaken by ALS Burnie for Rosebery were as follows: <ul style="list-style-type: none"> ○ 3-Acid Partial Digest (considered suitable for base metal sulphides). ○ Analysis of Pb, Zn, Cu, Ag, Fe by Atomic Absorption Spectrometry (AAS). ○ Au values are determined by fire assay. • From 2010 until 2016 the assay methods undertaken by ALS Burnie for Rosebery were as follows: <ul style="list-style-type: none"> ○ Dried, crushed to 2mm; cone split to give primary and duplicate samples with the remainder rejected. Pulverised to 80% passing 75µm. ○ Despatch to ALS Burnie. ○ Analysis of Pb, Zn, Cu and Fe by X-Ray Fluorescence (XRF) applying a lithium borate oxidative fusion (0.2g sub-sample charge). ○ Analysis of Ag by aqua regia digest and Atomic Absorption Spectrometry (AAS) (0.4g sub-sample charge). ○ Analysis of Au by fire assay, three acid digest and flame assay AAS (30g sub-sample charge). • From 2016 the assay methods undertaken by ALS Brisbane and Townsville

Criteria	Status
	<p>Rosebery were as follows:</p> <ul style="list-style-type: none"> ○ Analysis of Ag, Zn, Pb, Cu and Fe by four acid ore grade digest, ICPAES finish with extended upper reporting limits (ALS Brisbane). ○ Analysis of Au by fire assay, three acid digest and flame assay AAS (30g sub-sample charge) (ALS Townsville). • All of the above methods are considered effectively total and suitable for Mineral Resources estimation at Rosebery. • The employed assay techniques are considered suitable and representative; a comparison study using the Inductively Coupled Plasma (ICP) technique was completed to check the XRF accuracy in May 2013. Independent umpire laboratory ICP re-assay of 5% pulps took place in June 2015 and May 2016 using the Intertek laboratory in Perth. Pulps for analysis were randomly selected from a list of samples where (Pb + Zn)>5%. • No data from geophysical tools, spectrometers or handheld XRF instruments have been used for the estimation of Mineral Resources. • ALS laboratory Brisbane and Townsville releases its QAQC data to MMG for analysis of internal ALS standard performance. The performance of ALS internal standards appears to be satisfactory, with several standards used within the range of MMG submitted samples. • MMG routinely insert: <ul style="list-style-type: none"> ○ Matrix-matched standards, dolerite blanks and duplicates at a ratio of 1:20 to normal assays; ○ Blanks are inserted to check crush and pulverisation performance; ○ Duplicates are taken as quarter core, coarse crush and pulp repeats. • An umpire laboratory (Intertek Perth) is used to re-assay 5% of ore-grade pulps returned from the ALS laboratory. Analysis of routine sample results and control sample performance is reported monthly. • For the reporting period, sizing analysis of pulverised samples shows that 100% of samples passed the 85% passing 75µm. • QA/QC analysis has shown that: <ul style="list-style-type: none"> ○ Matrix-matched standards: Have continued to indicate a long term trend of under-reporting of zinc and lead (- 2.7%)- since moving to the ALS Brisbane facility this has improved. Gold, silver and copper standards have indicated an improvement in laboratory accuracy since moving to ALS Brisbane and Townsville. None of which degrades the Mineral Resources estimation confidence to any significant extent. ○ Blank performance for the reporting period has been good, with very low contamination rates. ○ An issue was recently identified with the duplicates namely around the sample preparation procedure. The process has been corrected and has been determined to have had no material impact on the accuracy or precision of the analyses over the period in question. ○ Umpire laboratory samples: Umpire pulp duplicates have historically displayed reasonable correlations. High CV%'s and differences of up to 6% (Fe) have been noted in the period where the sample preparation issue has occurred.

Criteria	Status
Verification of sampling and assaying	<ul style="list-style-type: none"> • All mineralised intersections, are viewed and verified by numerous company personnel by comparing assay results to core photos and logging. • Batches of sampling and assay data are entered by geologists; the performance of duplicates, blanks and standards is checked by the Mine Project Geologist after each assay batch is loaded to the database; batches with failed standards are flagged and pertinent samples are sent for re-assay. • Close twinning of mineralised intersections is not an intentional part of the delineation. However, the underground drill pattern often achieves a near-twinning or scissoring and this confirms individual intersections. • Re-assayed data, due to the failure of a standard, is reviewed to determine which batch is to be used for data export and Mineral Resources estimation. Batch status is recorded in the database for audit purposes. • Database validation algorithms are run to check data integrity before data is used for interpretation and Mineral Resources modelling. • Unreliable data is flagged and excluded from Mineral Resources estimation work. Data validation macros are used to identify data errors which are either rectified or excluded from the estimation process. • Since August 2014 all data below detection limit is replaced by half detection limit values. Prior to this date, the full detection limit was used. • No adjustments have been made to assay data – if there is any doubt about the data quality or location, the drillhole is excluded from the estimation process.
Location of data points	<ul style="list-style-type: none"> • Prior to March 2018, all diamond drillholes were downhole surveyed using a single-shot Reflex Ezi-shot tool at 30m intervals, with a full downhole Reflex gyro survey completed at end of hole by the drilling contractor. Where a gyro downhole survey is not practicable due to equipment limitations, then a multi-shot survey will be completed. • After March 2018, all diamond drillholes are downhole surveyed using a Champ Gyro north seeking survey tool which is used as a north-seeking tool for drillholes outside of the range between -20° and +20°. For holes between -20° and +20° drill holes are surveyed in the continuous mode (gyro using design azimuth for collar dip and azimuth). • Collar positions of underground drillholes are picked up by Rosebery mine surveyors using a Leica TPS 1200. Collar positions of surface drillholes are picked up by contract surveyors using differential GPS. Historically, surface drillhole collar locations were determined using a theodolite or handheld GPS. • Selected surface exploration drillholes have been downhole surveyed using a SPT north seeking gyro (parent holes only). • A downhole gyro measurement has been recorded from selective drillholes since March 2014 as an independent check of downhole survey accuracy. Initial analysis suggests the single shot surveys are accurate to 100m drillhole depth, and then diverge up to 4m at 400m depth. Given this outcome, gyro downhole surveys are now standard for all diamond holes. • Grid system used is the Cartesian Rosebery Mine Grid, offset from Magnetic North by 23.80° (as at March 1st, 2018) with mine grid origin at:

Criteria	Status
	<p>MGA94 E= 378981.981, N= 5374364.125; mine grid relative level (RL) equals AHD + 1.490m + 3048.000m.</p> <ul style="list-style-type: none"> • Topographic data derived from regular LIDAR overflights are carried out and correlated with surface field checks to confirm relativity to MGA and Rosebery Mine Grid.
Data spacing and distribution	<ul style="list-style-type: none"> • The Rosebery mineral deposit is drilled on variable spacing dependent on lens characteristics and access. Drill spacing ranges from 40m-60m to 10m-25m between sections and vertically. The final drill patterns vary mostly due to site access restrictions in some areas. Mineralisation has short scale structural variations observable in underground workings. Some of this variation is not discernible from drill data alone. Observations of mineralisation geometry are made by traditional geological mapping and more recently using photogrammetry images of mine development faces and backs. All ore drives and most non-ore development headings are mapped. • The combination of drill and other data is sufficient to establish the degree of geological and grade continuity appropriate for Mineral Resources and Ore Reserves estimation and the classifications applied. • Diamond drill samples are not composited prior to being sent to the laboratory however the nominal sample length is generally 1m. Reverse circulation drill samples are not used for Mineral Resources estimation.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> • Drillhole orientation is planned orthogonal to lens strike in vertical, radial fans. Drill fan spacing and orientation is planned to provide evenly spaced, high angle intercepts of the mineralised lenses where possible, thus minimising sampling bias related to orientation. Some drill intersections are at low angle to the dipping mineralisation due to access limitations. • Where drillholes from surface or older holes longer than 400m exist, attempts are made to confirm mineralised intercepts by repeat drilling from newly developed drives. Deep drill intersections are excluded from Mineral Resources modelling where duplicated by shorter underground drillholes. • Drilling orientation is not considered to have introduced sampling bias.
Sample security	<ul style="list-style-type: none"> • Measures to provide sample security include: <ul style="list-style-type: none"> ○ Samples are stored in a locked compound with restricted access during preparation. ○ Half-core samples for despatch to ALS Burnie are stored in sealed containers with security personnel at the MMG mine front gate for pick-up by ALS courier. ○ Receipt of samples acknowledged by ALS by email and checked against expected submission list. ○ Assay data returned separately in both spreadsheet and PDF formats.
Audit and reviews	<ul style="list-style-type: none"> • Coffey Mining Pty Ltd completed an audit of the core sample preparation area in April 2013. Key results are included in the 'Quality of assay data and laboratory tests' section above. • One internal audit each of the ALS Burnie, ALS Brisbane and ALS Townsville facilities were undertaken during the reporting period by the Competent Person. No material issues were identified during the inspections. There was however a sample preparation issue identified at ALS Burnie, This issue has

Criteria	Status
	<p>been rectified and has also been determined to have not materially impacted the precision or accuracy of the assays produced during the period in question. Historically, any issues identified have been rectified.</p>
<p>Section 2 Reporting of Exploration Results</p>	
<p>Mineral tenement and land tenure status</p>	<ul style="list-style-type: none"> • Rosebery Mine Lease ML 28M/1993 includes the Rosebery, Hercules and South Hercules polymetallic mines. It covers an area of 4,906 ha. • ML28M/93 located was granted to Pasminco Australia Limited by the State Government of Tasmania in May 1994. This lease represents the consolidation of 32 individual leases that previously covered the same area. • Tenure is held by MMG Australia Ltd for 30 years from 1st May 1994. • Lease expiry date is 1st May 2024. • The consolidated current mine lease includes two leases; (consolidated mining leases 32M/89 and 33M/89). These were explored in a joint venture with AngloGold Australia under the Rosebery Extension Joint Venture Heads of Agreement. This agreement covered two areas, one at the northern and the other at the southern end of the Rosebery Mine Lease, covering a total of 16.07 km². • The joint venture agreement was between the EZ Corp of Australia (now MMG Rosebery Mine) and Shell Company of Australia Limited (now AngloGold Australia Metals Pty. Ltd., formerly Acacia Resources (formerly Billiton)). A Heads of Agreement was signed on 16th May 1988 with initial participating interest of 50% for each party. Other partners in the joint venture are Little River Resources Ltd. and Norgold Ltd. They have a combined net smelter return royalty of 2.3695%, payable on production from the Rosebery Extension Joint Venture area. AngloGold withdrew from the joint venture on the 31st December 2001. • There are no known impediments to operating in the area.
<p>Exploration done by other parties</p>	<ul style="list-style-type: none"> • Tom Macdonald discovered the first indication of mineralisation in 1893 when he traced alluvial gold and zinc-lead sulphide boulders up Rosebery Creek. Twelve months later an expedition lead by Tom McDonald discovered the main lode through trenching operations, on what is now the 4 Level open cut (Easterbrook, 1962; Martin, 2002). • The Rosebery deposit was operated by several different operations until 1921 when the Electrolytic Zinc Company purchased both the Rosebery and Hercules Mines. • Drilling from surface and underground over time by current and previous owners has supported the discovery and delineation of Rosebery's mineralised lenses.
<p>Geology</p>	<ul style="list-style-type: none"> • The Rosebery volcanogenic massive sulphide (VMS) deposit is hosted within the Mt Read Volcanics, a Cambrian assemblage of lavas, volcanoclastics and sediments deposited in the Dundas Trough between the Proterozoic Rocky Cape Group and the Tyennan Block. • Sulphide mineralisation occurs in stacked stratabound massive to semi-massive base metal sulphide lenses between the Rosebery Thrust Fault and the Mt Black

Criteria	Status
	Thrust Fault; the host lithology and the adjoining faults all dip approximately 45 degrees east.
Drillhole information	<ul style="list-style-type: none"> • The Mineral Resources database consists of 5,903 diamond drillholes providing 249,483 samples. • No individual drillhole is material to the Mineral Resources estimate and hence this geological database is not supplied. • No exploration drilling took place in the 2017-2018 reporting period.
Data aggregation methods	<ul style="list-style-type: none"> • This is a Mineral Resources Statement and is not a report on exploration results hence no additional information is provided for this section. • No metal equivalents were used in the Mineral Resources estimation.
Relationship between mineralisation width and intercept lengths	<ul style="list-style-type: none"> • Mineralisation true widths are captured by interpreted mineralisation 3D wireframes. • Most drilling was at 50° to 60° angles in order to maximise true width intersections. • Geometry of mineralisation is interpreted as sub- vertical to vertical and as such current drilling allows true width of mineralisation to be determined.
Diagrams	<ul style="list-style-type: none"> • No individual drillhole is material to the Mineral Resources estimate and hence diagrams are not provided. • No exploration drilling took place in the 2017-2018 reporting period.
Balanced reporting	<ul style="list-style-type: none"> • This is a Mineral Resources Statement and is not a report on exploration results hence no additional information is provided for this section.
Other substantive exploration data	<ul style="list-style-type: none"> • This is a Mineral Resources Statement and is not a report on exploration results hence no additional information is provided for this section.
Further work	<ul style="list-style-type: none"> • Further underground near mine exploration drilling is being assessed.
Section 3 Estimating and Reporting of Mineral Resources	
Database integrity	<ul style="list-style-type: none"> • The following measures are in place to ensure database integrity: <ul style="list-style-type: none"> ○ All Rosebery drillhole data is stored in an SQL database on the Rosebery server, which is backed up at regular intervals. ○ Geological logging is entered directly into laptop computers which are uploaded to the database. Prior to 1996 DD holes were logged using Lotus spread sheets or on paper. ○ Assays are loaded into the database from spread sheets provided by the laboratory. • A database upgrade and full data migration was undertaken in November 2014. Several rounds of data migration checks were undertaken before allowing the database to go live. • Data validation procedures include: <ul style="list-style-type: none"> ○ Validation routines in the new database check for overlapping sample,

Criteria	Status								
	<p>lithological and alteration intervals.</p> <ul style="list-style-type: none"> ○ Random comparisons of raw data to recorded database data are undertaken prior to reporting for 5% of the additional drillholes added in any one year. No fatal flaws have been observed from this random data review. ○ Bulk data is imported into buffer tables and must be validated before being uploaded to the master database. 								
Site visits	<ul style="list-style-type: none"> • The 2018 Competent Person for Mineral Resources visits site on a regular basis. 								
Geological interpretation	<ul style="list-style-type: none"> • Economic Zn-Pb-Ag-Au mineralisation occurs as massive, semi massive and disseminated base metal sulphide lenses located within the Rosebery host sequence. Economic and near-economic mineralisation is easily visually identified in drill core and underground mine development. • Drill core is routinely sampled across zones of visible sulphide mineralisation. <p>The method used for defining mineralisation domains for the 2018 Lower Mine Mineral Resources estimate is described below:</p> <ul style="list-style-type: none"> • Peer reviewed exploratory data analysis was undertaken for each element of interest. • 3D wireframe models of each mineralisation style were created using an Indicator interpolation using Leapfrog Geo v4.2 software. Key data inputs included composited drill data converted to Indicators and mineralisation trend information derived from traditional mapping and high quality photo images of development faces and backs. • The interpolation uses a model representing the spatial variability of each variable and this was chosen on the basis of experimental variograms derived from the data. The variograms used are characterised by low nugget and ranges in the order of 60m-80m at low grade and 25m-30m at high grade. The ranges are strongly anisotropic. • The resultant wireframe models were visually compared to mapped or recorded mineralisation contacts from traditional geological mapping and Adamtech photo images. A close correlation between the models and points of observation is noted in most areas where data are available. • The domain models are broadly consistent with logged and mapped observations of the main lithology units present at mine scale, namely black shale, porphyry and the hanging wall and footwall contacts with the host sequence. <p>The Upper Mine Mineral Resources geological interpretation remains unchanged from previous years.</p>								
Dimensions	<ul style="list-style-type: none"> • The Rosebery mineral deposit extends from 400mE to 1800mE, 2500mN to -1100mN and 3400mRL to 1900mRL (Rosebery Mine grid co-ordinates) and is currently open to the north, south and at depth. Individual lenses vary in size from a few hundred metres up to 1000m along strike and/or down-dip. • The minimum, maximum and average thickness of the lower mine mineralised lenses are as follows: <table border="1" data-bbox="528 2051 1171 2078" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th data-bbox="528 2051 703 2078">Lens</th> <th data-bbox="703 2051 874 2078">Minimum (m)</th> <th data-bbox="874 2051 1045 2078">Maximum (m)</th> <th data-bbox="1045 2051 1171 2078">Mean (m)</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	Lens	Minimum (m)	Maximum (m)	Mean (m)				
Lens	Minimum (m)	Maximum (m)	Mean (m)						

Criteria	Status			
		K	0.2	36
	N	0.3	16	4
	P	0.2	12	3
	WXY (grouped)	0.3	21	3
Estimation and modelling techniques	<ul style="list-style-type: none"> • Lower mine: Grades estimation uses Ordinary Kriging (OK) as implemented in Maptek Vulcan version 10.1.5. The main inputs and parameters are described below: <ul style="list-style-type: none"> ○ Blocks and 1m composites flagged by domain and estimated individually. ○ Parent block size for estimation of 2mE x 7.5mN x 5mRL. ○ Block size approximates one half of drillhole spacing in northing and RL, and is consistent with the primary sampling interval in easting (1m). ○ Discretisation is 2x3x5 (X, Y, Z) for a total of 30 points per block. ○ Minimum sample search number is 8 and maximum number is 24. ○ Octant search methods were not used. ○ A minimum of 3 drillholes is required for a block to be estimated. ○ The block model covers the entire Lower Mine area. ○ Grade capping was applied to the high grade gold domain in some lenses. ○ A second estimation pass was used to estimate blocks in sparsely sampled areas not estimated in the primary estimation. • Upper mine: historical models have used either Ordinary Kriging or the inverse distance method. • All recoverable elements of economic interest to the Rosebery Operation (Zn, Pb, Cu, Ag, Au) and Fe have been estimated. • No other deleterious element or non-grade variables of economic significance have been identified – hence they are not estimated. • No dilution or recovery factors are taken into account during the estimation of Mineral Resources. These are addressed in the relevant Ore Reserves statement. • All metals are estimated individually, and no correlation between metals is assumed or used for estimation purposes. • Block model validation of the Lower Mine was conducted by: <ul style="list-style-type: none"> ○ Visual inspections for true fit with the high and low grade wireframes (to check for correct placement of blocks). ○ Visual comparison of block model grades against composite file grades. ○ Global statistical comparison of the estimated block model grades against the declustered composite statistics and raw length-weighted data. ○ Swath plots were generated and checked for K, N, P, W, X and Y lenses. The plots confirm overall consistency between data and estimates with a reasonable degree of smoothing. ○ Change of Support analysis was undertaken on most elements on a lens by lens basis. 			
Moisture	<ul style="list-style-type: none"> • Tonnes have been calculated on a dry basis, consistent with laboratory grade determinations. • No moisture calculations or assumptions are made in the modelling process. 			
Cut-off parameters	<ul style="list-style-type: none"> • Net Smelter Return (NSR) has been calculated for all block model blocks, and accounts for MMG's long-term economic assumptions (metal price, exchange rate), metal grades, metallurgical recoveries, smelter terms and conditions and 			

Criteria	Status
	<p>off-site costs. The NSR calculation was updated in April 2018.</p> <ul style="list-style-type: none"> Rosebery Lower Mine Mineral Resources were reported above a \$167/t NSR block grade cut-off. An example of minimum grades above \$167/t NSR cut-off is as follows: 4.5% Zn, 1.0% Pb, 15 g/t Ag, 0.8 g/t Au, 0.05% Cu. In the Upper Mine area the cut-off grade remains unchanged from the 2015 estimate and is \$179/t NSR. There has been no change to the Mineral Resources model, NSR calculation or NSR cut-off for the upper mine areas.
Mining factors or assumptions	<ul style="list-style-type: none"> Mineral Resources block models are used as the basis for detailed mine design and scheduling and to calculate derived NPV for the life of asset (LoA). Full consideration is made of the reasonable prospect of eventual economic extraction in relation to current and future economic parameters. All important assumptions including minimum mining width and dilution are included in the mine design process. Mined voids (stope and development drive shapes) are depleted from the final Mineral Resources estimate as at 30 June, 2018. For Mineral Resources in the vicinity of past mining areas, remnant pillars and other unrecovered Mineral Resources was identified after removing actual mined voids with a lateral margin of approximately 5m across strike. The 5m margin removed near-void skins and pillars as these are considered not to have reasonable prospects for eventual economic extraction.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> Metallurgical processing of ore at Rosebery involves crushing and grinding followed by flotation and filtration to produce saleable concentrates of copper, lead and zinc. Additionally, gold is partly recovered as doré following recovery from a gravity concentrator. Metallurgical recovery parameters for all payable elements are included in the NSR calculation, which is used as the cut-off grade for the Mineral Resources estimate. The metallurgical recovery function is based on recorded recoveries from the Rosebery concentrator and monitored in monthly reconciliation reports.
Environmental factors or assumptions	<ul style="list-style-type: none"> Environmental factors are considered in the Rosebery life of asset work, which is updated annually and includes provision for mine closure. Potentially acid forming (PAF) studies have been completed for sulphide-rich waste at Rosebery Mine in 2014. Determination of surface treatable and untreatable waste is currently determined by visual assessment guided by geological modelling and is not estimated or included in the 2018 Mineral Resources block models.
Bulk density	<ul style="list-style-type: none"> An empirical formula is used to determine the dry bulk density (DBD), based on Pb, Zn, Cu and Fe assays and assuming a fixed partition of the Fe species between chalcopyrite and pyrite. This formula is applied to the block model estimations after interpolation has been completed. The formula applied is: $DBD = 2.65 + 0.056 \times Pb\% + 0.0181 \times Zn\% + 0.0005 \times Cu\% + 0.0504 \times Fe\%$ A study conducted in August 1999 compared the estimated DBD against values determined using the weight in water, weight in air method and found the formula to be reliable. There has been no change to the formula in 2017-2018. A brief review was undertaken in the reporting period comparing estimated

Criteria	Status
	<p>density values (calculation applied to raw drillhole file) and the empirical formula – no material difference was identified.</p> <ul style="list-style-type: none"> • The Rosebery mineralisation does not contain significant voids or porosity. The DBD measurement does not attempt to account for any porosity.
Classification	<ul style="list-style-type: none"> • Mineral Resources classifications use criteria that required a minimum number of three drillholes. The spatial distribution of more than one drillhole ensures that any interpolated block was informed by sufficient samples to establish grade continuity. • Drillhole spacing for classification were based on an internal Rosebery drillhole spacing study undertaken in 2017. Results from the study indicate: <ul style="list-style-type: none"> ○ Measured Mineral Resources: 15m x 15m drillhole spacing ○ Indicated Mineral Resources: 30m x 30m drillhole spacing ○ Inferred Mineral Resources are generally defined as twice the spacing of Indicated Mineral Resources provided there is reasonable geological continuity. • Estimated zinc values were used for classification. • The Mineral Resources classification reflects the Competent Persons view on the confidence and uncertainty of the Rosebery Mineral Resources.
Audits or reviews	<ul style="list-style-type: none"> • A review was undertaken by AMC on the 2018 Rosebery Mineral Resource. AMC considers the Rosebery Mineral Resource estimate has been completed using usual industry practises and in accordance with the requirements and guidelines of the JORC Code 2012. MMG's approach is to include geological and grade components in compiling the resource estimates which AMC considers appropriate. AMC considers that the model forms a suitable basis for Mineral Resource reporting and for use in Ore Reserves and mining studies. No material issues were identified. • The 2018 Mineral Resources estimate was peer reviewed internally with no material issues identified.
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> • There is high geological confidence that the spatial location, continuity and estimated grades of the modelled lenses within the Rosebery Mineral Resources. The sheet-like, lensoidal nature of mineralisation historically exhibited is expected to be present in the remaining Mineral Resources at least at global scale. • Minor local variations are observed at a sub-20m scale; it is recognised that the short scale variation cannot be accurately captured even at very close drill spacing, and additional mapping data is important. Short scale geometry variation appears to be related to the preferential strain around relatively competent units in the mine sequence; there is little evidence of brittle fault offsets. • Twelve month rolling reconciliation figures for the Mineral Resources model to the mill treatment reports are within 10% for all metals with the exception of copper on an annual basis, suggesting that the Rosebery Mineral Resources estimation process is sound. • Mining and development images (including traditional mapping and digital photographic images) show good spatial correlation between modelled

Criteria	Status
	<p>mineralised boundaries and actual geology.</p> <ul style="list-style-type: none"> • The combination of Mineral Resources modelling, mapping, stope commentaries and face inspections provides reasonably accurate grade estimations for mill feed tracked on a basis of rolling weekly, monthly, quarterly and annually. • Remnant mineralisation in close proximity to voids in the upper and lower levels has been removed from the reported Mineral Resources. • The accuracy and confidence of this Mineral Resources estimate is considered suitable for mine planning and public reporting by the Competent Person.

6.2.3 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Mineral Resources statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Anna Lewin, confirm that I am the Competent Person for the Rosebery Mineral Resources section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a Member of The Australasian Institute of Mining and Metallurgy
- I have reviewed the relevant Rosebery Mineral Resources section of this Report to which this Consent Statement applies.

I am a contracted employee of MMG Ltd at the time of the estimation.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest

I verify that the Rosebery Mineral Resources section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to Rosebery Mineral Resources.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Rosebery Mineral Resources - I consent to the release of the 2018 Mineral Resources and Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resources and Ore Reserves Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

5/12/2018

Anna Lewin MAusIMM) (#992405)

Date:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resources and Ore Reserves Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Rex Berthelsen
Melbourne, VIC

Signature of Witness:

Witness Name and Residence: (e.g. town/suburb)

6.3 Ore Reserves – Rosebery

6.3.1 Results

The 2018 Rosebery Ore Reserves are summarised in Table 20.

Table 20 2018 Rosebery Ore Reserve tonnage and grade (as at 30 June 2018)

Rosebery Ore Reserves							Contained Metal				
	Tonnes (Mt)	Zinc (% Zn)	Lead (% Pb)	Copper (% Cu)	Silver (g/t Ag)	Gold (g/t Au)	Zinc (’000 t)	Lead (’000 t)	Copper (’000 t)	Silver (Moz)	Gold (Moz)
Rosebery											
Proved	3.7	8.3	3.0	0.22	114	1.4	303	8	111	13.5	0.2
Probable	1.7	7.3	2.9	0.19	113	1.4	123	3	49	6.1	0.1
Total	5.4	7.9	3.0	0.21	114	1.4	426	11	160	19.6	0.2
Stockpile											
Proved	0.02	9.3	3.5	0.19	135	1.4	2	0.05	0.87	0.11	0.00
Total	5.4	8.0	3.0	0.21	114	1.4	428	11	161	19.7	0.2

Tonnes and grade are rounded according to JORC Code guidelines and may show apparent addition errors.

Cut-off grade is based on Net Smelter Return after Royalties (NSR), expressed as a dollar value of A\$167/t.

Contained metal does not imply recoverable metal.

6.4 Ore Reserves JORC 2012 Assessment and Reporting Criteria

The following information provided in Table 21 complies with the 2012 JORC Code requirements specified by "Table-1 Section 4" of the Code.

Table 21 JORC 2012 Code Table 1 Assessment and Reporting Criteria for Rosebery Ore Reserve 2018

Assessment Criteria	Commentary
Mineral Resources estimate for conversion to Ore Reserves	<ul style="list-style-type: none"> • The Mineral Resources reported inclusive of the Mineral Resources used to define the Ore Reserves. • The Mineral Resources model used the MMG March 2018 Mineral Resources model. (ROS_1803_fm_reso_v3.bmf) • There is high geological confidence in the spatial location, continuity and estimated grades of the modelled lenses within the Rosebery Mineral Resources. The sheetlike, lensoidal nature of mineralisation historically exhibited is expected to be present in the remaining Mineral Resources at least at a global scale.
Site visits	<ul style="list-style-type: none"> • The Competent Person for the Dugald River Ore Reserves has frequently visited the site during 2017/2018.
Study status	<ul style="list-style-type: none"> • The mine is an operating site with on-going detailed Life of Asset planning.
Cut-off parameters	<ul style="list-style-type: none"> • The 2018 Mineral Resources and Ore Reserves have cut-off grades calculated, based on corporate guidance on metal prices and exchange rates. The site capital and operating costs, production profile, royalties and selling costs based on the 2018 Budget. Processing recoveries based on historical performance. • The breakeven cut-off grade (BCOG) and mineral Resources cut-off grade (RCOG) have been calculated using budget 2018 cost. • The operating costs, both fixed and variable, have been attributed on a per mined tonnes basis using the planned mine production rate of 1.0Mtpa • The Net Smelter Return (NSR) values have been based on metal prices, exchange rates, treatment charges and refinery charges (TC's & RC's), government royalties and metallurgical recoveries. • The NSR value for both BCOG and RCOG is to the mine gate and includes sustaining capital for the 2018 Ore Reserves. • Infill Diamond drilling has been included as part of the growth capital and not as sustaining capital • Concerning the Ore Reserves (OR) and Life of Asset (LoA), the break-even cut-off grade (BCOG) was used to evaluate the economic profitability. The Stope Cut-off Grade (SCOG) has been used to create the stope shapes only that includes a planned dilution. •

Assessment Criteria	Commentary																																			
		<table border="1"> <thead> <tr> <th data-bbox="786 259 940 331">Category of Cut-off</th> <th data-bbox="940 259 1093 331">Bud 2018 AU\$/t processed</th> <th data-bbox="1093 259 1189 331">Bud 2017 AU\$/t processed</th> <th data-bbox="1189 259 1426 331">Diff AU\$/t</th> </tr> </thead> <tbody> <tr> <td data-bbox="786 331 940 362">BCOG</td> <td data-bbox="940 331 1093 362">167</td> <td data-bbox="1093 331 1189 362">166</td> <td data-bbox="1189 331 1426 362">1</td> </tr> <tr> <td data-bbox="786 362 940 394">SCOG</td> <td data-bbox="940 362 1093 394">142</td> <td data-bbox="1093 362 1189 394">149</td> <td data-bbox="1189 362 1426 394">-7</td> </tr> <tr> <td data-bbox="786 394 940 425">DCOG</td> <td data-bbox="940 394 1093 425">60</td> <td data-bbox="1093 394 1189 425">81</td> <td data-bbox="1189 394 1426 425">-21</td> </tr> <tr> <td data-bbox="786 425 940 456">ICOG</td> <td data-bbox="940 425 1093 456">105</td> <td data-bbox="1093 425 1189 456">100</td> <td data-bbox="1189 425 1426 456">5</td> </tr> <tr> <td data-bbox="786 456 940 488">MCOG</td> <td data-bbox="940 456 1093 488">96</td> <td data-bbox="1093 456 1189 488">80</td> <td data-bbox="1189 456 1426 488">16</td> </tr> <tr> <td data-bbox="786 488 940 519">RCOG</td> <td data-bbox="940 488 1093 519">167</td> <td data-bbox="1093 488 1189 519">166</td> <td data-bbox="1189 488 1426 519">1</td> </tr> <tr> <td data-bbox="786 519 940 551">TCOG</td> <td data-bbox="940 519 1093 551">197</td> <td data-bbox="1093 519 1189 551">197</td> <td data-bbox="1189 519 1426 551">0</td> </tr> </tbody> </table>	Category of Cut-off	Bud 2018 AU\$/t processed	Bud 2017 AU\$/t processed	Diff AU\$/t	BCOG	167	166	1	SCOG	142	149	-7	DCOG	60	81	-21	ICOG	105	100	5	MCOG	96	80	16	RCOG	167	166	1	TCOG	197	197	0		
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RCOG	167	166	1																																	
TCOG	197	197	0																																	
Mining factors or assumptions	<ul style="list-style-type: none"> • Mining production carried out by long-hole open stoping with a Decline Access. The majority is a longitudinal retreat while some limited areas are by wider transverse stopes. • The lenses are divided into panels and are mined using a bottom-up sequence in a continuous 45 degree retreating front towards the level access drives. The nature of this mining sequence causes fluctuations in the grade profile of the short-term schedules. Each stoping panels contain between 3 and 5 sub-levels with crown pillars left in-situ between the backs of up-hole stopes and the lowest sill drive of the panel above. • Backfilling of stope voids is carried out using two methods; Cemented Rock Fill (CRF) and Rock Fill (RF). Up-hole retreat stopes left as an open void due to lack of access for fill placement. CRF and RF are filling methods adopted in the K, N, P, WU & X, and already developed WL & Y levels. • Stope design is carried out using the Mineable Shape Optimiser (MSO) process within the Deswik Software with the stope cut-off factor of AU\$142/t, allowing for a 0.5m to 1.5m hanging wall dilution within the designed shape. The length of each block used in MSO set at 5m with each Stope is a combination of three or four of these blocks giving a stope strike length of 15m or 20m. Stope strike lengths of 15m were used in W and X Lens while the others lenses used 20m. The height set to 20-25m (floor to floor) and the minimum mining width of 4.5m. The horizontal width has been adjusted to 4.65m to allow for the low dip of the ore body and to achieve the 4.5 m true widths. • A Mining Recovery factor of 70%-95%, depending on the area, is applied to Mined ore tonnes. • Access to the orebody is through a decline 5.5 mH x 5.5 mW at a 1:7 gradient. The standoff distance from orebody and stoping footwall and major infrastructure; stockpiles, vent rises, escape-ways, declines and ancillary development are 65m. • For Ore Reserve reporting no Inferred Mineral Resource material included in the mine design inventory. • Production of ore is in Measured and Indicated Mineral Resources only with grade control drilling programs scheduled to convert Indicated Mineral Resources before development or stoping activities. Ore development is strictly under survey control. Geological development control is currently not implemented at Rosebery. 																																			

Assessment Criteria	Commentary														
	<ul style="list-style-type: none"> The current primary ventilation system supplies approximately 550 m³/s (Measured at depth) of air to the underground mine, which is designed to allow extraction from the multiple ore lenses. 														
Geotechnical	<ul style="list-style-type: none"> Rosebery is one of the deepest mines in Australia with challenging ground conditions that result in the closure (squeezing) of development drives close to stoping areas and mining-induced seismicity. Just in time development, preferential drive orientations and high displacement support combined with multiple stages of rehabilitation are used to maintain serviceability of development. Seismic monitoring, seismic re-entry exclusion periods following massive stope firings and high displacement ground support are used to control risk to personnel from seismic events. Dilution is estimated based on the average overbreak recorded in reconciliations from adjacent stopes in the different panels/stoping areas of the mine which are then used to inform dilution for the ore reserve. Numerical modelling using both Linear elastic (MAP3D) and non-linear (Abacus) is conducted by MMG personnel and Beck Engineering to assess the overall mine sequence to minimise potential seismicity and drive closure. 														
Metallurgical factors or assumptions	<ul style="list-style-type: none"> Rosebery is a poly-metallic underground mine with all ore processed through an on-site mill and concentrator. Underground ore production sourced from multiple ore lenses. The table below outlines the critical production physicals for 2018. These based on actual data to June 2018 and forecast for the remainder of the year. The processing plant has a nameplate capacity of 1.0 Mtpa. The site is currently mine constrained, and mining and processing physicals are the same rates. Minimal stockpiles are maintained for the mill. <table border="1" data-bbox="624 1503 1334 1608"> <thead> <tr> <th>Tonnes (t)</th> <th>Zinc (%)</th> <th>Lead (%)</th> <th>Copper (%)</th> <th>Gold (g/t)</th> <th>Silver (g/t)</th> <th>Fe (%)</th> </tr> </thead> <tbody> <tr> <td>1,064,428</td> <td>9.1</td> <td>3.6</td> <td>0.26</td> <td>1.47</td> <td>122</td> <td>6.4</td> </tr> </tbody> </table> <ul style="list-style-type: none"> From the mill there are four saleable products generated: <ul style="list-style-type: none"> Gold Doré Copper Concentrate Zinc Concentrate Lead Concentrate The flow chart below outlines the block flowsheet, products and payable metals. Based on the grades for 2018 (table above), the subsequent recoveries calculated from the regression analysis. These have been determined by inputting the grades into the NSR calculator spreadsheet to determine the relevant recoveries. These are summarised in the below table. 	Tonnes (t)	Zinc (%)	Lead (%)	Copper (%)	Gold (g/t)	Silver (g/t)	Fe (%)	1,064,428	9.1	3.6	0.26	1.47	122	6.4
Tonnes (t)	Zinc (%)	Lead (%)	Copper (%)	Gold (g/t)	Silver (g/t)	Fe (%)									
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Assessment Criteria	Commentary					
	Product	Copper (%)	Zinc (%)	Lead (%)	Silver (g/t)	Gold (g/t)
	Zinc Concentrate		86%			
	Lead Concentrate		9%	82%	44%	17%
	Copper Concentrate	57%			40%	44%
	Gold Dore				0.2%	31%
Environmental	<ul style="list-style-type: none"> The 2/5 Tailings storage facility Dam was commissioned in April 2018. Commissioning included a new pump station, tailings pipeline and seepage collection ponds Waste water management at Rosebery involves collecting potentially contaminated water, including storm water and mine water at the Effluent Treatment Plant (ETP), where lime is added prior to pumping the whole volume of treated water to the Bobadil TSF via the Flume (an open concrete channel flowing under gravity to the TSF). After the final polishing stage, water is subsequently discharged to Lake Pieman. The ETP hydraulic capacity is approximately 600 l/sec and the plant is capable to receive 335 l/sec of site mine water with remaining limited spare capacity of approximately 265 l/sec to treat the site surface rain or storm water. Environmental legacy sites - There are a range of environmental legacy sites that are indirectly related to Rosebery that are being managed by MMG's Australia, Africa and Asia Regional hub (AAA). The historic Hercules area has a large impact on the land area and receiving waterways. This area is the most significant "legacy site" for Rosebery management. Smaller historic legacy sites include the Zeehan Smelter site, at least ten known historic mines such as Jupiter's, and a number of small historic workings. Waste rock - Waste rock is characterised as either NAF, PAF or High PAF. To-date the majority of waste rock produced has been retained underground and used for stope filling, either as RF or CRF. Previously, surplus waste rock was trucked to the surface and unloaded at the waste rock dump and was treated by adding a layer of lime on top and below every layer of waste rock. Recent Life of Asset (LoA) planning suggests there will be no requirement for waste rock to be trucked to surface. 					
Infrastructure	<ul style="list-style-type: none"> MMG Australia Limited holds title to the Rosebery Mine Lease (ML 28M/1993 – 4,906ha) which covers an area that includes the Rosebery, Hercules and South Hercules base and precious metal mines. Electric power to the site feeds in through No. 1 Substation located adjacent to the Mill Car Park on Arthur Street. There is a contract for the supply to the site with the Electrical Supply Authority for the region. The Commerce Department manages this, and all responsibilities (such as notification, to change in supply by either party) are detailed in this contract. The Electrical Supply Authority's substation currently has an N+1 arrangement which ensures that supply is maintained in the event of a loss of critical equipment (e.g. 					

Assessment Criteria	Commentary
	<p>Transformer). This also provides the Electrical Supply Authority with the ability to manage a potential increase in supply requirement by the site. Further, works are currently underway to provide an upgrade to the substation infrastructure, the result of which will provide a significant increase in the security of the supply to the site.</p> <ul style="list-style-type: none"> • Freshwater for the site is currently sourced from Lake Pieman, with allotments of 5,500 ML and 1,647 ML respectively. This will leave Lake Pieman as the sole source of fresh water. • In total, the Rosebery Mine operation employs 343 MMG people and a further 147 contractors, covering all aspects of the operation. Within the mining area, there are 175 MMG employees. • Primary communication from the Rosebery Mine site is by phone along with surface mobile phone coverage, provided by Telstra. Phones are available throughout the main office building along with the mill and other surface buildings. There is also an extension of the phone system underground. Along with the phone system, there is connected to email and internet services. This is available through the office area through a wireless system. • The main system for communication underground is through radio via a leaky feeder and fibre system. The radio system operates on multiple channels with general, extended discussion and emergency channels. • With mining activity taking place underground at Rosebery, access to the operating areas is by the main decline, "The Fletcher Decline". • While there are multiple paths from the certain points underground, only one main route is used to access the upper mid area of K Lens. From this point, access splits between two declines to the K/N/P Lens area and the W/X/Y Lenses. Other declines are used to direct return air. The ore is hauled out of the mine in a fleet of 55-60 tonne trucks. • The Rosebery primary ventilation circuit is essentially a series circuit where airflow accumulates airborne contaminants and heat as it progresses deeper into the mine, at the 46K Level fresh air is introduced into the circuit via the NDC shaft diluting contaminated air, and finally reporting to the return airways and exhausting to surface. The current primary ventilation system supplies approximately 550 m³/s of air usefully used in the lower part of the underground mine (Y Lens Exhaust, 61K Exhaust, 58W Exhaust, U/G Fuel bay, U/G Compressor and U/G Magazine). The system comprises three primary fan installations on the surface (PSF1, PSF2 and PSF3) and two booster fan installations underground (19B Booster Fans and 33P Booster Fans). The specifications of these fan installations are detailed below: <ul style="list-style-type: none"> ○ PSF1 (New NUC) are 2 x 1800 kW Howden centrifugal fans. Design Duty is 400 m³/s. ○ PSF 2 (Old NUC) is a single 550kW centrifugal fan. The duty is 100 m³/s.

Assessment Criteria	Commentary
	<ul style="list-style-type: none"> ○ PSF 3 (SUC) is 2 x 550 kW Korfmann KGL 2600 mm axial fans in parallel. The duty is 161 m³/s. ○ The 33P Booster fan is a Flaktwoods 550kW 2600 VP axial fan. ○ 19B Booster fans are 2 x Twin 110 kW CC1400 MK4 secondary fans mounted in parallel. • The main intake airways of the mine are the decline portal, No.2 Shaft and the NDC shaft. • A crib room and workshop facility at the 46K Level to provide these facilities closer to the current and ongoing working areas. • The concentrate is transported using the Emu Bay Railway, which is a freight only line that connects the West Coast area to the port in Burnie. • Tailings from the ore treatment were placed in a Tailings Storage Facility (TSF) located to the north of Rosebery at Bobadil until April 2018. Tailings have subsequently been discharged to the new 2/5 TSF to the south-west of the Rosebery township. • Other Rosebery site infrastructure includes mineral processing facilities (mill, concentrator, filtration and rail load-out), and buildings (offices, workshops, change-house).
Costs	<ul style="list-style-type: none"> • Costs used in assisting with the setting of the cut-off value used for the Ore Reserves estimation were based on the 2018 Budget. Costs were included of Operating and Sustaining Capital. • MMG Group Finance supplies the commodity price and exchange rate assumptions. These price assumptions, then apply to the period to which the ore is scheduled to be produced to determine the extracted NSR. • All applicable inflation rates, exchange rates, transportation charges, smelting & refining costs, penalties for failure to meet specification and royalties are included as part of the NSR calculations evaluated against the block model to estimate projected value. • No deleterious elements of economic significance occur in the concentrates.
Revenue factors	<ul style="list-style-type: none"> • Commodity prices and the exchange rate assumptions, treatment, refining, royalties and transportation costs for different commodities were supplied by MMG Group Finance and had been included in the NSR calculation. • The formulas and assumptions used in the NSR calculation are based on the historical data provided by the Rosebery Metallurgy Department. • The economic evaluation was carried out to verify whether the stope NSR value is above the designed using the NSR cut-off generate economic revenue. The mining physicals required to access and mine stopes were determined during the mine design process. The cost assumptions were applied to the mining physicals, and the revenue was calculated by multiplying the recovered ore tonnes by the appropriate NSR value. The profitable and marginal

Assessment Criteria	Commentary
	stopes were included in the Ore Reserves.
Market assessment	<ul style="list-style-type: none"> • Although the rate of growth of global zinc consumption is slowing, demand is still expected to increase by 1-2%pa over the medium term, with growth mainly coming from China the world's developing nations. • Stocks of refined zinc are currently at historically low levels after several years where production was constrained by limited mine production and concentrate availability. The low mine production resulted from a period of low metal prices and the closure of several major mines due to resource exhaustion. • Zinc mine production is now recovering as new mine projects and restarted operations such as Dugald River, Lady Loretta, Gamsberg and New Century come to the market during 2018 and 2019. Beyond these projects, there is uncertainty surrounding future new supply, while there is also limited growth in new smelting capacity. Increasingly stringent environmental regulations in China also restrict supply growth in that region. • New projects tend to be more economically challenging than existing or recently closed operations due to a range of factors including grade, size and location. • The combination of current low stocks, reasonable demand growth prospects and limitations on future supply should be supportive of the zinc price over the medium term. • Rosebery has life of mine agreements in place with Nyrstar covering 100% of zinc and lead concentrate production, which is sold to them on international terms. There is also good demand for Rosebery's small production of copper concentrates and this is covered by two long-term contracts.
Economic	<ul style="list-style-type: none"> • Rosebery is an established operating mine. Costs detailing used in the NPV calculation are based on historical data. Revenues are calculated based on historical and contracted realisation costs and realistic long-term metal prices. • The mine is profitable, and life-of-asset economic modelling shows that the Ore Reserves are economic. The Life of Asset (LOA) financial model demonstrates the mine has a positive NPV calculated. MMG uses a discount rate appropriate to the size and nature of the organisation and deposit.
Social	<ul style="list-style-type: none"> • The West Coast area of Tasmania has a strong, long history with mining. There are a large number of people employed by the mine from the town of Rosebery and the local government area. • Community issues and feedback associated with the Rosebery mine are generally received through the MMG Community Liaison Office. All issues are reported on a Communication and Complaints form and forwarded to the Administration and Community Assistant for action, per the Site Complaints Procedure. The Administration and Community Assistant makes direct contact with the complainant to

Assessment Criteria	Commentary																																													
	<p>discuss the issue and once details are understood, communicates with the department concerned to resolve the matter through to resolution.</p> <ul style="list-style-type: none"> • During the 2017/2018 reporting period, a total of three community complaints were received: one linked to noise from blasting; one relating to dust; and the third linked to water discharge. All complaints were investigated and resolved in consultation with the complainant. • A key social condition linked to the TSF was development of a community walking track and recreation area. Rosebery is on track to meet this condition in early 2019, with construction of the track and is nearing completion. • In 2019, Rosebery will also undertake a range of social performance activities, including updating the Rosebery social baseline study; Social Impact and Opportunities Assessment; and development of a management plan to support future social performance and impact management activities. 																																													
Tailings	<ul style="list-style-type: none"> • Construction of Stage 1 of the 2/5 TSF completed in April 2018. The table below outlines the expected tails storage capacities at the start of 2019 for Bobadil, and the completion of the stage lifts for Dam 2/5. <table border="1" data-bbox="555 1084 1412 1272"> <thead> <tr> <th>Location</th> <th>Tailings Capacity (Tonnes)</th> <th>Comment</th> </tr> </thead> <tbody> <tr> <td>Bobadil</td> <td>1,140,000</td> <td>Forecast 2019 completion</td> </tr> <tr> <td>Bobadil</td> <td>1,040,000</td> <td>Forecast 2022 completion</td> </tr> <tr> <td>Dam 2/5 – Stage 1</td> <td>2,250,000</td> <td>Completed and in use</td> </tr> <tr> <td>Dam 2/5 – Stage 2</td> <td>TBD</td> <td></td> </tr> </tbody> </table> <ul style="list-style-type: none"> • The status of approvals and communication with the government provided in the table below. All projects have been approved promptly with close communication maintained by the Environmental Protection Agency (EPA). • The table below details the current surface waste stockpiles, and lists those that could be used for backfill activities before closure. Some waste rock dumps are located under existing infrastructure, and could not recover before closure on the mine. <table border="1" data-bbox="555 1585 1348 1906"> <thead> <tr> <th>Location</th> <th>Closure Estimate (Tonnes)</th> <th>Assume Available* (Tonnes)</th> </tr> </thead> <tbody> <tr> <td>WRD Assay Creek</td> <td>330,000</td> <td>330,000</td> </tr> <tr> <td>WRD Overflow Car-park</td> <td>220,000</td> <td>-</td> </tr> <tr> <td>WRD behind 7L workshop</td> <td>570,000</td> <td>570,000</td> </tr> <tr> <td>WRD next to crusher</td> <td>540,000</td> <td>-</td> </tr> <tr> <td>WRD along William Street</td> <td>60,000</td> <td>60,000</td> </tr> <tr> <td>WRD next to Geo Core Shed</td> <td>130,000</td> <td>130,000</td> </tr> <tr> <td>WRD next to Services Workshop (BLDS16)</td> <td>60,000</td> <td>-</td> </tr> <tr> <td>4L Waste</td> <td>500,000</td> <td>500,000</td> </tr> <tr> <td>TOTAL</td> <td>2,410,000</td> <td>1,590,000</td> </tr> </tbody> </table> <p><i>* Assumes available for backfill activities before closure, WRD location not impacting the required infrastructure</i></p>	Location	Tailings Capacity (Tonnes)	Comment	Bobadil	1,140,000	Forecast 2019 completion	Bobadil	1,040,000	Forecast 2022 completion	Dam 2/5 – Stage 1	2,250,000	Completed and in use	Dam 2/5 – Stage 2	TBD		Location	Closure Estimate (Tonnes)	Assume Available* (Tonnes)	WRD Assay Creek	330,000	330,000	WRD Overflow Car-park	220,000	-	WRD behind 7L workshop	570,000	570,000	WRD next to crusher	540,000	-	WRD along William Street	60,000	60,000	WRD next to Geo Core Shed	130,000	130,000	WRD next to Services Workshop (BLDS16)	60,000	-	4L Waste	500,000	500,000	TOTAL	2,410,000	1,590,000
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Classification	<ul style="list-style-type: none"> • Ore Reserves classification follows the Mineral Resources classification where Proved Ore Reserves are only derived from Measured Mineral Resource, and Probable Ore Reserves are only 																																													

Assessment Criteria	Commentary
	<p>derived from Indicated Mineral Resources. No Inferred Mineral Resources have been included in the Ore Reserves.</p> <ul style="list-style-type: none"> • The results of the Ore Reserves appropriately reflect the Competent Person’s view of the deposit. • Where stopes contain more than one Mineral Resources category, then the individual classification components have been reported as outlined above.
Audit or Reviews	<ul style="list-style-type: none"> • The Processing and Mineral Resources competent person at Rosebery reviewed the NSR script to ensure correct operation for each model. Detail has been added to the script and a background document to track when and who has made changes. • Mineral Resources block models were validated during the design and evaluation process. • There has been an external audit carried out on the Ore Reserves process during 2018 for the 2017 Ore Reserve estimation. (AMC Consultants 20 July 2018). Below overall comment from AMC; • “Overall, AMC considers the methodology used to generate the 2017 Reserves follows good industry practise.”
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> • The key risks that could materially change or affect the Ore Reserves estimate for Rosebery include: <ul style="list-style-type: none"> ○ Seismicity: The Rosebery mine has had several significant seismic events in the past. Potential exists for future seismic events to occur that may potentially impact on the overall recovery of the Ore Reserves. ○ Induced stress: the depth of mining at Rosebery leads to drive closure and difficult mining conditions. This may impact the ability of Rosebery to extract the ore reserves contained within sill pillars. ○ Drop in zinc grade and metal price. • Close-spaced drilling is applied to define tonnage and grade before mining locally. Ore Reserves based on all available relevant information. <ul style="list-style-type: none"> ○ The Proved Ore Reserves is based on a local scale and is suitable as a local estimate. ○ The Probable Ore Reserves based on local and global scale information. • Ore Reserves accuracy and confidence that may have a material change in modifying factors discussed above. • This Ore Reserve based on the results of an operating mine. The confidence in the estimate compared with actual production data.

6.4.1 Expert Input Table

A number of persons have contributed key inputs to the Ore Reserves determination. These are listed below in Table 22.

In compiling the Ore Reserves, the Competent Person has reviewed the supplied information for reasonableness but has relied on this advice and information to be correct.

Table 22 Contributing Experts – Rosebery Ore Reserves

EXPERT PERSON / COMPANY	AREA OF EXPERTISE
Anna Lewin, Senior Resource Geologist MMG Ltd (Melbourne)	Geological Mineral Resources
Joshua Annear, Group Manager Business Evaluation, MMG Ltd (Melbourne)	Economic Assumptions
Steve Whitehead, General Manager Marketing, MMG Ltd (Melbourne)	Marketing, Sea freight and TC/RC
Kevin Rees, Senior Process Engineer, MMG Ltd (Melbourne)	Metallurgy
Angus J Henderson, Snr Mgr Commercial & Business Support, MMG Ltd (AAA)	Mining capital and Operating Costs
Christian Holland, Principal Geotechnical Engineer, MMG Ltd (Melbourne)	Geotechnical
Karel Steyn, Principal Mining Engineer, MMG Ltd (Melbourne)	Mining Parameters, Cut-off estimation, Mine Design and Scheduling
Donna Noonan, Principal Closure Planning, MMG Ltd (Melbourne)	Environmental

6.4.2 Statement of Compliance with JORC Code Reporting Criteria and Consent to Release

This Ore Reserve statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("2012 JORC Code").

Competent Person Statement

I, Karel Steyn, confirm that I am the Competent Person for the Rosebery Ore Reserve section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a Member of The Australasian Institute of Mining and Metallurgy
- I have reviewed the relevant Rosebery Ore Reserve section of this Report, to which this Consent Statement applies.

I am a full-time employee of MMG Ltd. at the time of the estimation.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest.

I verify that the Rosebery Ore Reserve section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Rosebery Ore Reserve.

Competent Person Consent

Pursuant to the requirements Clause 9 of the JORC Code 2012 Edition (Written Consent Statement)

With respect to the sections of this report for which I am responsible – the Rosebery Ore Reserves - I consent to the release of the 2018 Ore Reserves Statement as at 30 June 2018 Executive Summary and Technical Appendix Report and this Consent Statement by the directors of MMG Limited:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

5/12/2018

Karel Steyn MAusIMM (#309192)

Date:

This signature was scanned for the exclusive use in this document – the *MMG Mineral Resource and Ore Reserve Statement as at 30 June 2018* – with the author's approval. Any other use is not authorised.

Rex Berthelsen
Melbourne

Signature of Witness:

Witness Name and Residence: (e.g. town/suburb)

7 HIGH LAKE

This Mineral Resources remains unchanged since reporting in 2013. This information can be found in the 2013 MMG Mineral Resources and Ore Reserves Statement as at 30 June 2013 Technical Appendix.

8 IZOK LAKE

This Mineral Resources remains unchanged since reporting in 2013. This information can be found in the 2013 MMG Mineral Resources and Ore Reserves Statement as at 30 June 2013 Technical Appendix.